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PLANE AND SPHERICAL

TRIGONOMETRY.

BY

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BOSTON:
PUBLISHED BY GINN & COMPANY.
1887.

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PREFACE.

IN preparing this work the aim has been to furnish just so much of Trigonometry as is actually taught in our best schools and colleges. Consequently, development of functions in series and all other investigations that are important only for the special student have been omitted. The principles have been unfolded with the utmost brevity consistent with simplicity and clearness, and interesting problems have been selected with a view to awaken a real love for the study. Much time and labor have been spent in devising the simplest proofs for the propositions, and in exhibiting the best methods of arranging the logarithmic work.

The object of the work on Surveying and Navigation is to present these subjects in a clear and intelligible way, according to the best methods in actual use; and also to present them in so small a compass that students in general may find the time to acquire a competent knowledge of these very interesting and important studies.

The author is under particular obligation for assistance to G. A. Hill, A.M., of Cambridge, Mass., and to Prof. James L. Patterson, of Lawrenceville, N.J.

G. A. WENTWORTH.

PHILLIPS EXETER ACADEMY,
September, 1882.

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PLANE TRIGONOMETRY.

CHAPTER I.

TRIGONOMETRIC FUNCTIONS OF ACUTE ANGLES.

§ 1. DEFINITIONS.

THE sides and angles of a plane triangle are so related that any three given parts, provided at least one of them is a side, determine the shape and the size of the triangle.

Geometry shows how, from three such parts, to *construct* the triangle and find the values of the unknown parts.

Trigonometry shows how to *compute* the unknown parts of a triangle from the numerical values of the given parts.

Geometry shows in a general way that the sides and angles of a triangle are mutually dependent. Trigonometry begins by showing the exact nature of this dependence in the *right triangle*, and for this purpose employs the *ratios of its sides.*

Let MAN (Fig. 1) be an acute angle. If from any points B, D, F,..... in one of its sides perpendiculars BC, DE, FG,..... are let fall to the other side, then the right triangles ABC, ADE, AFG,..... thus formed have the angle A common, and are therefore mutually equiangular and similar. Hence, the ratios of their corresponding sides, pair by pair, are equal. That is,

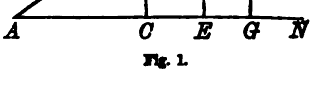

Fig. 1.

$$\frac{AC}{AB}=\frac{AE}{AD}=\frac{AG}{AF}; \quad \frac{AC}{BC}=\frac{AE}{DE}=\frac{AG}{FG}; \text{ etc.}$$

Hence, for every value of an acute angle A there are certain *numbers* that express the values of the ratios of the sides *in all right triangles that have this acute angle A.*

There are altogether six different ratios:

I. The ratio of the opposite leg to the hypotenuse is called the *Sine* of A, and is written $\sin A$.

II. The ratio of the adjacent leg to the hypotenuse is called the *Cosine* of A, and written $\cos A$.

III. The ratio of the opposite leg to the adjacent leg is called the *Tangent* of A, and written $\tan A$.

IV. The ratio of the adjacent leg to the opposite leg is called the *Cotangent* of A, and written $\cot A$.

V. The ratio of the hypotenuse to the adjacent leg is called the *Secant* of A, and written $\sec A$.

VI. The ratio of the hypotenuse to the opposite leg is called the *Cosecant* of A, and written $\csc A$.

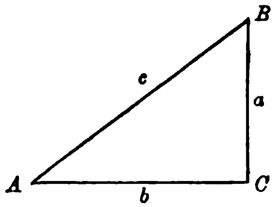

Fig. 2.

In the right triangle ABC (Fig. 2) let a, b, c denote the lengths of the sides opposite to the acute angles A, B, and the right angle C, respectively, these lengths being all expressed in terms of a common unit. Then,

$$\sin A = \frac{a}{c} = \frac{\text{opposite leg}}{\text{hypotenuse}}. \qquad \cos A = \frac{b}{c} = \frac{\text{adjacent leg}}{\text{hypotenuse}}.$$

$$\tan A = \frac{a}{b} = \frac{\text{opposite leg}}{\text{adjacent leg}}. \qquad \cot A = \frac{b}{a} = \frac{\text{adjacent leg}}{\text{opposite leg}}.$$

$$\sec A = \frac{c}{b} = \frac{\text{hypotenuse}}{\text{adjacent leg}}. \qquad \csc A = \frac{c}{a} = \frac{\text{hypotenuse}}{\text{opposite leg}}.$$

These six ratios are called the **Trigonometric Functions** of the angle A.

Exercise I.

1. What are the functions of the other acute angle B of the triangle ABC (Fig. 2)?

2. Prove that if two angles, A and B, are complements of each other (*i.e.*, if $A+B=90°$), then,

$$\sin A=\cos B, \quad \tan A=\cot B, \quad \sec A=\csc B;$$
$$\cos A=\sin B, \quad \cot A=\tan B, \quad \csc A=\sec B.$$

3. Find the values of the functions of A, if a, b, c respectively have the following values:

(i.) 3, 4, 5. (iii.) 8, 15, 17. (v.) 3.9, 8, 8.9.
(ii.) 5, 12, 13. (iv.) 9, 40, 41. (vi.) 1.19, 1.20, 1.69.

4. What condition must be fulfilled by the lengths of the three lines a, b, c (Fig. 2) in order to make them the sides of a right triangle? Is this condition fulfilled in Example 3?

5. Find the values of the functions of A, if a, b, c respectively have the following values:

(i.) $2mn,\ m^2-n^2,\ m^2+n^2.$ (iii.) $pqr,\ qrs,\ rsp.$

(ii.) $\dfrac{2xy}{x-y},\ x+y,\ \dfrac{x^2+y^2}{x-y}.$ (iv.) $\dfrac{mn}{pq},\ \dfrac{mv}{sq},\ \dfrac{nr}{ps}.$

6. Prove that the values of a, b, c, in (i.) and (ii.), Example 5, satisfy the condition necessary to make them the sides of a right triangle.

7. What equations of condition must be satisfied by the values of a, b, c, in (iii.) and (iv.), Example 5, in order that the values may represent the sides of a right triangle?

Compute the functions of A and B when,

8. $a=24,\ b=143.$ 11. $a=\sqrt{p^2+q^2},\ b=\sqrt{2pq}.$
9. $a=0.264,\ c=0.265.$ 12. $a=\sqrt{p^2+pq},\ c=p+q.$
10. $b=9.5,\ c=19.3.$ 13. $b=2\sqrt{pq},\ c=p+q.$

Compute the functions of A when,

14. $a = 2b$.
15. $a = \frac{3}{5}c$.
16. $a + b = \frac{5}{4}c$.
17. $a - b = \frac{c}{4}$.
18. Find a if $\sin A = \frac{3}{5}$ and $c = 20.5$.
19. Find b if $\cos A = 0.44$ and $c = 3.5$.
20. Find a if $\tan A = \frac{11}{3}$ and $b = 2\frac{5}{11}$.
21. Find b if $\cot A = 4$ and $a = 17$.
22. Find c if $\sec A = 2$ and $b = 20$.
23. Find c if $\csc A = 6.45$ and $a = 35.6$.

Construct a right triangle; given,

24. $c = 6$, $\tan A = \frac{3}{2}$.
25. $a = 3.5$, $\cos A = \frac{1}{2}$.
26. $b = 2$, $\sin A = 0.6$.
27. $b = 4$, $\csc A = 4$.

28. In a right triangle, $c = 2.5$ miles, $\sin A = 0.6$, $\cos A = 0.8$; compute the legs.

29. Construct (with a protractor) the ∠s 20°, 40°, and 70°; determine their functions by measuring the necessary lines, and compare the values obtained in this way with the more correct values given in the following table:

	sin	*cos*	*tan*	*cot*	*sec*	*csc*
20°	0.342	0.940	0.364	2.747	1.064	2.924
40°	0.643	0.766	0.839	1.192	1.305	1.556
70°	0.940	0.342	2.747	0.364	2.924	1.064

30. Find, by means of the above table, the legs of a right triangle if $A = 20°$, $c = 1$; also, if $A = 20°$, $c = 4$.

31. In a right triangle, given $a = 3$ and $c = 5$; find the hypotenuse of a similar triangle in which $a = 240{,}000$ miles.

32. By dividing the length of a vertical rod by the length of its horizontal shadow, the tangent of the angle of elevation of the sun at the time of observation was found to be 0.82. How high is a tower, if the length of its horizontal shadow at the same time is 174.3 yards?

§ 2. REPRESENTATION OF FUNCTIONS BY LINES.

The functions of an angle, being ratios, are numbers; but we may represent them by *lines* if we first choose a unit of length, and then construct right triangles, such that the denominators of the ratios shall be equal to this unit. The most convenient way to do this is as follows:

About a point O (Fig. 3) as a centre, with a radius equal to one unit of length, describe a circle and draw two diameters AA' and BB' perpendicular to each other.

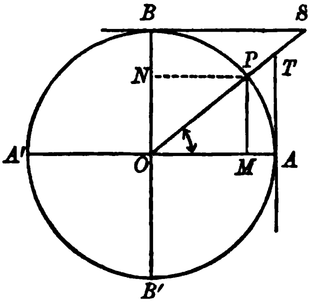

Fig. 3.

The circle with radius equal to 1 is called a *unit* circle, AA' the *horizontal*, and BB' the *vertical* diameter.

Let AOP be an acute angle, and let its value (in degrees, etc.) be denoted by x. We may regard the $\angle x$ as generated by a radius OP that revolves about O from the position OA to the position shown in the figure; viewed in this way, OP is called the *moving* radius.

Draw $PM \perp$ to OA. In the rt. $\triangle$ OPM the hypotenuse $OP = 1$; therefore, $\sin x = PM$; $\cos x = OM$.

Since PM is equal to ON, and ON is the projection of OP on BB', and since OM is the projection of OP on AA', therefore, *in a unit circle*,

$\sin x =$ projection of moving radius on vertical diameter;

$\cos x =$ projection of moving radius on horizontal diameter.

Through A and B draw tangents to the circle meeting OP, produced in T and S, respectively; then, in the rt. $\triangle$ OAT, the leg $OA = 1$, and in the rt. $\triangle$ OBS, the leg $OB = 1$; while the $\angle OSB = \angle x$ (why?). Therefore,

$$\tan x = AT; \quad \sec x = OT; \quad \cot x = BS; \quad \csc x = OS.$$

These six *line* values (as they may be termed) of the functions are all expressed in terms of the radius of the circle as a unit; and it is clear that as the angle varies in value the line values of the functions will always remain equal *numerically* to the ratio values. Hence, in studying the changes in the functions as the angle is supposed to vary, we may employ the simpler line values instead of the ratio values.

EXERCISE II.

1. Represent by lines the functions of a larger angle than that shown in Fig. 3.

2. Show that $\sin x$ is less than $\tan x$.

3. Show that $\sec x$ is greater than $\tan x$.

4. Show that $\csc x$ is greater than $\cot x$.

Construct the angle x if,

5. $\tan x = 3$. 7. $\cos x = \frac{1}{4}$. 9. $\sin x = 2 \cos x$.

6. $\csc x = 2$. 8. $\sin x = \cos x$. 10. $4 \sin x = \tan x$.

11. Show that the sine of an angle is equal to one-half the chord of twice the angle.

12. Find x if $\sin x$ is equal to one-half the side of a regular inscribed decagon.

13. Given x and y ($x + y$ being less than 90°); construct the value of $\sin(x + y) - \sin x$.

14. Given x and y ($x + y$ being less than 90°); construct the value of $\tan(x + y) - \sin(x + y) + \tan x - \sin x$.

Given an angle x; construct an angle y such that,

15. $\sin y = 2 \sin x$. 17. $\tan y = 3 \tan x$.

16. $\cos y = \frac{1}{2} \cos x$. 18. $\sec y = \csc x$.

19. Show by construction that $2 \sin A > \sin 2A$.

20. Given two angles A and B ($A + B$ being less than 90°); show that $\sin(A + B) < \sin A + \sin B$.

21. Given $\sin x$ in a unit circle; find the length of a line corresponding in position to $\sin x$ in a circle whose radius is r?

22. In a right triangle, given the hypotenuse c, and also $\sin A = m$, $\cos A = n$; find the legs.

§ 3. Changes in the Functions as the Angle Changes.

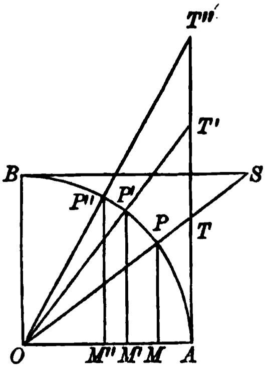

Fig. 4.

If we suppose the ∠ AOP, or x (Fig. 4) to increase gradually by the revolution of the moving radius OP about O, the point P will move along the arc AB towards B, T will move along the tangent AT away from A, S will move along the tangent BS towards B, and M will move along the radius OA towards O.

Hence, the lines PM, AT, OT will gradually increase in length, and the lines OM, BS, OS, will gradually decrease. That is,

As an acute angle increases, its sine, tangent, and secant also increase, while its cosine, cotangent, and cosecant decrease.

On the other hand, if we suppose x to decrease gradually, the reverse changes in its functions will occur.

If we suppose x to decrease to 0°, OP will coincide with OA and be parallel to BS. Therefore, PM and AT will vanish, OM will become equal to OA, while BS and OS will each be infinitely long, and be represented in value by the symbol ∞.

And if we suppose x to increase to 90°, OP will coincide with OB and be parallel to AT. Therefore, PM and OS will each be equal to OB, OM and BS will vanish, while AT and OT will each be infinite in length.

Hence, as the angle x increases from 0° to 90°,

$\sin x$ increases from 0 to 1,
$\cos x$ decreases from 1 to 0,
$\tan x$ increases from 0 to ∞,
$\cot x$ decreases from ∞ to 0,
$\sec x$ increases from 1 to ∞,
$\csc x$ decreases from ∞ to 1.

The values of the functions of 0° and of 90° are the *limiting* values of the functions of an acute angle. It is evident that (disregarding the limiting values),

Sines and cosines are always less than 1;

Secants and cosecants are always greater than 1;

Tangents and cotangents have all values between 0 and ∞.

REMARK. We are now able to understand why the sine, cosine, etc., of an angle are called *functions* of the angle. By a *function* of any magnitude is meant another magnitude which remains the same so long as the first magnitude remains the same, but changes in value for every change in the value of the first magnitude. This, as we now see, is the relation in which the sine, cosine, etc., of an angle stand to the angle.

§ 4. FUNCTIONS OF COMPLEMENTARY ANGLES.

The general form of two complementary angles is A and $90° - A$.

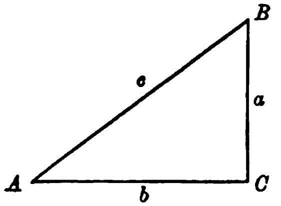

Fig. 5.

In the rt. △ ABC (Fig. 5)
$A + B = 90°$, hence $B = 90° - A$.
Therefore (§ 1),

$$\begin{aligned}\sin A &= \cos B = \cos(90° - A),\\ \cos A &= \sin B = \sin(90° - A),\\ \tan A &= \cot B = \cot(90° - A),\\ \cot A &= \tan B = \tan(90° - A),\\ \sec A &= \csc B = \csc(90° - A),\\ \csc A &= \sec B = \sec(90° - A).\end{aligned}$$

Therefore,

Each function of an acute angle is equal to the co-named function of the complementary angle.

NOTE. Cosine, cotangent, and cosecant are sometimes called *co-functions*; the words are simply abbreviated forms of *complement's sine*, *complement's tangent*, and *complement's secant*.

Hence, also,

Any function of an angle between 45° *and* 90° *may be found by taking the co-named function of the complementary angle between* 0° *and* 45°.

EXERCISE III.

1. Express the following functions as functions of the complementary angle:

$\sin 30°$. $\tan 89°$. $\csc 18° 10'$. $\cot 82° 19'$.
$\cos 45°$. $\cot 15°$. $\cos 37° 24'$. $\csc 54° 46'$.

2. Express the following functions as functions of an angle less than 45°:

$\sin 60°$. $\tan 57°$. $\csc 69° 2'$. $\cot 89° 59'$.
$\cos 75°$. $\cot 84°$. $\cos 85° 39'$. $\csc 45° 1'$.

3. Given $\tan 30° = \frac{1}{3}\sqrt{3}$; find $\cot 60°$.
4. Given $\tan A = \cot A$; find A.
5. Given $\cos A = \sin 2A$; find A.
6. Given $\sin A = \cos 2A$; find A.
7. Given $\cos A = \sin(45° - \frac{1}{2}A)$; find A.
8. Given $\cot \frac{1}{2}A = \tan A$; find A.
9. Given $\tan(45° + A) = \cot A$; find A.
10. Find A if $\sin A = \cos 4A$.
11. Find A if $\cot A = \tan 8A$.
12. Find A if $\cot A = \tan nA$.

§ 5. RELATIONS OF THE FUNCTIONS OF AN ANGLE.

Since (Fig. 5) $a^2 + b^2 = c^2$, therefore,

$$\frac{a^2}{c^2} + \frac{b^2}{c^2} = 1 \quad \text{or} \quad \left(\frac{a}{c}\right)^2 + \left(\frac{b}{c}\right)^2 = 1.$$

Therefore (§ 1), $(\sin A)^2 + (\cos A)^2 = 1$;

or, as usually written for convenience,

$$\sin^2 A + \cos^2 A = 1. \qquad [1]$$

That is: *The sum of the squares of the sine and the cosine of an angle is equal to unity.*

Formula [1] enables us to find the cosine of an angle when the sine is known, and *vice versa*. The values of $\sin A$ and of $\cos A$ deduced from [1] are:

$$\sin A = \sqrt{1-\cos^2 A}, \quad \cos A = \sqrt{1-\sin^2 A}.$$

Since $$\frac{a}{c} \div \frac{b}{c} = \frac{a}{c} \times \frac{c}{b} = \frac{a}{b},$$

therefore (§ 1), $$\tan A = \frac{\sin A}{\cos A}. \qquad [2]$$

That is: *The tangent of an angle is equal to the sine divided by the cosine.*

Formula [2] enables us to find the tangent of an angle when the sine and the cosine are known.

Since $\frac{a}{c} \times \frac{c}{a} = 1,\quad \frac{b}{c} \times \frac{c}{b} = 1,$ and $\frac{a}{b} \times \frac{b}{a} = 1,$

therefore (§ 1), $$\left.\begin{aligned} \sin A \times \csc A &= 1 \\ \cos A \times \sec A &= 1 \\ \tan A \times \cot A &= 1 \end{aligned}\right\}. \qquad [3]$$

That is: *The sine and the cosecant of an angle, the cosine and secant, and the tangent and cotangent, pair by pair, are reciprocals.*

The equations in [3] enable us to find an unknown function contained in any pair of these reciprocals when the other function in this pair is known.

EXERCISE IV.

1. Prove Formulas [1] – [3], using for the functions the line values in unit circle given in § 3.

2. Prove that $1 + \tan^2 A = \sec^2 A$.

   Hint. Divide the terms of the equation $a^2 + b^2 = c^2$ by b^2.

3. Prove that $1 + \cot^2 A = \csc^2 A$.

4. Prove that $\cot A = \dfrac{\cos A}{\sin A}$.

§ 6. APPLICATION OF FORMULAS [1]–[3].

Formulas [1], [2], and [3] enable us, when any one function of an angle is given, to find all the others. A given value of any one function, therefore, determines all the others.

EXAMPLE 1. Given $\sin A = \frac{2}{3}$; find the other functions.

By [1], $\cos A = \sqrt{1 - \frac{4}{9}} = \sqrt{\frac{5}{9}} = \frac{1}{3}\sqrt{5}.$

By [2], $\tan A = \frac{2}{3} \div \frac{1}{3}\sqrt{5} = \frac{2}{3} \times \frac{3}{\sqrt{5}} = \frac{2}{\sqrt{5}}.$

By [3], $\cot A = \frac{\sqrt{5}}{2}, \quad \sec A = \frac{3}{\sqrt{5}}, \quad \csc A = \frac{3}{2}.$

EXAMPLE 2. Given $\tan A = 3$; find the other functions.

By [2], $\frac{\sin A}{\cos A} = 3.$

And by [1], $\sin^2 A + \cos^2 A = 1.$

If we solve these equations (regarding $\sin A$ and $\cos A$ as two unknown quantities), we find that,

$$\sin A = 3\sqrt{\tfrac{1}{10}}, \quad \cos A = \sqrt{\tfrac{1}{10}}.$$

Then by [3], $\cot A = \frac{1}{3}, \quad \sec A = \sqrt{10}, \quad \csc A = \frac{1}{3}\sqrt{10}.$

EXAMPLE 3. Given $\sec A = m$; find the other functions.

By [3], $\cos A = \frac{1}{m}.$

By [1], $\sin A = \sqrt{1 - \frac{1}{m^2}} = \sqrt{\frac{m^2 - 1}{m^2}} = \frac{1}{m}\sqrt{m^2 - 1}.$

By [2], [3], $\tan A = \sqrt{m^2 - 1}, \quad \cot A = \frac{1}{\sqrt{m^2 - 1}},$

$$\csc A = \frac{m}{\sqrt{m^2 - 1}}.$$

EXERCISE V.

Find the values of the other functions when,

1. $\sin A = \frac{12}{13}$.
2. $\sin A = 0.8$.
3. $\cos A = \frac{60}{61}$.
4. $\cos A = 0.28$.
5. $\tan A = \frac{4}{3}$.
6. $\cot A = 1$.
7. $\cot A = 0.5$.
8. $\sec A = 2$.
9. $\csc A = \sqrt{2}$.
10. $\sin A = m$.
11. $\sin A = \frac{2m}{1+m^2}$.
12. $\cos A = \frac{2mn}{m^2+n^2}$.

13. Given $\tan 45° = 1$; find the other functions of 45°.

14. Given $\sin 30° = \frac{1}{2}$; find the other functions of 30°.

15. Given $\csc 60° = \frac{2}{3}\sqrt{3}$; find the other functions of 60°.

16. Given $\tan 15° = 2 - \sqrt{3}$; find the other functions of 15°.

17. Given $\cot 22° 30' = \sqrt{2} + 1$; find the other functions of 22° 30′.

18. Given $\sin 0° = 0$; find the other functions of 0°.

19. Given $\sin 90° = 1$; find the other functions of 90°.

20. Given $\tan 90° = \infty$; find the other functions of 90°.

21. Express the values of all the other functions in terms of $\sin A$.

22. Express the values of all the other functions in terms of $\cos A$.

23. Express the values of all the other functions in terms of $\tan A$.

24. Express the values of all the other functions in terms of $\cot A$.

25. Given $2 \sin A = \cos A$; find $\sin A$ and $\cos A$.

26. Given $4 \sin A = \tan A$; find $\sin A$ and $\tan A$.

27. If $\sin A : \cos A = 9 : 40$, find $\sin A$ and $\cos A$,

28. Transform the quantity $\tan^2 A + \cot^2 A - \sin^2 A - \cos^2 A$ into a form containing only $\cos A$.

29. Prove that $\sin A + \cos A = (1 + \tan A) \cos A$.

30. Prove that $\tan A + \cot A = \sec A \times \csc A$.

§ 7. FUNCTIONS OF 45°.

Let ABC (Fig. 6) be an isosceles right triangle, in which the length of the hypotenuse AB is equal to 1; then AC is equal to BC, and the angle A is equal to 45°. Since $\overline{AC}^2 + \overline{BC}^2 = 1$, therefore $2\,\overline{AC}^2 = 1$, and $AC = \sqrt{\tfrac{1}{2}} = \tfrac{1}{2}\sqrt{2}$.

Therefore (§ 1),

$$\sin 45^\circ = \cos 45^\circ = \tfrac{1}{2}\sqrt{2}.$$
$$\tan 45^\circ = \cot 45^\circ = 1.$$
$$\sec 45^\circ = \csc 45^\circ = \sqrt{2}.$$

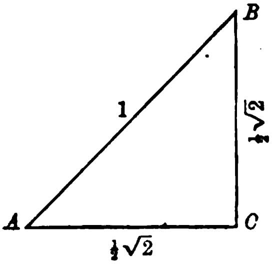

Fig. 6.

§ 8. FUNCTIONS OF 30° AND 60°.

Let ABC be an equilateral triangle in which the length of each side is equal to 1; and let CD bisect the angle C. Then CD is perpendicular to AB and bisects AB; hence, $AD = \tfrac{1}{2}$, and $CD = \sqrt{1 - \tfrac{1}{4}} = \sqrt{\tfrac{3}{4}} = \tfrac{1}{2}\sqrt{3}$.

In the right triangle ADC, the angle $ACD = 30°$, and the angle $CAD = 60°$.

Whence (§ 1),

$$\sin 30^\circ = \cos 60^\circ = \tfrac{1}{2}.$$
$$\cos 30^\circ = \sin 60^\circ = \tfrac{1}{2}\sqrt{3}.$$
$$\tan 30^\circ = \cot 60^\circ = \frac{1}{\sqrt{3}} = \tfrac{1}{3}\sqrt{3}.$$
$$\cot 30^\circ = \tan 60^\circ = \sqrt{3}.$$
$$\sec 30^\circ = \csc 60^\circ = \frac{2}{\sqrt{3}} = \tfrac{2}{3}\sqrt{3}.$$
$$\csc 30^\circ = \sec 60^\circ = 2.$$

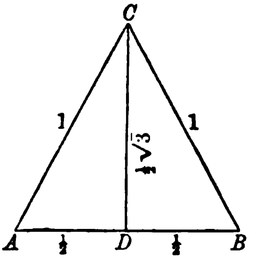

Fig. 7.

The results for sine and cosine of 30°, 45°, and 60° may be easily remembered by arranging them in the following form:

Angle...	30°	45°	60°	$\tfrac{1}{2} = 0.5$
Sine	$\tfrac{1}{2}$	$\tfrac{1}{2}\sqrt{2}$	$\tfrac{1}{2}\sqrt{3}$	$\tfrac{1}{2}\sqrt{2} = 0.70711$
Cosine...	$\tfrac{1}{2}\sqrt{3}$	$\tfrac{1}{2}\sqrt{2}$	$\tfrac{1}{2}$	$\tfrac{1}{2}\sqrt{3} = 0.86603$

CHAPTER II.

THE RIGHT TRIANGLE.

§ 9. THE GIVEN PARTS.

IN order to solve a right triangle, two parts besides the right angle must be given, one of them at least being a side.

The two given parts may be:

I. An acute angle and the hypotenuse.
II. An acute angle and the opposite leg.
III. An acute angle and the adjacent leg.
IV. The hypotenuse and a leg.
V. The two legs.

§ 10. CASE I.

Given $A = 34° 28'$ and $c = 18.75$; required B, a, b.

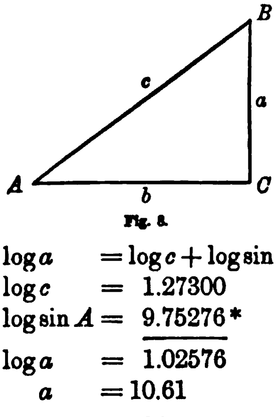

Fig. 8.

1. $B = 90° - A = 55° 32'$.

2. $\frac{a}{c} = \sin A$; $\therefore a = c \sin A$.

3. $\frac{b}{c} = \cos A$; $\therefore b = c \cos A$.

$$\begin{array}{ll|ll}
\log a & = \log c + \log \sin A & \log b & = \log c + \log \cos A \\
\log c & = \ \ 1.27300 & \log c & = \ \ 1.27300 \\
\log \sin A & = \ \ \underline{9.75276}\text{*} & \log \cos A & = \ \ \underline{9.91617} \\
\log a & = \ \ 1.02576 & \log b & = \ \ 1.18917 \\
a & = 10.61 & b & = 15.459
\end{array}$$

---

* For Logarithms, and directions how to use them, see Wentworth and Hill's *Five-place Tables*.

When −10 belongs to a logarithm or cologarithm, and is not written, it must be *remembered* that the logarithm or cologarithm is 10 too large.

§ 11. Case II.

Given $A = 62° 10'$, $a = 78$; find B, b, c.

1. $B = 90° - A = 27° 50'$.
2. $\frac{b}{a} = \cot A$; $\therefore b = a \cot A$.
3. $\frac{a}{c} = \sin A$.

$\therefore a = c \sin A$, and $c = \frac{a}{\sin A}$.

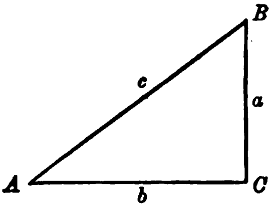

Fig. 9.

$\log b$	$= \log a + \log \cot A$	$\log c$	$= \log a + \operatorname{colog} \sin A$
$\log a$	$= 1.89209$	$\log a$	$= 1.89209$
$\log \cot A$	$= 9.72262$	$\operatorname{colog} \sin A$	$= 0.05340$
$\log b$	$= 1.61471$	$\log c$	$= 1.94549$
b	$= 41.182$	c	$= 88.204$

§ 12. Case III.

Given $A = 50° 2'$, $b = 88$; find B, a, c.

1. $B = 90° - A = 39° 58'$.
2. $\frac{a}{b} = \tan A$; $\therefore a = b \tan A$.
3. $\frac{b}{c} = \cos A$.

$\therefore b = c \cos A$, and $c = \frac{b}{\cos A}$.

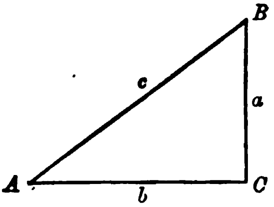

Fig. 10.

$\log a$	$= \log b + \log \tan A$	$\log c$	$= \log b + \operatorname{colog} \cos A$
$\log b$	$= 1.94448$	$\log b$	$= 1.94448$
$\log \tan A$	$= 10.0767$	$\operatorname{colog} \cos A$	$= 0.19223$
$\log a$	$= 2.02118$	$\log c$	$= 2.13671$
a	$= 105.0$	c	$= 137.0$

§ 13. CASE IV.

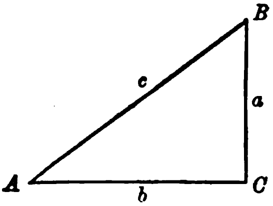

Fig. 11.

Given $c = 58.40$, $a = 47.55$; find A, B, b.

1. $\sin A = \frac{a}{c}$.

2. $B = 90° - A$.

3. $\frac{b}{a} = \cot A$; $\quad \therefore b = a \cot A$.

$$\begin{aligned} \log \sin A &= \log a + \operatorname{colog} c \\ \log a &= 1.67715 \\ \operatorname{colog} c &= \underline{8.23359} \\ \log \sin A &= 9.91074 \\ A &= 54° 31' \\ B &= 35° 29' \end{aligned}$$

$$\begin{aligned} \log b &= \log a + \log \cot A \\ \log a &= 1.67715 \\ \log \cot A &= \underline{9.85300} \\ \log b &= 1.53015 \\ b &= 33.896 \end{aligned}$$

§ 14. CASE V.

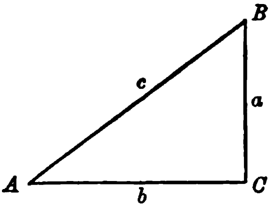

Fig. 12.

Given $a = 40$, $b = 27$; find A, B, c.

1. $\tan A = \frac{a}{b}$.

2. $B = 90° - A$.

3. $\frac{a}{c} = \sin A$.

$\therefore a = c \sin A$; $\quad \therefore c = \frac{a}{\sin A}$.

$$\begin{aligned} \log \tan A &= \log a + \operatorname{colog} b \\ \log a &= 1.60206 \\ \operatorname{colog} b &= \underline{8.56864} \\ \log \tan A &= 10.17070 \\ A &= 55° 59' \\ B &= 34° 1' \end{aligned}$$

$$\begin{aligned} \log c &= \log a + \operatorname{colog} \sin A \\ \log a &= 1.60206 \\ \operatorname{colog} \sin A &= \underline{0.08152} \\ \log c &= 1.68358 \\ c &= 48.259 \end{aligned}$$

§ 15. GENERAL METHOD OF SOLVING THE RIGHT TRIANGLE.

From these five cases it appears that the general method of finding an unknown part in a right triangle is as follows:

Choose from the equation $A + B = 90°$, and the equations that define the functions of the angles, an equation in which the required part only is unknown; solve this equation, if necessary, to find the value of the unknown part; then compute the value, using logarithms whenever convenient.

NOTE 1. In Cases IV. and V. the unknown side may also be found by Geometry, from the equation $a^2 + b^2 = c^2$; whence we obtain

(for Case IV.) $b = \sqrt{c^2 - a^2} = \sqrt{(c+a)(c-a)}$;

(for Case V.) $c = \sqrt{a^2 + b^2}$.

These equations express the values of b and c directly in terms of the two given sides; and if the values of the sides are simple numbers (*e.g.* 5, 12, 13), it is often easier to find b or c in this way. But this value of c is not adapted to logarithms, and this value of b is not so readily worked out by logarithms as the value of b given in § 13.

NOTE 2. In Case IV. if the given sides (here a and c) are nearly alike in value, then A is near 90°, and its value cannot be accurately found from the tables, because the sines of large angles differ little in value (as is evident from Fig. 4). In this case it is better to find B first, by means of a formula proved later (see page 47); viz.,

$$\tan \tfrac{1}{2} B = \sqrt{\frac{c-a}{c+a}};$$

and to find b by the method given in Note 1, since the same logarithms are used in both cases.

EXAMPLE. Given $a = 49$, $c = 50$; find A, B, b.

$$\begin{aligned}
\log b &= \tfrac{1}{2}[\log(c-a) + \log(c+a)] \\
c - a &= 1 \\
c + a &= 99 \\
\log(c-a) &= 0.00000 \\
\log(c+a) &= \underline{1.99564} \\
&\; 2\overline{)1.99564} \\
\log b &= 0.99782 \\
b &= 9.95
\end{aligned}$$

$$\begin{aligned}
\log\tan\tfrac{1}{2}B &= \tfrac{1}{2}[\log(c-a) \\
&\qquad + \operatorname{colog}(c+a)] \\
\log(c-a) &= 0.00000 \\
\operatorname{colog}(c+a) &= \underline{8.00436} \\
&\; 2\overline{)\underline{8.00436}} \\
\log\tan\tfrac{1}{2}B &= 9.00218 \\
\tfrac{1}{2}B &= 5° 44' 21'' \\
B &= 11° 29' \\
A &= 78° 31'
\end{aligned}$$

§ 16. AREA OF THE RIGHT TRIANGLE.

It is shown in Geometry that the area of a triangle is equal to one-half the product of the base by the altitude.

Therefore, if a and b denote the legs of a right triangle, and F the area,

$$F = \tfrac{1}{2}ab.$$

By means of this formula the area may always be found when a and b are given or have been computed.

For example: Find the area, having given:

CASE I. (§ 10).

$A = 34^\circ 28'$, $c = 18.75$.

First find (as in § 10) $\log a$ and $\log b$.

$$\log(F) = \log a + \log b + \operatorname{colog} 2$$

$$\begin{aligned} \log a &= 1.02578 \\ \log b &= 1.18915 \\ \operatorname{colog} 2 &= \underline{9.69897} \\ \log(F) &= 1.91390 \\ F &= 82.016 \end{aligned}$$

CASE IV. (§ 13).

$a = 47.54$, $c = 58.40$.

First find (as in § 13) $\log a$ and $\log b$.

$$\log(F) = \log a + \log b + \operatorname{colog} 2$$

$$\begin{aligned} \log a &= 1.67715 \\ \log b &= 1.53025 \\ \operatorname{colog} 2 &= \underline{9.69897} \\ \log(F) &= 2.90637 \\ F &= 806.06 \end{aligned}$$

EXERCISE VI.

1. In Case II. give another way of finding c, after b has been found.

2. In Case III. give another way of finding c, after a has been found.

3. In Case IV. give another way of finding b, after the angles have been found.

4. In Case V. give another way of finding c, after the angles have been found.

5. Given B and c; find A, a, b.
6. Given B and b; find A, a, c.
7. Given B and a; find A, b, c.
8. Given b and c; find A, B, a.

Solve the following triangles:

	GIVEN:		REQUIRED:		
9	$a=6$,	$c=12$.	$A=30^\circ$,	$B=60^\circ$,	$b=10.392$.
10	$A=60^\circ$,	$b=4$.	$B=30^\circ$,	$c=8$,	$a=6.9282$.
11	$A=30^\circ$,	$a=3$.	$B=60^\circ$,	$c=6$,	$b=5.1961$.
12	$a=4$,	$b=4$.	$A=B=45^\circ$, $c=5.6568$.		
13	$a=2$,	$c=2.82843$.	$A=B=45^\circ$, $b=2$.		
14	$c=627$,	$A=23^\circ\,30'$.	$B=66^\circ\,30'$,	$a=250.02$,	$b=575.0$.
15	$c=2280$,	$A=28^\circ\,5'$.	$B=61^\circ\,55'$,	$a=1073.3$,	$b=2011.6$.
16	$c=72.15$,	$A=39^\circ\,34'$.	$B=50^\circ\,26'$,	$a=45.958$,	$b=55.620$.
17	$c=1$,	$A=36^\circ$.	$B=54^\circ$,	$a=0.58779$,	$b=0.80902$.
18	$c=200$,	$B=21^\circ\,47'$.	$A=68^\circ\,13'$,	$a=185.73$,	$b=74.22$.
19	$c=93.4$,	$B=76^\circ\,25'$.	$A=13^\circ\,35'$,	$a=21.936$,	$b=90.788$.
20	$a=637$,	$A=\ \ 4^\circ\,35'$.	$B=85^\circ\,25'$,	$b=7946$,	$c=7971.5$.
21	$a=48.532$,	$A=36^\circ\,44'$.	$B=53^\circ\,16'$,	$b=65.031$,	$c=81.144$.
22	$a=0.0008$,	$A=86^\circ$.	$B=\ \ 4^\circ$,	$b=0.0000559$,	$c=0.000802$
23	$b=50.937$,	$B=43^\circ\,48'$.	$A=46^\circ\,12'$,	$a=53.116$,	$c=73.59$.
24	$b=2$,	$B=\ \ 3^\circ\,38'$.	$A=86^\circ\,22'$,	$a=31.497$,	$c=31.560$.
25	$a=992$,	$B=76^\circ\,19'$.	$A=13^\circ\,41'$,	$b=4074.5$.	$c=4193.6$.
26	$a=73$,	$B=68^\circ\,52'$.	$A=21^\circ\,8$,	$b=188.86$,	$c=202.47$.
27	$a=2.189$,	$B=45^\circ\,25'$.	$A=44^\circ\,35'$,	$b=2.2211$,	$c=3.1185$.
28	$b=4$,	$A=37^\circ\,56'$.	$B=52^\circ\,4'$,	$a=3.1176$,	$c=5.0714$.
29	$c=8590$,	$a=4476$.	$A=31^\circ\,24'$,	$B=58^\circ\,36'$,	$b=7332.8$.
30	$c=86.53$,	$a=71.78$.	$A=56^\circ\,3'$,	$B=33^\circ\,57'$,	$b=48.324$.
31	$c=9.35$,	$a=8.49$.	$A=65^\circ\,14'$,	$B=24^\circ\,46'$,	$b=3.917$.
32	$c=2194$,	$b=1312.7$.	$A=53^\circ\,15'$,	$B=36^\circ\,45'$,	$a=1758$.
33	$c=30.69$,	$b=18.256$.	$A=53^\circ\,30'$,	$B=36^\circ\,30'$,	$a=24.67$.
34	$a=38.313$,	$b=19.522$.	$A=63^\circ$,	$B=27^\circ$,	$c=43$.
35	$a=1.2291$,	$b=14.950$.	$A=\ \ 4^\circ\,42'$,	$B=85^\circ\,18'$,	$c=15$.
36	$a=415.38$,	$b=62.080$.	$A=81^\circ\,30'$,	$B=\ \ 8^\circ\,30'$,	$c=420$.
37	$a=13.690$,	$b=16.926$.	$A=38^\circ\,58'$,	$B=51^\circ\,2'$,	$c=21.769$.
38	$c=91.92$,	$a=2.19$.	$A=1^\circ\,21'\,55''$,	$B=88^\circ\,38'\,5''$,	$b=91.894$.

Compute the unknown parts and also the area, having given:

39. $a=5$, $b=6$.
40. $a=0.615$, $c=70$.
41. $b=\sqrt[3]{2}$, $c=\sqrt{3}$.
42. $a=7$, $A=18^\circ\,14'$.
43. $b=12$, $A=29^\circ\,8'$.
44. $c=68$, $A=69^\circ\,54'$.
45. $c=27$, $B=44^\circ\,4'$.
46. $a=47$, $B=48^\circ\,49'$.
47. $b=9$, $B=34^\circ\,44'$.
48. $c=8.462$. $B=86^\circ\,4'$.

49. Find the value of F in terms of c and A.

50. Find the value of F in terms of a and A.

51. Find the value of F in terms of b and A.

52. Find the value of F in terms of a and c.

53. Given $F = 58$, $a = 10$; solve the triangle.

54. Given $F = 18$, $b = 5$; solve the triangle.

55. Given $F = 12$, $A = 29°$; solve the triangle.

56. Given $F = 100$, $c = 22$; solve the triangle.

57. Find the angles of a right triangle if the hypotenuse is equal to three times one of the legs.

58. Find the legs of a right triangle if the hypotenuse $= 6$, and one angle is twice the other.

59. In a right triangle given c, and $A = nB$; find a and b.

60. In a right triangle the difference between the hypotenuse and the greater leg is equal to the difference between the two legs; find the angles.

The angle of elevation of an object (or angle of depression, if the object is below the level of the observer) is the angle which a line from the eye to the object makes with a horizontal line in the same vertical plane.

61. At a horizontal distance of 120 feet from the foot of a steeple, the angle of elevation of the top was found to be $60° 30'$; find the height of the steeple.

62. From the top of a rock that rises vertically 326 feet out of the water, the angle of depression of a boat was found to be $24°$; find the distance of the boat from the foot of the rock.

63. How far is a monument, in a level plain, from the eye, if the height of the monument is 200 feet and the angle of elevation of the top $3° 30'$?

64. In order to find the breadth of a river a distance AB was measured along the bank, the point A being directly opposite a tree C on the other side. The angle ABC was also measured. If $AB = 96$ feet, and $ABC = 21° 14'$, find the breadth of the river.

If $ABC = 45°$, what would be the breadth of the river?

65. Find the angle of elevation of the sun when a tower a feet high casts a horizontal shadow b feet long. Find the angle when $a = 120$, $b = 70$.

66. How high is a tree that casts a horizontal shadow b feet in length when the angle of elevation of the sun is $A°$? Find the height of the tree when $b = 80$, $A = 50°$.

67. What is the angle of elevation of an inclined plane if it rises 1 foot in a horizontal distance of 40 feet?

68. A ship is sailing due north-east with a velocity of 10 miles an hour. Find the rate at which she is moving due north, and also due east.

69. In front of a window 20 feet high is a flower-bed 6 feet wide. How long must a ladder be to reach from the edge of the bed to the window?

70. A ladder 40 feet long may be so placed that it will reach a window 33 feet high on one side of the street, and by turning it over without moving its foot it will reach a window 21 feet high on the other side. Find the breadth of the street.

71. From the top of a hill the angles of depression of two successive milestones, on a straight level road leading to the hill, are observed to be 5° and 15°. Find the height of the hill.

72. A fort stands on a horizontal plain. The angle of elevation at a certain point on the plain is 30°, and at a point 100 feet nearer the fort it is 45°. How high is the fort?

73. From a certain point on the ground the angles of elevation of the belfry of a church and of the top of the steeple were found to be 40° and 51° respectively. From a point 300 feet farther off, on a horizontal line, the angle of elevation of the top of the steeple is found to be 33° 45′. Find the distance from the belfry to the top of the steeple.

74. The angle of elevation of the top of an inaccessible fort C, observed from a point A, is 12°. At a point B, 219 feet from A and on a line AB perpendicular to AC, the angle ABC is 61° 45′. Find the height of the fort.

§ 17. THE ISOSCELES TRIANGLE.

An isosceles triangle is divided by the perpendicular from the vertex to the base into two equal right triangles.

Therefore, an isosceles triangle is determined by any two parts that determine one of these right triangles.

Let the parts of an isosceles triangle ABC (Fig. 13), among which the altitude CD is to be included, be denoted as follows:

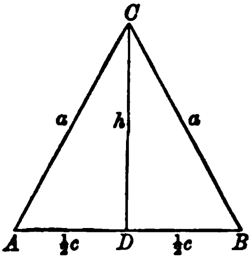

Fig. 13.

$a =$ one of the equal sides.
$c =$ the base.
$h =$ the altitude.
$A =$ one of the equal angles.
$C =$ the angle at the vertex.

For example: Given a and c; required A, C, h.

1. $\cos A = \frac{\frac{1}{2}c}{a} = \frac{c}{2a}$.

2. $C + 2A = 180°$; $\therefore C = 180° - 2A = 2(90° - A)$.

3. h may be found directly in terms of a and c from the equation

$$h^2 + \frac{c^2}{4} = a^2,$$

which gives $$h = \sqrt{(a - \frac{1}{2}c)(a + \frac{1}{2}c)}.$$

But it is better to find the angles first, and then find h from either one of the two equations,

$$\frac{h}{a} = \sin A, \quad \text{or} \quad \frac{h}{\frac{1}{2}c} = \tan A.$$

whence $$h = a \sin A, \text{ or } \quad h = \tfrac{1}{2}c \tan A.$$

The numerical values of A, C, and h may be computed by the aid of logarithms, as in the case of the right triangle.

The area F of the triangle may be found, when c and h are given or have been found, by means of the formula

$$F = \tfrac{1}{2}ch.$$

EXERCISE VII.

In an isosceles triangle:

1. Given a and A; find C, c, h.
2. Given a and C; find A, c, h.
3. Given c and A; find C, a, h.
4. Given c and C; find A, a, h.
5. Given h and A; find C, a, c.
6. Given h and C; find A, a, c.
7. Given a and h; find A, C, c.
8. Given c and h; find A, C, a.
9. Given $a = 14.3$, $c = 11$; find A, C, h.
10. Given $a = 0.295$, $A = 68° 10'$; find c, h, F.
11. Given $c = 2.352$, $C = 69° 49'$; find a, h, F.
12. Given $h = 7.4847$, $A = 76° 14'$; find a, c, F.
13. Given $a = 6.71$, $h = 6.60$; find A, C, c.
14. Given $c = 9$, $h = 20$; find A, C, a.
15. Given $c = 147$, $F = 2572.5$; find A, C, a, h.
16. Given $h = 16.8$, $F = 43.68$; find A, C, a, c.
17. Find the value of F in terms of a and c.
18. Find the value of F in terms of a and C.
19. Find the value of F in terms of a and A.
20. Find the value of F in terms of h and C.
21. A barn is 40 × 80 feet, the pitch of the roof is 45°; find the length of the rafters and the area of both sides of the roof.
22. In a unit circle what is the length of the chord corresponding to the angle 45° at the centre?
23. If the radius of a circle = 30, and the length of a chord = 44, find the angle at the centre.
24. Find the radius of a circle if a chord whose length is 5 subtends at the centre an angle of 133°.
25. What is the angle at the centre of a circle if the corresponding chord is equal to $\frac{2}{3}$ of the radius?
26. Find the area of a circular sector if the radius of the circle = 12, and the angle of the sector = 30°.

§ 18. THE REGULAR POLYGON.

Lines drawn from the centre of a regular polygon (Fig. 14) to the vertices are radii of the circumscribed circle; and lines drawn from the centre to the middle points of the sides are radii of the inscribed circle. These lines divide the polygon into equal right triangles. Therefore, a regular polygon is determined by a right triangle whose sides are the radius of the circumscribed circle, the radius of the inscribed circle, and half of one side of the polygon.

If the polygon has n sides, the angle of this right triangle at the centre is equal to

$$\frac{1}{2}\left(\frac{360^\circ}{n}\right) \text{ or } \frac{180^\circ}{n}.$$

If, also, a side of the polygon, or one of the above-mentioned radii, is given, this triangle may be solved, and the solution gives the unknown parts of the polygon.

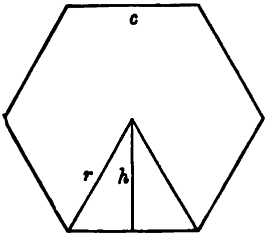

Fig. 14.

Let,

n = number of sides.
c = length of one side.
r = radius of circumscribed circle.
h = radius of inscribed circle.
p = the perimeter.
F = the area.

Then, by Geometry,

$$F = \tfrac{1}{2} hp.$$

EXERCISE VIII.

1. Given $n = 10$, $c = 1$; find r, h, F.
2. Given $n = 12$, $p = 70$; find r, h, F.
3. Given $n = 18$, $r = 1$; find h, p, F.
4. Given $n = 20$, $r = 20$; find h, c, F.
5. Given $n = 8$, $h = 1$; find r, c, F.
6. Given $n = 11$, $F = 20$; find r, h, c.
7. Given $n = 7$, $F = 7$; find r, h, p.

8. Find the side of a regular decagon inscribed in a unit circle.

9. Find the side of a regular decagon circumscribed about a unit circle.

10. If the side of an inscribed regular hexagon is equal to 1, find the side of an inscribed regular dodecagon.

11. Given n and c, and let b denote the side of the inscribed regular polygon having $2n$ sides; find b in terms of n and c.

12. Compute the difference between the areas of a regular octagon and a regular nonagon if the perimeter of each is 16.

13. Compute the difference between the perimeters of a regular pentagon and a regular hexagon if the area of each is 12.

14. From a square whose side is equal to 1 the corners are cut away so that a regular octagon is left. Find the area of this octagon.

15. Find the area of a regular pentagon if its diagonals are each equal to 12.

16. The area of an inscribed regular pentagon is 331.8; find the area of a regular polygon of 11 sides inscribed in the same circle.

17. The perimeter of an equilateral triangle is 20; find the area of the inscribed circle.

18. The area of a regular polygon of 16 sides, inscribed in a circle, is 100; find the area of a regular polygon of 15 sides, inscribed in the same circle.

19. A regular dodecagon is circumscribed about a circle, the circumference of which is equal to 1; find the perimeter of the dodecagon.

20. The area of a regular polygon of 25 sides is equal to 40; find the area of the ring comprised between the circumferences of the inscribed and the circumscribed circles.

CHAPTER III.

GONIOMETRY.

§ 21. DEFINITION OF GONIOMETRY.

IN order to prepare the way for the solution of an oblique triangle, we now proceed to extend the definitions of the trigonometric functions to angles of all magnitudes, and to deduce certain useful relations of the functions of different angles.

That branch of Trigonometry which treats of trigonometric functions in general, and of their relations, is called **Goniometry.**

§ 22. ANGLES OF ANY MAGNITUDE.

Let the radius OP of a circle (Fig. 16) generate an angle by turning about the centre O. This angle will be measured by the arc described by the point P; and it may have any magnitude, because the arc described by P may have any magnitude.

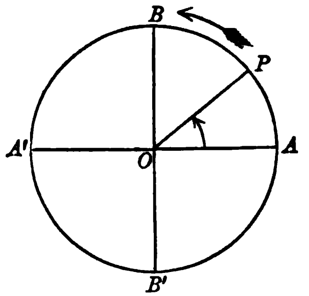

Fig. 16.

Let the horizontal line OA be the initial position of OP, and let OP revolve in the direction shown by the arrow, or opposite to the way clock-hands revolve. Let, also, the four quadrants into which the circle is divided by the horizontal and vertical diameters AA', BB', be numbered I., II., III., IV., in the direction of the motion.

During one revolution *OP* will form with *OA* all angles from 0° to 360°. Any particular angle is said to be an angle of the quadrant in which *OP* lies; so that,

Angles between 0° and 90° are angles of Quadrant I.
Angles between 90° and 180° are angles of Quadrant II.
Angles between 180° and 270° are angles of Quadrant III.
Angles between 270° and 360° are angles of Quadrant IV.

If *OP* make another revolution, it will describe all angles from 360° to 720°, and so on.

If *OP*, instead of making another revolution in the direction of the arrow, be supposed to revolve *backwards* about *O*, this backward motion tends to undo or cancel the original forward motion. Hence, the angle thus generated must be regarded as a *negative* angle; and this negative angle may obviously have any magnitude. Thus we arrive at the conception of an angle of any magnitude, positive or negative.

§ 23. GENERAL DEFINITIONS OF THE FUNCTIONS.

The definitions of the trigonometric functions may be extended to all angles, by making the functions of any angle equal to the line values in a unit circle drawn for the angle in question, as explained in § 3. *But the lines that represent the sine, cosine, tangent, and cotangent must be regarded as negative, if they are opposite in direction to the lines that represent the corresponding functions of an angle in the first quadrant; and the lines that represent the secant and cosecant must be regarded as negative, if they are opposite in direction to the moving radius.*

Figs. 17–20 show the functions drawn for an angle *AOP* in each quadrant taken in order. In constructing them, it must be remembered that the tangents to the circle are *always* drawn through *A* and *B*, *never* through *A′* or *B′*.

Let the angle *AOP* be denoted by x; then, in each figure the *absolute* values of the functions, that is, their values without regard to the signs + and —, are as follows:

$\sin x = MP$, $\tan x = AT$, $\sec x = OT$.
$\cos x = OM$, $\cot x = BS$, $\csc x = OS$.

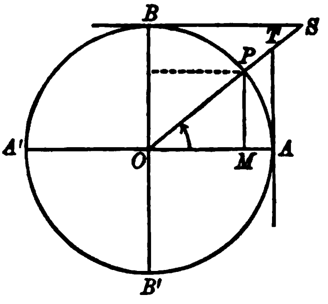

Fig. 17.

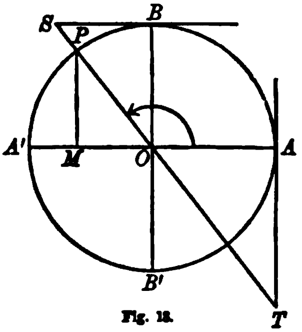

Fig. 18.

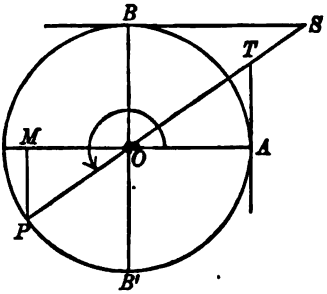

Fig. 19.

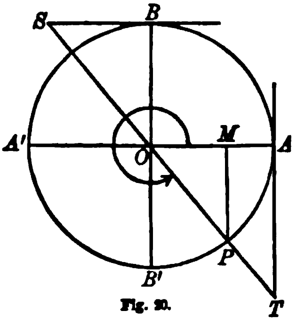

Fig. 20.

Keeping in mind the position of the points *A* and *B*, we may define in words the first four functions of the angle *x* thus:

$\sin x =$ the vertical projection of the moving radius;
$\cos x =$ the horizontal projection of the moving radius;
$\tan x =$ the distance measured along a tangent to the circle from the beginning of the first quadrant to the moving radius produced;
$\cot x =$ the distance measured along a tangent to the circle from the end of the first quadrant to the moving radius produced.

Sec *x* and csc *x* are the distances from the centre of the circle measured along the moving radius produced to the tangent and cotangent respectively.

§ 24. ALGEBRAIC SIGNS OF THE FUNCTIONS.

The lengths of the lines, defined above as the functions of any angle, are expressed numerically in terms of the radius of the circle as the unit. But, before these lengths can be treated as algebraic quantities, they must have the sign + or − prefixed, according to the condition stated in § 23.

The reason for this condition lies in that fundamental relation between algebraic and geometric magnitudes, in virtue of which *contrary signs in Algebra correspond to opposite directions in Geometry.*

The sine MP and the tangent AT always extend from the horizontal diameter, but sometimes *upwards* and sometimes *downwards;* the cosine OM and the cotangent BS always extend from the vertical diameter, but sometimes *towards the right* and sometimes *towards the left.* The functions of an angle in the first quadrant are assumed to be positive. Therefore,

1. Sines and tangents extending from the horizontal diameter *upwards*, are positive; *downwards*, negative.

2. Cosines and cotangents extending from the vertical diameter *towards the right*, are positive; *towards the left*, are negative.

The signs of the secant and cosecant are always made to agree with those of the cosine and sine respectively. This agreement is secured if secants and cosecants extending from the centre, *in the direction of the moving radius*, are considered positive; *in the opposite direction*, negative.

Hence, the signs of the functions for each quadrant are:

	I.	II.	III.	IV.
Sine and cosecant	+	+	−	−
Cosine and secant	+	−	−	+
Tangent and cotangent	+	−	+	−

§ 25. FUNCTIONS OF A VARIABLE ANGLE.

Let the angle x increase continuously from $0°$ to $360°$; what changes will the values of its functions undergo?

It is easy, by reference to Figs. 21–24, to trace these changes throughout all the quadrants.

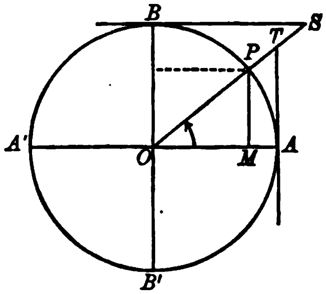

Fig. 21.

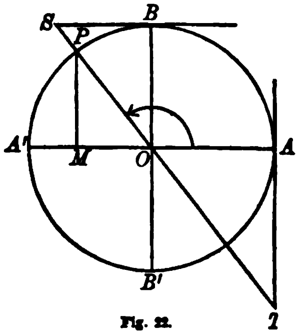

Fig. 22.

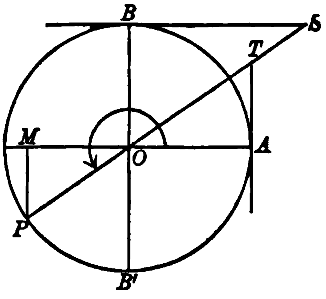

Fig. 23.

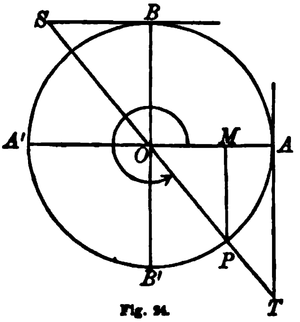

Fig. 24.

1. *The Sine.* In the first quadrant, the sine MP increases from 0 to 1; in the second, it remains positive, and decreases from 1 to 0; in the third, it is negative, and increases in absolute value from 0 to 1; in the fourth, it is negative, and decreases in absolute value from 1 to 0.

2. *The Cosine.* In the first quadrant, the cosine OM decreases from 1 to 0; in the second, it becomes negative and increases in absolute value from 0 to 1; in the third, it is negative and decreases in absolute value from 1 to 0; in the fourth, it is positive and increases from 0 to 1.

3. *The Tangent.* In the first quadrant, the tangent AT increases from 0 to ∞; in the second quadrant, as soon as the angle exceeds 90° by the smallest conceivable amount, the moving radius OP, prolonged in the direction opposite to that of OP, will cut AT at a point T situated very far *below* A; hence, the tangents of angles near 90° in the second quadrant have very large *negative* values. As the angle increases, the tangent AT continues negative but diminishes in absolute value. When $x = 180°$, then T coincides with A, and $\tan 180° = 0$. In the third quadrant, the tangent is positive and increases from 0 to ∞; in the fourth, it is negative and decreases in absolute value from ∞ to 0.

4. *The Cotangent.* In the first quadrant, the cotangent BS decreases from ∞ to 0; in the second quadrant, it is negative and increases in absolute value from 0 to ∞; in the third and fourth quadrants, it has the same sign, and undergoes the same changes as in the first and second quadrants respectively.

5. *The Secant.* In the first quadrant, the secant OT increases from 1 to ∞; in the second quadrant, it becomes negative (being measured in the direction opposite to that of OP), and decreases in absolute value from ∞ to 1, so that $\sec 180° = -1$; in the third quadrant, it continues negative, and increases in absolute value from 1 to ∞; in the fourth quadrant, it is positive, and decreases from ∞ to 1.

6. *The Cosecant.* In the first quadrant, the cosecant OS decreases from ∞ to 1; in the second quadrant, it remains positive, and increases from 1 to ∞; in the third quadrant, it becomes negative, and decreases in absolute value from ∞ to 1, so that $\csc 270° = -1$; in the fourth quadrant, it is negative, and increases in absolute value from 1 to ∞.

The limiting values of the functions are as follows:

	0°	90°	180°	270°	360°
Sine	± 0	1	± 0	− 1	± 0
Cosine	1	± 0	− 1	± 0	1
Tangent	± 0	± ∞	± 0	± ∞	± 0
Cotangent	± ∞	± 0	± ∞	± 0	± ∞
Secant	1	± ∞	− 1	± ∞	1
Cosecant	± ∞	1	± ∞	− 1	± ∞

Sines and cosines extend from +1 to −1; tangents and cotangents from +∞ to −∞; secants and cosecants from +∞ to +1, and from −1 to −∞.

In the table given above the double sign ± is placed before 0 and ∞. From the preceding investigation it appears that the functions *always change sign in passing through* 0 *and* ∞; and the sign + or − prefixed to 0 or ∞ simply shows the direction from which the value is reached.

Take, for example, tan 90°: The nearer an acute angle is to 90°, the greater the *positive* value of its tangent; and the nearer an obtuse angle is to 90°, the greater the *negative* value of its tangent. When the angle *is* 90°, OP (Fig. 21) is parallel to AT, and cannot meet it. But tan 90° may be regarded as extending either in the positive or in the negative direction; and according to the view taken, it will be + ∞ or − ∞.

§ 26. Functions of Angles Larger than 360°.

It is obvious that the functions of $360° + x$ are the same both in sign and in absolute value as those of x; for the moving radius has the same position in both cases. In general, if n denote any positive whole number,

The functions of $(n \times 360° + x)$ *are the same as those of* x.

For example: the functions of $2200°$ = the functions of $(6 \times 360° + 40°)$ = the functions of $40°$.

§ 27. EXTENSION OF FORMULAS [1]–[3] TO ALL ANGLES.

The Formulas established for *acute* angles in § 5 hold true for *all* angles. Thus, Formula [1],

$$\sin^2 x + \cos^2 x = 1,$$

is universally true; for, whether MP and OM (Figs. 21–24) are positive or negative, $\overline{MP}^2$ and $\overline{OM}^2$ are always positive, and in each quadrant $\overline{MP}^2 + \overline{OM}^2 = \overline{OP}^2 = 1$.

Also, Formulas

$$[2] \quad \tan x = \frac{\sin x}{\cos x},$$

and

$$[3] \begin{cases} \sin x \times \csc x = 1, \\ \cos x \times \sec x = 1, \\ \tan x \times \cot x = 1, \end{cases}$$

are universally true; for the algebraic signs of the functions, as given in the table at the end of § 24, agree with those in Formulas [2] and [3]; and with regard to the absolute values, we have in each quadrant from the similar triangles OMP, OAT, OBS, (Figs. 21–24) the proportions

$$\begin{aligned} AT &: OA = MP : OM, \\ MP &: OP = OB : OS, \\ OM &: OP = OA : OT, \\ AT &: OA = OB : BS, \end{aligned}$$

which, by substituting 1 for the radius, and the right names for the other lines, are easily reduced to the above formulas.

Formulas [1]–[3] enable us, from a given value of one function, to find the absolute values of the other five functions, and also the sign of the reciprocal function. But in order to determine the proper signs to be placed before the other four functions, we must know the quadrant to which the angle in question belongs; or what amounts to the same thing, the sign of any *one* of these four functions; for, by reference to the Table of Signs (§ 24) it will be seen that the signs of any two functions that are not reciprocals determine the quadrant to which the angle belongs.

Example. Given $\sin x = +\frac{4}{5}$, and $\tan x$ negative; find the values of the other functions.

Since $\sin x$ is positive, x must be an angle in Quadrant I. or in Quadrant II.; but, since also $\tan x$ is negative, Quadrant I. is inadmissable.

By [1], $\cos x = \pm\sqrt{1 - \frac{16}{25}} = \pm\frac{3}{5}$.

Since the angle is in Quadrant II. the minus sign must be taken, and we have

$$\cos x = -\tfrac{3}{5}.$$

By [2] and [3],

$$\tan x = -\tfrac{4}{3},\quad \cot x = -\tfrac{3}{4},\quad \sec x = -\tfrac{5}{3},\quad \csc x = \tfrac{5}{4}.$$

Exercise IX.

1. Construct the functions of an angle in Quadrant II. What are their signs?

2. Construct the functions of an angle in Quadrant III. What are their signs?

3. Construct the functions of an angle in Quadrant IV. What are their signs?

4. What are the signs of the functions of the following angles: 340°, 239°, 145°, 400°, 700°, 1200°, 3800°?

5. How many angles less than 360° have the value of the sine equal to $+\frac{5}{7}$, and in what quadrants do they lie?

6. How many values less than 720° can the angle x have if $\cos x = +\frac{2}{3}$, and in what quadrants do they lie?

7. If we take into account only angles less than 180°, how many values can x have if $\sin x = \frac{4}{7}$? if $\cos x = \frac{1}{5}$? if $\cos x = -\frac{4}{5}$? if $\tan x = \frac{2}{3}$? if $\cot x = -7$?

8. Within what limits must the angle x lie if $\cos x = -\frac{2}{3}$? if $\cot x = 4$? if $\sec x = 80$? if $\csc x = -3$? (x to be less than 360°.)

9. In what quadrant does an angle lie if sine and cosine are both negative? if cosine and tangent are both negative? if the cotangent is positive and the sine negative?

10. Between 0° and 3600° how many angles are there whose sines have the absolute value $\frac{3}{5}$? Of these sines how many are positive and how many negative?

11. In finding $\cos x$ by means of the equation $\cos x = \pm\sqrt{1-\sin^2 x}$, when must we choose the positive sign and when the negative sign?

12. Given $\cos x = -\sqrt{\frac{1}{2}}$; find the other functions when x is an angle in Quadrant II.

13. Given $\tan x = \sqrt{3}$; find the other functions when x is an angle in Quadrant III.

14. Given $\sec x = +7$, and $\tan x$ negative; find the other functions of x.

15. Given $\cot x = -3$; find all the possible values of the other functions.

16. What functions of an angle of a triangle may be negative? In what case are they negative?

17. What functions of an angle of a triangle determine the angle, and what functions fail to do so?

18. Why may $\cot 360°$ be considered equal either to $+\infty$ or to $-\infty$?

19. Obtain by means of Formulas [1]–[3] the other functions of the angles given:

(i.) $\tan 90° = \infty$. (iii.) $\cot 270° = 0$.
(ii.) $\cos 180° = -1$. (iv.) $\csc 360° = -\infty$.

20. Find the values of $\sin 450°$, $\tan 540°$, $\cos 630°$, $\cot 720°$, $\sin 810°$, $\csc 900°$.

21. For what angle in each quadrant are the absolute values of the sine and cosine alike?

Compute the values of the following expressions:

22. $a \sin 0° + b \cos 90° - c \tan 180°$.

23. $a \cos 90° - b \tan 180° + c \cot 90°$.

24. $a \sin 90° - b \cos 360° + (a-b) \cos 180°$.

25. $(a^2 - b^2) \cos 360° - 4ab \sin 270°$.

§ 28. REDUCTION OF FUNCTIONS TO THE FIRST QUADRANT.

In a unit circle (Fig. 25) draw two diameters PR and QS equally inclined to the horizontal diameter AA', or so that the angles AOP, $A'OQ$, $A'OR$, and AOS shall be equal. From the points P, Q, R, S let fall perpendiculars to AA'; the four right triangles thus formed, with a common vertex at O, are equal; because they have equal hypotenuses (radii of the circle) and equal acute angles at O. Therefore, the perpendiculars PM, QN, RN, SM, are equal. Now these four lines are the sines of the angles AOP, AOQ, AOR, and AOS, respectively. Therefore, *in absolute value*,

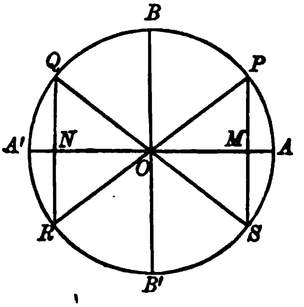

Fig. 25.

$$\sin AOP = \sin AOQ = \sin AOR = \sin AOS.$$

And from § 27 it follows that *in absolute value* the cosines of these angles are also equal; and likewise the tangents, the cotangents, the secants, and the cosecants.*

Hence, *for every acute angle* (AOP) *there is an angle in each of the higher quadrants whose functions, in absolute value, are equal to those of this acute angle.*

Let $\angle AOP = x$, $\angle POB = y$; then $x + y = 90°$, and the functions of x are equal to the co-named functions of y (§ 4); further,

$$\angle AOQ \text{ (in Quadrant II.)} = 180° - x = 90° + y,$$
$$\angle AOR \text{ (in Quadrant III.)} = 180° + x = 270° - y,$$
$$\angle AOS \text{ (in Quadrant IV.)} = 360° - x = 270° + y.$$

Hence, if we prefix in each case the proper sign (§ 24), we have the two following series of Formulas:

---

* In future, secants and cosecants will be disregarded. They may be found by [3] if wanted, but are seldom used in computations.

Angle in Quadrant II.

$$\sin(180^\circ - x) = \sin x. \qquad \sin(90^\circ + y) = \cos y.$$
$$\cos(180^\circ - x) = -\cos x. \qquad \cos(90^\circ + y) = -\sin y.$$
$$\tan(180^\circ - x) = -\tan x. \qquad \tan(90^\circ + y) = -\cot y.$$
$$\cot(180^\circ - x) = -\cot x. \qquad \cot(90^\circ + y) = -\tan y.$$

Angle in Quadrant III.

$$\sin(180^\circ + x) = -\sin x. \qquad \sin(270^\circ - y) = -\cos y.$$
$$\cos(180^\circ + x) = -\cos x. \qquad \cos(270^\circ - y) = -\sin y.$$
$$\tan(180^\circ + x) = \tan x. \qquad \tan(270^\circ - y) = \cot y.$$
$$\cot(180^\circ + x) = \cot x. \qquad \cot(270^\circ - y) = \tan y.$$

Angle in Quadrant IV.

$$\sin(360^\circ - x) = -\sin x. \qquad \sin(270^\circ + y) = -\cos y.$$
$$\cos(360^\circ - x) = \cos x. \qquad \cos(270^\circ + y) = \sin y.$$
$$\tan(360^\circ - x) = -\tan x. \qquad \tan(270^\circ + y) = -\cot y.$$
$$\cot(360^\circ - x) = -\cot x. \qquad \cot(270^\circ + y) = -\tan y.$$

Hence, by selecting the right formulas,

The functions of all angles can be reduced to the functions of angles not greater than 45°. Thus, to find the functions of 220° and 230°, we should consider 220° as (180° + 40°), but 230° as (270° − 40°).

It is evident from these formulas that,

If an acute angle be added to or subtracted from **180° or 360°**, *the functions of the resulting angle are equal in absolute value to the* **like-named** *functions of the acute angle; but if an acute angle be added to or subtracted from* **90° or 270°**, *the functions of the resulting angle are equal in absolute value to the* **co-named** *functions of the acute angle.*

It is evident from the formulas for $(180^\circ - x)$ that,

A given value of a sine determines two supplementary angles, one acute, the other obtuse; a given value of any other function (except the cosecant) determines only one angle: acute if the value is positive, obtuse if the value is negative.

§ 29. ANGLES WHOSE DIFFERENCE IS 90°.

The general form of two such angles is x and $90° + x$, and they must lie in adjoining quadrants. The relations between their functions were found in § 28, but only for the case when x is acute. These relations, however, may be shown to hold true for all values of x.

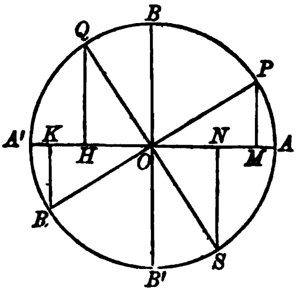

Fig. 26.

In a unit circle (Fig. 26) draw two diameters PR and QS perpendicular to each other, and let fall to AA' the perpendiculars PM, QH, RK, and SN. The right triangles OMP, OHQ, OKR, and ONS are equal, because they have equal hypotenuses and equal acute angles POM, OQH, ROK, and OSN.

Therefore, $OM = QH = OK = NS$,
and $PM = OH = KR = ON$.

Hence, taking also into account the algebraic sign,

$$\begin{aligned}
\sin AOQ &= \cos AOP; & \sin AOS &= \cos AOR;\\
\cos AOQ &= -\sin AOP; & \cos AOS &= -\sin AOR;\\
\sin AOR &= \cos AOQ; & \sin(360° + AOP) &= \cos AOS;\\
\cos AOR &= -\sin AOQ; & \cos(360° + AOP) &= -\sin AOS.
\end{aligned}$$

In all these equations, if x denote the angle on the right-hand side, the angle on the left-hand side will be $90° + x$. Therefore, if x be an angle in any one of the four quadrants,

$$\sin(90° + x) = \cos x,$$
$$\cos(90° + x) = -\sin x.$$

And, by § 27,

$$\tan(90° + x) = -\cot x,$$
$$\cot(90° + x) = -\tan x.$$

In like manner, it can be shown that all the formulas of § 28 hold true, whatever be the value of the angle x.

§ 30. FUNCTIONS OF A NEGATIVE ANGLE.

If the angle AOP (Fig. 25) is denoted by x, the equal angle AOS, generated by a *backward* rotation of the moving radius from the initial position OA, will be denoted by $-x$. It is obvious that the position OS of the moving radius for this angle is identical with its position for the angle $360° - x$. Therefore, the functions of the angle $-x$ are the same as those of the angle $360° - x$; or (§ 28),

$$\sin(-x) = -\sin x, \qquad \tan(-x) = -\tan x,$$
$$\cos(-x) = \cos x, \qquad \cot(-x) = -\cot x.$$

EXERCISE X.

1. Express $\sin 250°$ in terms of the functions of an acute angle greater than 45°, and also in terms of the functions of an acute angle less than 45°.

Ans. 1. $\sin 250° = \sin(180° + 70°) = -\sin 70°$.
2. $\sin 250° = \sin(270° - 20°) = -\cos 20°$.

Express the following functions in terms of the functions of angles less than 45°:

2. $\sin 172°$.
3. $\cos 100°$.
4. $\tan 125°$.
5. $\cot\ 91°$.
6. $\sec 110°$.
7. $\csc 157°$.
8. $\sin 204°$.
9. $\cos 359°$.
10. $\tan 300°$.
11. $\cot 264°$.
12. $\sec 244°$.
13. $\csc 271°$.
14. $\sin 163° 49'$.
15. $\cos 195° 33'$.
16. $\tan 269° 15'$.
17. $\cot 139° 17'$.
18. $\sec 299° 45'$.
19. $\csc\ 92° 25'$.

Express all the functions of the following negative angles in terms of those of positive angles less than 45°:

20. $-75°$.
21. $-127°$.
22. $-200°$.
23. $-345°$.
24. $-52° 37'$.
25. $-196° 54'$.

26. Find the functions of 120°.

HINT. $120° = 180° - 60°$, or, $120° = 90° + 30°$; then apply § 28.

Find the functions of the following angles:

27. 135°. 29. 210°. 31. 240°. 33. -30°.

28. 150°. 30. 225°. 32. 300°. 34. -225°.

35. Given $\sin x = -\sqrt{\frac{1}{2}}$, and $\cos x$ negative; find the other functions of x, and the value of x.

36. Given $\cot x = -\sqrt{3}$, and x in Quadrant II.; find the other functions of x, and the value of x.

37. Find the functions of 3540°.

38. What angles less than 360° have a sine equal to $-\frac{1}{2}$? a tangent equal to $-\sqrt{3}$?

39. Which of the angles mentioned in Examples 27–34 have a cosine equal to $-\sqrt{\frac{1}{2}}$? a cotangent equal to $-\sqrt{3}$?

40. What values of x between 0° and 720° will satisfy the equation $\sin x = +\frac{1}{2}$?

41. In each of the following cases find the other angle between 0° and 360° for which the corresponding function (sign included) has the same value: $\sin 12^\circ$, $\cos 26^\circ$, $\tan 45^\circ$, $\cot 72^\circ$; $\sin 191^\circ$, $\cos 120^\circ$, $\tan 244^\circ$, $\cot 357^\circ$.

42. Given $\tan 238^\circ = 1.6$; find $\sin 122^\circ$.

43. Given $\cos 333^\circ = 0.89$; find $\tan 117^\circ$.

Simplify the following expressions:

44. $a \cos(90^\circ - x) + b \cos(90^\circ + x)$.

45. $m \cos(90^\circ - x) \sin(90^\circ - x)$.

46. $(a - b) \tan(90^\circ - x) + (a + b) \cot(90^\circ + x)$.

47. $a^2 + b^2 - 2ab \cos(180^\circ - x)$.

48. $\sin(90^\circ + x) \sin(180^\circ + x) + \cos(90^\circ + x) \cos(180^\circ - x)$.

49. $\cos(180^\circ + x) \cos(270^\circ - y) - \sin(180^\circ + x) \sin(270^\circ - y)$.

50. $\tan x + \tan(-y) - \tan(180^\circ - y)$.

51. For what values of x is the expression $\sin x + \cos x$ positive, and for what values negative? Represent the result by a drawing in which the sectors corresponding to the negative values are shaded.

52. Answer the question of last example for $\sin x - \cos x$.

53. Find the functions of $(x - 90^\circ)$ in terms of the functions of x.

54. Find the functions of $(x - 180^\circ)$ in terms of the functions of x.

§ 31. Functions of the Sum of Two Angles.

In a unit circle (Fig. 27) let the angle $AOB = x$, the angle $BOC = y$; then the angle $AOC = x + y$.

In order to express $\sin(x+y)$ and $\cos(x+y)$ in terms of the sines and cosines of x and y, draw $CF \perp OA$, $CD \perp OB$, $DE \perp OA$, $DG \perp CF$; then $CD = \sin y$, $OD = \cos y$, and the angle $DCG =$ the angle $GDO = x$. Also,

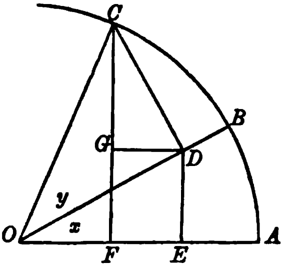

Fig. 27.

$$\sin(x+y) = CF = DE + CG.$$

$$\frac{DE}{OD} = \sin x; \quad \text{hence, } DE = \sin x \times OD = \sin x \cos y.$$

$$\frac{CG}{CD} = \cos x; \quad \text{hence, } CG = \cos x \times CD = \cos x \sin y.$$

Therefore, $\boldsymbol{\sin(x+y) = \sin x \cos y + \cos x \sin y}$. [4]

Again, $\cos(x+y) = OF = OE - DG$.

$$\frac{OE}{OD} = \cos x; \quad \text{hence, } OE = \cos x \times OD = \cos x \cos y.$$

$$\frac{DG}{CD} = \sin x; \quad \text{hence, } DG = \sin x \times CD = \sin x \sin y.$$

Therefore, $\boldsymbol{\cos(x+y) = \cos x \cos y - \sin x \sin y}$. [5]

In this proof x and y, and also the sum $x+y$, are assumed to be acute angles. If the sum $x+y$ of the acute angles x and y is obtuse, as in Fig. 28, the proof remains, word for word, the same as above, the only difference being that the sign of OF will be negative, as DG is now greater than OE. The above formulas, therefore, hold true for all acute angles x and y.

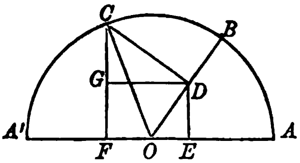

Fig. 28.

If these formulas hold true for any two acute angles x and y, they hold true when one of the angles is increased by 90°. Thus, if for x we write $x' = 90° + x$, then, by § 29,

$$\begin{aligned}\sin(x'+y) &= \sin(90°+x+y) = \cos(x+y),\\ \cos(x'+y) &= \cos(90°+x+y) = -\sin(x+y).\end{aligned}$$

Hence, by [5], $\sin(x'+y) = \cos x \cos y - \sin x \sin y$,
by [4], $\cos(x'+y) = -\sin x \cos y - \cos x \sin y$.

Now, by § 29, $\cos x = \sin(90°+x) = \sin x'$,
$\sin x = -\cos(90°+x) = -\cos x'$.

Therefore, by putting $\sin x'$ for $\cos x$, and $-\cos x'$ for $\sin x$, in the right-hand members of the above equations,

$$\begin{aligned}\sin(x'+y) &= \sin x' \cos y + \cos x' \sin y,\\ \cos(x'+y) &= \cos x' \cos y - \sin x' \sin y.\end{aligned}$$

Hence, it follows that Formulas [4] and [5] are universally true. For they have been proved true for any two acute angles, and also true when one of these angles is increased by 90°; hence they are true for each repeated increase of one or the other angle by 90°, and therefore true for the sum of any two angles whatever.

By § 27,

$$\tan(x+y) = \frac{\sin(x+y)}{\cos(x+y)} = \frac{\sin x \cos y + \cos x \sin y}{\cos x \cos y - \sin x \sin y}.$$

If we divide each term of the numerator and denominator of the last fraction by $\cos x \cos y$, and again apply § 27, we obtain

$$\mathbf{\tan(x+y) = \frac{\tan x + \tan y}{1 - \tan x \tan y}.} \qquad [6]$$

In like manner, by dividing each term of the numerator and denominator of the value of $\cot(x+y)$ by $\sin x \sin y$, we obtain

$$\mathbf{\cot(x+y) = \frac{\cot x \cot y - 1}{\cot x + \cot y}.} \qquad [7]$$

§ 32. FUNCTIONS OF THE DIFFERENCE OF TWO ANGLES.

In a unit circle (Fig. 29) let the angle $AOB = x$, the angle $COB = y$; then the angle $AOC = x - y$.

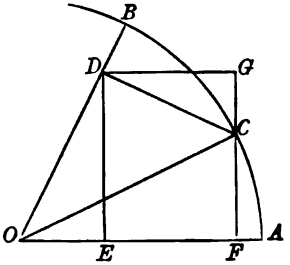

Fig. 29.

In order to express $\sin(x-y)$ and $\cos(x-y)$ in terms of the sines and cosines of x and y, draw $CF \perp OA$, $CD \perp OB$, $DE \perp OA$, $DG \perp FC$ prolonged; then $CD = \sin y$, $OD = \cos y$, and the angle $DCG =$ the angle $EDC = x$. And, $\sin(x-y) = CF = DE - CG$.

$$\frac{DE}{OD} = \sin x; \quad \text{hence, } DE = \sin x \times OD = \sin x \cos y.$$

$$\frac{CG}{CD} = \cos x; \quad \text{hence, } CG = \cos x \times CD = \cos x \sin y.$$

Therefore, $\mathbf{\sin(x-y) = \sin x \cos y - \cos x \sin y}$. [8]

Again, $\cos(x-y) = OF = OE + DG$.

$$\frac{OE}{OD} = \cos x; \quad \text{hence, } OE = \cos x \times OD = \cos x \cos y.$$

$$\frac{DG}{CD} = \sin x; \quad \text{hence, } DG = \sin x \times CD = \sin x \sin y.$$

Therefore, $\mathbf{\cos(x-y) = \cos x \cos y + \sin x \sin y}$. [9]

In this proof, both x and y are assumed to be acute angles; but, whatever be the values of x and y, the same method of proof will always lead to Formulas [8] and [9], when due regard is paid to the algebraic signs.

The general application of these formulas may be at once shown by deducing them from the general formulas established in § 31, as follows:

It is obvious that $(x-y)+y = x$. If we apply Formulas [4] and [5] to $(x-y)+y$, then

$$\sin\{(x-y)+y\} \text{ or } \sin x = \sin(x-y)\cos y + \cos(x-y)\sin y,$$
$$\cos\{(x-y)+y\} \text{ or } \cos x = \cos(x-y)\cos y - \sin(x-y)\sin y.$$

Multiply the first equation by $\cos y$, the second by $\sin y$,

$$\sin x\cos y = \sin(x-y)\cos^2 y + \cos(x-y)\sin y\cos y,$$
$$\cos x\sin y = -\sin(x-y)\sin^2 y + \cos(x-y)\sin y\cos y;$$

whence, by subtraction,

$$\sin x\cos y - \cos x\sin y = \sin(x-y)(\sin^2 y + \cos^2 y).$$

But $\sin^2 y + \cos^2 y = 1$; therefore, by transposing,
$$\sin(x-y) = \sin x\cos y - \cos x\sin y.$$

Again, if we multiply the first equation by $\sin y$, the second equation by $\cos y$, and add the results, we obtain, by reducing,

$$\cos(x-y) = \cos x\cos y + \sin x\sin y.$$

Therefore, Formulas [8] and [9], like [4] and [5], from which they have been derived, are universally true.

From [8] and [9], by proceeding as in § 31, we obtain

$$\tan(x-y) = \frac{\tan x - \tan y}{1 + \tan x\tan y}. \qquad [10]$$

$$\cot(x-y) = \frac{\cot x\cot y + 1}{\cot y - \cot x}. \qquad [11]$$

Formulas [4]–[11] may be combined as follows:

$$\sin(x \pm y) = \sin x\cos y \pm \cos x\sin y,$$

$$\cos(x \pm y) = \cos x\cos y \mp \sin x\sin y,$$

$$\tan(x \pm y) = \frac{\tan x \pm \tan y}{1 \mp \tan x\tan y},$$

$$\cot(x \pm y) = \frac{\cot x\cot y \mp 1}{\cot y \pm \cot x}.$$

§ 33. FUNCTIONS OF TWICE AN ANGLE.

If, in Formulas [4]-[7], $y = x$, they become:

$$\sin 2x = 2 \sin x \cos x. \quad [12] \qquad \cos 2x = \cos^2 x - \sin^2 x. \quad [13]$$

$$\tan 2x = \frac{2 \tan x}{1 - \tan^2 x}. \quad [14] \qquad \cot 2x = \frac{\cot^2 x - 1}{2 \cot x}. \quad [15]$$

By these formulas the functions of twice an angle are found when the functions of the angle are given.

§ 34. FUNCTIONS OF HALF AN ANGLE.

Take the formulas

$$\cos^2 x + \sin^2 x = 1 \quad [1]$$

$$\cos^2 x - \sin^2 x = \cos 2x \quad [13]$$

Subtract, $2 \sin^2 x = 1 - \cos 2x$

Add, $2 \cos^2 x = 1 + \cos 2x$

Whence

$$\sin x = \pm \sqrt{\frac{1 - \cos 2x}{2}}, \qquad \cos x = \pm \sqrt{\frac{1 + \cos 2x}{2}}.$$

These values, if z is put for $2x$, and hence $\frac{1}{2}z$ for x, become

$$\sin \tfrac{1}{2} z = \pm \sqrt{\frac{1 - \cos z}{2}}. \quad [16] \qquad \cos \tfrac{1}{2} z = \pm \sqrt{\frac{1 + \cos z}{2}}. \quad [17]$$

Hence, by division (§ 27),

$$\tan \tfrac{1}{2} z = \pm \sqrt{\frac{1 - \cos z}{1 + \cos z}}. \quad [18] \qquad \cot \tfrac{1}{2} z = \pm \sqrt{\frac{1 + \cos z}{1 - \cos z}}. \quad [19]$$

By these formulas the functions of half an angle may be computed when the cosine of the entire angle is given.

The proper sign to be placed before the root in each case depends on the quadrant in which the angle $\frac{1}{2}z$ lies. (§ 24.)

Let the student show from Formula [18] that

$$\tan \tfrac{1}{2} B = \sqrt{\frac{c - a}{c + a}}. \quad \text{(See page 19, Note 2.)}$$

§ 35. Sums and Differences of Functions.

From [4], [5], [8], and [9], by addition and subtraction:

$$\begin{aligned}\sin(x+y)+\sin(x-y) &= 2\sin x\cos y,\\ \sin(x+y)-\sin(x-y) &= 2\cos x\sin y,\\ \cos(x+y)+\cos(x-y) &= 2\cos x\cos y,\\ \cos(x+y)-\cos(x-y) &= -2\sin x\sin y;\end{aligned}$$

or, by making $x+y=A$, and $x-y=B$,

and therefore, $x=\frac{1}{2}(A+B)$, and $y=\frac{1}{2}(A-B)$,

$$\mathbf{\sin A+\sin B = 2\sin\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}(A-B).} \quad [20]$$

$$\mathbf{\sin A-\sin B = 2\cos\tfrac{1}{2}(A+B)\sin\tfrac{1}{2}(A-B).} \quad [21]$$

$$\mathbf{\cos A+\cos B = 2\cos\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}(A-B).} \quad [22]$$

$$\mathbf{\cos A-\cos B = -2\sin\tfrac{1}{2}(A+B)\sin\tfrac{1}{2}(A-B).} \quad [23]$$

From [20] and [21], by division, we obtain

$$\frac{\sin A+\sin B}{\sin A-\sin B}=\tan\tfrac{1}{2}(A+B)\cot\tfrac{1}{2}(A-B);$$

or, since $\cot\frac{1}{2}(A-B)=\dfrac{1}{\tan\frac{1}{2}(A-B)}$,

$$\mathbf{\frac{\sin A+\sin B}{\sin A-\sin B}=\frac{\tan\frac{1}{2}(A+B)}{\tan\frac{1}{2}(A-B)}.} \quad [24]$$

Exercise XI.

1. Find the value of $\sin(x+y)$ and $\cos(x+y)$, when $\sin x=\frac{3}{5}$, $\cos x=\frac{4}{5}$, $\sin y=\frac{5}{13}$, $\cos y=\frac{12}{13}$.

2. Find $\sin(90°-y)$ and $\cos(90°-y)$ by making $x=90°$ in Formulas [8] and [9].

Find, by Formulas [4]–[11], the first four functions of:

3. $90°+y$.
4. $180°-y$.
5. $180°+y$.
6. $270°-y$.
7. $270°+y$.
8. $360°-y$.
9. $360°+y$.
10. $x-90°$.
11. $x-180°$.
12. $x-270°$.
13. $-y$.
14. $45°-y$.
15. $45°+y$.
16. $30°+y$.
17. $60°-y$.

18. Find $\sin 3x$ in terms of $\sin x$.
19. Find $\cos 3x$ in terms of $\cos x$.
20. Given $\tan \frac{1}{2}x = 1$; find $\cos x$.
21. Given $\cot \frac{1}{2}x = \sqrt{3}$; find $\sin x$.
22. Given $\sin x = 0.2$; find $\sin \frac{1}{2}x$ and $\cos \frac{1}{2}x$.
23. Given $\cos x = 0.5$; find $\cos 2x$ and $\tan 2x$.
24. Given $\tan 45^\circ = 1$; find the functions of $22^\circ\, 30'$.
25. Given $\sin 30^\circ = 0.5$; find the functions of 15°.
26. Prove that $\tan 18^\circ = \dfrac{\sin 33^\circ + \sin 3^\circ}{\cos 33^\circ + \cos 3^\circ}$.

Prove the following formulas:

27. $\sin 2x = \dfrac{2 \tan x}{1 + \tan^2 x}$.
28. $\cos 2x = \dfrac{1 - \tan^2 x}{1 + \tan^2 x}$.
29. $\tan \frac{1}{2}x = \dfrac{\sin x}{1 + \cos x}$.
30. $\cot \frac{1}{2}x = \dfrac{\sin x}{1 - \cos x}$.
31. $\sin \frac{1}{2}x \pm \cos \frac{1}{2}x = \sqrt{1 \pm \sin x}$.
32. $\dfrac{\tan x \pm \tan y}{\cot x \pm \cot y} = \pm \tan x \tan y$.
33. $\tan(45^\circ - x) = \dfrac{1 - \tan x}{1 + \tan x}$.

If A, B, C are the angles of a triangle, prove that:

34. $\sin A + \sin B + \sin C = 4 \cos \frac{1}{2}A \cos \frac{1}{2}B \cos \frac{1}{2}C$.
35. $\cos A + \cos B + \cos C = 1 + 4 \sin \frac{1}{2}A \sin \frac{1}{2}B \sin \frac{1}{2}C$.
36. $\tan A + \tan B + \tan C = \tan A \times \tan B \times \tan C$.
37. $\cot \frac{1}{2}A + \cot \frac{1}{2}B + \cot \frac{1}{2}C = \cot \frac{1}{2}A \times \cot \frac{1}{2}B \times \cot \frac{1}{2}C$.

Change to forms more convenient for logarithmic computation:

38. $\cot x + \tan x$.
39. $\cot x - \tan x$.
40. $\cot x + \tan y$.
41. $\cot x - \tan y$.
42. $\dfrac{1 - \cos 2x}{1 + \cos 2x}$.
43. $1 + \tan x \tan y$.
44. $1 - \tan x \tan y$.
45. $\cot x \cot y + 1$.
46. $\cot x \cot y - 1$.
47. $\dfrac{\tan x + \tan y}{\cot x + \cot y}$.

CHAPTER IV.

THE OBLIQUE TRIANGLE.

§ 36. LAW OF SINES.

Let A, B, C denote the angles of a triangle ABC (Figs. 30 and 31), and a, b, c, respectively, the lengths of the opposite sides.

Draw $CD \perp AB$, and meeting AB (Fig. 30) or AB produced (Fig. 31) at D. Let $CD = h$.

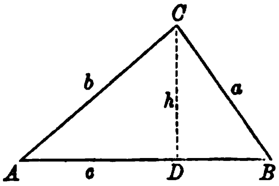

Fig. 30.

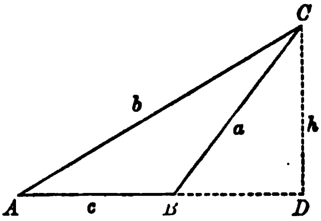

Fig. 31.

In both figures, $\frac{h}{b} = \sin A$.

In Fig. 30, $\frac{h}{a} = \sin B$.

In Fig. 31, $\frac{h}{a} = \sin (180° - B) = \sin B$.

Therefore, whether h lies within or without the triangle, we obtain, by division,

$$\frac{\mathbf{a}}{\mathbf{b}} = \frac{\mathbf{\sin A}}{\mathbf{\sin B}}. \qquad [25]$$

By drawing perpendiculars from the vertices A and B to the opposite sides we may obtain, in the same way,

$$\frac{b}{c}=\frac{\sin B}{\sin C}, \qquad \frac{a}{c}=\frac{\sin A}{\sin C}.$$

Hence the Law of Sines, which may be thus stated:

The sides of a triangle are proportional to the sines of the opposite angles.

If we regard these three equations as proportions, and take them by alternation, it will be evident that they may be written in the symmetrical form,

$$\frac{a}{\sin A}=\frac{b}{\sin B}=\frac{c}{\sin C}.$$

Each of these equal ratios has a simple geometrical meaning which will appear if the Law of Sines is proved as follows:

Circumscribe a circle about the triangle ABC (Fig. 32), and draw the radii OA, OB, OC; these radii divide the triangle into three isosceles triangles. Let R denote the radius. Draw $OM \perp BC$. By Geometry, the angle $BOC = 2A$; hence, the angle $BOM = A$, then $BM = R \sin BOM = R \sin A$.

$\therefore BC$ or $a = 2R \sin A$.

In like manner, $b = 2R \sin B$, and $c = 2R \sin C$. Whence we obtain

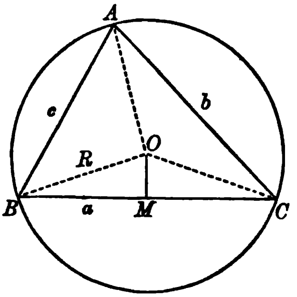

Fig. 32.

$$2R=\frac{a}{\sin A}=\frac{b}{\sin B}=\frac{c}{\sin C}.$$

That is: *The ratio of any side of a triangle to the sine of the opposite angle is numerically equal to the diameter of the circumscribed circle.*

§ 37. LAW OF COSINES.

This law gives the value of one side of a triangle in terms of the other two sides and the angle included between them.

In Figs. 30 and 31, $a^2 = h^2 + BD^2$.

In Fig. 30, $BD = c - AD$;

in Fig. 31, $BD = AD - c$;

in both cases, $BD^2 = AD^2 - 2c \times AD + c^2$.

Therefore, in all cases, $a^2 = h^2 + AD^2 + c^2 - 2c \times AD$.

Now, $h^2 + AD^2 = b^2$,

and $AD = b \cos A$.

Therefore, $$\mathbf{a^2 = b^2 + c^2 - 2bc \cos A.} \qquad [26]$$

In like manner, it may be proved that

$$b^2 = a^2 + c^2 - 2ac \cos B,$$
$$c^2 = a^2 + b^2 - 2ab \cos C.$$

The three formulas have precisely the same form, and the law may be stated as follows:

The square of any side of a triangle is equal to the sum of the squares of the other two sides, diminished by twice the product of the sides and the cosine of the included angle.

§ 38. LAW OF TANGENTS.

By § 36, $a : b = \sin A : \sin B$;

whence, by the Theory of Proportion,

$$\frac{a-b}{a+b} = \frac{\sin A - \sin B}{\sin A + \sin B}.$$

But by [24], page 48,

$$\frac{\sin A - \sin B}{\sin A + \sin B} = \frac{\tan \frac{1}{2}(A - B)}{\tan \frac{1}{2}(A + B)}.$$

Therefore,

$$\mathbf{\frac{a-b}{a+b} = \frac{\tan \frac{1}{2}(A - B)}{\tan \frac{1}{2}(A + B)}.} \qquad [27]$$

By merely changing the letters,

$$\frac{a-c}{a+c}=\frac{\tan\frac{1}{2}(A-C)}{\tan\frac{1}{2}(A+C)},\quad \frac{b-c}{b+c}=\frac{\tan\frac{1}{2}(B-C)}{\tan\frac{1}{2}(B+C)}.$$

Hence the Law of Tangents:

The difference of two sides of a triangle is to their sum as the tangent of half the difference of the opposite angles is to the tangent of half their sum.

NOTE. If in [27] $b>a$, then $B>A$. The formula is still true, but to avoid negative quantities, the formula in this case should be written

$$\frac{b-a}{b+a}=\frac{\tan\frac{1}{2}(B-A)}{\tan\frac{1}{2}(B+A)}.$$

EXERCISE XII.

1. What do the formulas of § 36 become when one of the angles is a right angle?

2. Prove by means of the Law of Sines that the bisector of an angle of a triangle divides the opposite side into parts proportional to the adjacent sides.

3. What does Formula [26] become when $A=90°$? when $A=0°$? when $A=180°$? What does the triangle become in each of these cases?

NOTE. The case where $A=90°$ explains why the theorem of § 37 is sometimes termed the *Generalized Theorem of Pythagoras.*

4. Prove (Figs. 30 and 31) that whether the angle B is acute or obtuse $c=a\cos B+b\cos A$. What are the two symmetrical formulas obtained by changing the letters? What does the formula become when $B=90°$?

5. From the three following equations (found in the last exercise) prove the theorem of § 37:

$$\begin{aligned} c&=a\cos B+b\cos A,\\ b&=a\cos C+c\cos A,\\ a&=b\cos C+c\cos B. \end{aligned}$$

HINT. Multiply the first equation by c, the second by b, the third by a; then from the first subtract the *sum* of the second and third.

6. In Formula [27] what is the maximum value of $\frac{1}{2}(A-B)$? of $\frac{1}{2}(A+B)$?

7. Find the form to which Formula [27] reduces, and describe the nature of the triangle, when

(i.) $C=90°$; (ii.) $A-B=90°$, and $B=C$.

§ 39. The Given Parts of an Oblique Triangle.

The formulas established in §§ 36–38, together with the equation $A+B+C=180°$, are sufficient for solving every case of an oblique triangle. The three parts that determine an oblique triangle may be:

I. One side and two angles;
II. Two sides and the angle opposite to one of these sides;
III. Two sides and the included angle;
IV. The three sides.

In all cases let A, B, C denote the angles, a, b, c the sides opposite these angles respectively.

§ 40. Case I.

Given one side a, and two angles A and B; find the remaining parts C, b, and c.

1. $C=180°-(A+B)$.

2. $\frac{b}{a}=\frac{\sin B}{\sin A}$; $\therefore b=\frac{a \sin B}{\sin A}=\frac{a}{\sin A}\times \sin B$.

3. $\frac{c}{a}=\frac{\sin C}{\sin A}$; $\therefore c=\frac{a \sin C}{\sin A}=\frac{a}{\sin A}\times \sin C$.

Example. $a=24.31$, $A=45° 18'$, $B=22° 11'$.

The work may be arranged as follows:

$a=24.31$	$\log a=1.38578$	$=1.38578$
$A=45° 18'$	$\text{colog} \sin A=0.14825$	$=0.14825$
$B=\underline{22° 11'}$	$\log \sin B=\underline{9.57700}$	$\log \sin C=\underline{9.96556}$
$A+B=67° 29'$	$\log b=1.11103$	$\log c=1.49959$
$C=112° 31'$	$b=12.913$	$c=31.593$

EXERCISE XIII.

1. Given $a = 500$, $A = 10° 12'$, $B = 46° 36'$;
find $C = 123° 12'$, $b = 2051.48$, $c = 2362.61$.
2. Given $a = 795$, $A = 79° 59'$, $B = 44° 41'$;
find $C = 55° 20'$, $b = 567.688$, $c = 663.986$.
3. Given $a = 804$, $A = 99° 55'$, $B = 45° 1'$;
find $C = 35° 4'$, $b = 577.313$, $c = 468.933$.
4. Given $a = 820$, $A = 12° 49'$, $B = 141° 59'$;
find $C = 25° 12'$, $b = 2276.63$, $c = 1573.89$.
5. Given $c = 1005$, $A = 78° 19'$, $B = 54° 27'$;
find $C = 47° 14'$, $a = 1340.6$, $b = 1113.8$.
6. Given $b = 13.57$, $B = 13° 57'$, $C = 57° 13'$;
find $A = 108° 50'$, $a = 53.276$, $c = 47.324$.
7. Given $a = 6412$, $A = 70° 55'$, $C = 52° 9'$;
find $B = 56° 56'$, $b = 5685.9$, $c = 5357.5$.
8. Given $b = 999$, $A = 37° 58'$, $C = 65° 2'$;
find $B = 77°$, $a = 630.77$, $c = 929.48$.

9. In order to determine the distance of a hostile fort A from a place B, a line BC and the angles ABC and BCA were measured, and found to be 322.55 yards, 60° 34′, and 56° 10′, respectively. Find the distance AB.

10. In making a survey by triangulation, the angles B and C of a triangle ABC were found to be 50° 30′ and 122° 9′, respectively, and the length BC is known to be 9 miles. Find AB and AC.

11. Two observers 5 miles apart on a plain, and facing each other, find that the angles of elevation of a balloon in the same vertical plane with themselves are 55° and 58°, respectively. Find the distance from the balloon to each observer, and also the height of the balloon above the plain.

12. In a parallelogram given a diagonal d and the angles x and y which this diagonal makes with the sides. Find the sides. Compute the results when $d = 11.237$, $x = 19° 1'$, and $y = 42° 54$.

13. A lighthouse was observed from a ship to bear N. 34° E.; after sailing due south 3 miles, it bore N. 23° E. Find the distance from the lighthouse to the ship in both positions.

NOTE. The phrase *to bear N. 34° E.* means that the line of sight to the lighthouse is in the north-east quarter of the horizon, and makes, with a line due north, an angle of 34°.

14. In a trapezoid given the parallel sides a and b, and the angles x and y at the ends of one of the parallel sides. Find the non-parallel sides. Compute the results when $a = 15$, $b = 7$, $x = 70°$, $y = 40°$.

Solve the following examples without using logarithms:

15. Given $b = 7.07107$, $A = 30°$, $C = 105°$; find a and c.

16. Given $c = 9.562$, $A = 45°$, $B = 60°$; find a and b.

17. The base of a triangle is 600 feet, and the angles at the base are 30° and 120°. Find the other sides and the altitude.

18. Two angles of a triangle are, the one 20°, the other 40°. Find the ratio of the opposite sides.

19. The angles of a triangle are as 5 : 10 : 21, and the side opposite the smallest angle is equal to 3. Find the other sides.

20. Given one side of a triangle equal to 27, the adjacent angles equal each to 30°. Find the radius of the circumscribed circle. (See § 36, Remark.)

§ 41. CASE II.

Given two sides a and b, and the angle A opposite to the side a; find the remaining parts B, C, c.

This case, like the preceding case, is solved by means of the Law of Sines.

Since $$\frac{\sin B}{\sin A} = \frac{b}{a}, \text{ therefore } \sin B = \frac{b \sin A}{a};$$

$$C = 180° - (A + B).$$

And since $$\frac{c}{a} = \frac{\sin C}{\sin A}, \text{ therefore } c = \frac{a \sin C}{\sin A}.$$

When an angle is determined by its sine it admits of two values, which are supplements of each other (§ 28); hence, either value of B may be taken unless excluded by the conditions of the problem.

If $a > b$, then by Geometry $A > B$, and B must be acute whatever be the value of A; for a triangle can have only one obtuse angle. Hence, there is *one, and only one, triangle* that will satisfy the given conditions.

If $a = b$, then by Geometry $A = B$; both A and B must be acute, and *the required triangle is isosceles.*

If $a < b$, then by Geometry $A < B$, and A must be acute in order that the triangle may be possible. If A is acute, it is evident from Fig. 33, where $\angle BAC = A$, $AC = b$, $CB = CB' = a$, that *the two triangles* ACB *and* ACB' *will satisfy the given conditions*, provided a is greater than the perpendicular CP; that is, provided a is greater than $b \sin A$ (§ 10). The angles ABC and $AB'C$ are supplementary (since $\angle ABC = \angle BB'C$); they are in fact the supplementary angles obtained from the formula

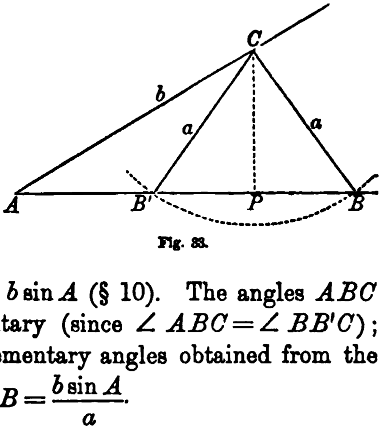

Fig. 33.

$$\sin B = \frac{b \sin A}{a}.$$

If, however, $a = b \sin A = CP$ (Fig. 33), then $\sin B = 1$, $B = 90°$, and *the triangle required is a right triangle.*

If $a < b \sin A$, that is, $< CP$, then $\sin B > 1$, and *the triangle is impossible.*

These results, for convenience, may be thus stated:

If $a > b$, or $a = b$, or if $a = b \sin A$, *One* solution.

If $a < b$, but $> b \sin A$, and $A < 90°$, *Two* solutions.

If $a < b$ and $A > 90°$, or if $a < b \sin A$ and $A < 90°$, *No* solution.

The number of solutions can often be determined by inspection. If there is any doubt, it may be removed by computing the value of $b \sin A$.

Or we may proceed to compute $\log \sin B$. If $\log \sin B = 0$, the triangle required is a right triangle. If $\log \sin B > 0$, the triangle is impossible. If $\log \sin B < 0$, there is *one* solution when $a > b$; there are *two* solutions when $a < b$.

When there are two solutions, let B', C', c' denote the unknown parts of the second triangle; then,

$$B' = 180° - B, \quad C' = 180° - (A + B') = B - A,$$

$$c' = \frac{a \sin C'}{\sin A}.$$

EXAMPLES.

1. Given $a = 16$, $b = 20$, $A = 106°$; find the remaining parts.

In this case $a < b$, and $A > 90°$; therefore the triangle is impossible.

2. Given $a = 36$, $b = 80$, $A = 30°$; find the remaining parts.

Here we have $b \sin A = 80 \times \frac{1}{2} = 40$; so that $a < b \sin A$, and the triangle is impossible.

3. Given $a = 72630$, $b = 117480$, $A = 80° 0' 50''$; find B, C, c.

$a = 72630$	$\operatorname{colog} a = 5.13888$	Here $\log \sin B > 0$.
$b = 117480$	$\log b = 5.06996$	$\therefore$ *no* solution.
$A = 80° 0' 50''$	$\log \sin A = 9.99337$	
	$\log \sin B = 0.20221$	

4. Given $a = 13.2$, $b = 15.7$, $A = 57° 13' 15.3''$; find B, C, c.

$a = 13.2$	$\operatorname{colog} a = 8.87943$	$c = b \cos A$
$b = 15.7$	$\log b = 1.19590$	$\log b = 1.19590$
$A = 57° 13' 15.3''$	$\log \sin A = 9.92467$	$\log \cos A = 9.73352$
Here $\log \sin B = 0$,	$\log \sin B = 0.00000$	$\log c = 0.92942$
$\therefore$ a *right* triangle.	$B = 90°$	$c = 8.5$
	$\therefore C = 32° 46' 44.7''$	

5. Given $a = 767$, $b = 242$, $A = 36°53'2''$; find B, C, c.

$a = 767$	$\text{colog}\, a = 7.11520$	$\log a = 2.88480$
$b = 242$	$\log b = 2.38382$	$\log\sin C = 9.86970$
$A = 36°\,53'\,2''$	$\log\sin A = 9.77830$	$\text{colog}\sin A = 0.22170$
Here $a > b$,	$\log\sin B = 9.27732$	$\log c = 2.97620$
and $\log\sin B < 0$.	$B = 10°\,54'\,58''$	$c = 946.675$
∴ *one* solution.	$\therefore C = 132°\,12'\,0''$	

6. Given $a = 177.01$, $b = 216.45$, $A = 35°36'20''$; find the other parts.

$a = 177.01$	$\text{colog}\, a = 7.75200$	$\log a = 2.24800$	2.24800
$b = 216.45$	$\log b = 2.33536$	$\text{colog}\sin A = 0.23493$	0.23493
$A = 35°\,36'\,20''$	$\log\sin A = 9.76507$	$\log\sin C = 9.99462$	9.23034
Here $a < b$,	$\log\sin B = 9.85243$	$\log c = 2.47755$	1.71327
and $\log\sin B < 0$.	$B = 45°\,23'\,28''$	$c = 300.29$ or	51.674
∴ *two* solutions.	or $134°\,36'\,32''$		
	$\therefore C = 99°\,0'\,12''$		
	or $9°\,47'\,8''$		

EXERCISE XIV.

1. Determine the number of solutions in each of the following cases:

(i.) $a = 80$, $b = 100$, $A = 30°$.
(ii.) $a = 50$, $b = 100$, $A = 30°$.
(iii.) $a = 40$, $b = 100$, $A = 30°$.
(iv.) $a = 13.4$, $b = 11.46$, $A = 77°20'$.
(v.) $a = 70$, $b = 75$, $A = 60°$.
(vi.) $a = 134.16$, $b = 84.54$, $B = 52°9'11''$.

2. Given $a = 840$, $b = 485$, $A = 21°31'$;
find $B = 12°13'34''$, $C = 146°15'26''$, $c = 1272.18$.

3. Given $a = 9.399$, $b = 9.197$, $A = 120°35'$;
find $B = 57°23'40''$, $C = 2°1'20'$, $c = 0.38525$.

4. Given $a = 91.06$, $b = 77.04$, $A = 51°9'6''$;
find $B = 41°13'$, $C = 87°37'54''$, $c = 116.82$.

5. Given $a = 55.55$, $b = 66.66$, $B = 77°44'40''$;
find $A = 54°31'13''$, $C = 47°44'7''$, $c = 50.481$.

6. Given $a = 309$, $b = 360$, $A = 21° 14' 25''$;
find $B = 24° 57' 54''$, $C = 133° 47' 41''$, $c = 615.67$,
$B' = 155° 2' 6''$, $C' = 3° 43' 29''$, $c' = 55.41$.

7. Given $a = 8.716$, $b = 9.787$, $A = 38° 14' 12''$;
find $B = 44° 1' 28''$, $C = 97° 44' 20''$, $c = 13.954$,
$B' = 135° 58' 32''$, $C' = 5° 47' 16''$, $c' = 1.4203$.

8. Given $a = 4.4$, $b = 5.21$, $A = 57° 37' 17''$;
find $B = 90°$, $C = 32° 22' 43''$, $c = 2.79$.

9. Given $a = 34$, $b = 22$, $B = 30° 20'$;
find $A = 51° 18' 27''$, $C = 98° 21' 33''$, $c = 43.098$,
$A' = 128° 41' 33''$, $C' = 20° 58' 27''$, $c' = 15.593$.

10. Given $b = 19$, $c = 18$, $C = 15° 49'$;
find $B = 16° 43' 13''$, $A = 147° 27' 47''$, $a = 35.519$,
$B' = 163° 16' 47''$, $A' = 0° 54' 13''$, $a' = 1.0408$,

11. Given $a = 75$, $b = 29$, $B = 16° 15' 36''$; find the difference between the areas of the two corresponding triangles.

12. Given in a parallelogram the side a, a diagonal d, and the angle A made by the two diagonals; find the other diagonal.

Special case: $a = 35$, $d = 63$, $A = 21° 36' 30''$.

§ 42. CASE III.

Given two sides a and b and the included angle C; find the remaining parts A, B, and c.

SOLUTION I. The angles A and B may both be found by means of Formula [27], § 38, which may be written

$$\tan \tfrac{1}{2}(A - B) = \frac{a - b}{a + b} \times \tan \tfrac{1}{2}(A + B).$$

Since $\tfrac{1}{2}(A + B) = \tfrac{1}{2}(180° - C)$, the value of $\tfrac{1}{2}(A + B)$ is known; so that this equation enables us to find the value of $\tfrac{1}{2}(A - B)$. We then have

$$\tfrac{1}{2}(A + B) + \tfrac{1}{2}(A - B) = A,$$

and $$\tfrac{1}{2}(A + B) - \tfrac{1}{2}(A - B) = B.$$

After A and B are known, the side c may be found by the Law of Sines, which gives its value in two ways, as follows:

$$c = \frac{a \sin C}{\sin A}, \quad \text{or} \quad c = \frac{b \sin C}{\sin B}.$$

SOLUTION II. The third side c may be found directly from the equation (§ 37)

$$c = \sqrt{a^2 + b^2 - 2ab \cos C};$$

and then, by the Law of Sines, the following equations for computing the values of the angles A and B are obtained:

$$\sin A = a \times \frac{\sin C}{c}, \quad \sin B = b \times \frac{\sin C}{c}.$$

SOLUTION III. If, in the triangle ABC (Fig. 34), BD is drawn perpendicular to the side AC, then

$$\tan A = \frac{BD}{AD} = \frac{BD}{AC - DC}.$$

Now $BD = a \sin C$ (§ 10),

and $DC = a \cos C$.

$$\therefore \tan A = \frac{a \sin C}{b - a \cos C}.$$

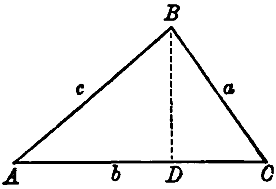

Fig. 34.

By merely changing the letters,

$$\tan B = \frac{b \sin C}{a - b \cos C}.$$

It is not necessary, however, to use both formulas. When one angle, as A, has been found, the other, B, may be found from the relation $A + B + C = 180°$.

When the angles are known, the third side is found by the Law of Sines, as in Solution I.

NOTE. When all three unknown parts are required, Solution I. is the most convenient in practice. When only the third side c is desired, Solution II. may be used to advantage, provided the values of a^2 and b^2 can be readily obtained without the aid of logarithms. But Solutions II. and III. are not adapted to logarithmic work.

EXAMPLES.

1. Given $a = 748$, $b = 375$, $C = 63° 35' 30''$; find A, B, and c.

$a + b = 1123$		
$a - b = 373$	$\log(a - b) = 2.57171$	$\log b = 2.57403$
$(A+B) = 116° 24' 30''$	$\text{colog}(a + b) = 6.94961$	$\log\sin C = 9.95214$
$\frac{1}{2}(A+B) = 58° 12' 15''$	$\log\tan\frac{1}{2}(A+B) = 0.20766$	$\text{colog}\sin B = 0.30073$
$\frac{1}{2}(A-B) = 28° 10' 52''$	$\log\tan\frac{1}{2}(A-B) = 9.72898$	$\log c = 2.82690$
$A = 86° 23' 7''$	$\frac{1}{2}(A-B) = 28° 10' 52''$	$c = 671.27$
$B = 30° 1' 23''$		

NOTE. In the above Example we use the angle B in finding the side c, rather than the angle A, because A is near 90°, and therefore its sine should be avoided.

2. Given $a = 4$, $c = 6$, $B = 60°$; find the third side b.

Here Solution II. may be used to advantage. We have

$$b = \sqrt{a^2 + c^2 - 2ac\cos B} = \sqrt{16 + 36 - 24} = \sqrt{28};$$

$$\log 28 = 1.44716, \quad \log\sqrt{28} = 0.72358, \quad \sqrt{28} = 5.2915;$$

that is, $b = 5.2915$.

EXERCISE XV.

1. Given $a = 77.99$, $b = 83.39$, $C = 72° 15'$; [§ 38, N.
find $A = 51° 15'$, $B = 56° 30'$, $c = 95.24$.

2. Given $b = 872.5$, $c = 632.7$, $A = 80°$;
find $B = 60° 45'$, $C = 39° 15'$, $a = 984.83$.

3. Given $a = 17$, $b = 12$, $C = 59° 17'$;
find $A = 77° 12' 53''$, $B = 43° 30' 7''$, $c = 14.987$.

4. Given $b = \sqrt{5}$, $c = \sqrt{3}$, $A = 35° 53'$;
find $B = 93° 28' 36''$, $C = 50° 38' 24''$, $a = 1.313$.

5. Given $a = 0.917$, $b = 0.312$, $C = 33° 7' 9''$;
find $A = 132° 18' 27''$, $B = 14° 34' 24''$, $c = 0.67748$.

6. Given $a = 13.715$, $c = 11.214$, $B = 15° 22' 36''$;
find $A = 118° 55' 49''$, $C = 45° 41' 35''$, $b = 4.1554$.

7. Given $b = 3000.9$, $c = 1587.2$, $A = 86° 4' 4''$;
find $B = 65° 13' 51''$, $C = 28° 42' 5''$, $a = 3297.2$.

8. Given $a = 4527$, $b = 3465$, $C = 66°\,6'\,27''$;
find $A = 68°\,29'\,15''$, $B = 45°\,24'\,18''$, $c = 4449$.

9. Given $a = 55.14$, $b = 33.09$, $C = 30°\,24'$;
find $A = 117°\,24'\,33''$, $B = 32°\,11'\,27''$, $c = 31.431$.

10. Given $a = 47.99$, $b = 33.14$, $C = 175°\,19'\,10''$;
find $A = 2°\,46'\,8''$, $B = 1°\,54'\,42''$, $c = 81.066$.

11. If two sides of a triangle are each equal to 6, and the included angle is 60°, find the third side.

12. If two sides of a triangle are each equal to 6, and the included angle is 120°, find the third side.

13. Apply Solution I. to the case in which $a = b$ or the triangle is isosceles.

14. If two sides of a triangle are 10 and 11, and the included angle is 50°, find the third side.

15. If two sides of a triangle are 43.301 and 25, and the included angle is 30°, find the third side.

16. In order to find the distance between two objects A and B separated by a swamp, a station C was chosen, and the distances $CA = 3825$ yards, $CB = 3475.6$ yards, together with the angle $ACB = 62°\,31'$, were measured. Find the distance from A to B.

17. Two inaccessible objects A and B are each viewed from two stations C and D 562 yards apart. The angle ACB is $62°\,12'$, BCD $41°\,8'$, ADB $60°\,49'$, and ADC $34°\,51'$; required the distance AB.

18. Two trains start at the same time from the same station, and move along straight tracks that form an angle of 30°, one train at the rate of 30 miles an hour, the other at the rate of 40 miles an hour. How far apart are the trains at the end of half an hour?

19. In a parallelogram given the two diagonals 5 and 6, and the angle that they form $49°\,18'$. Find the sides.

20. In a triangle one angle $= 139°\,54'$, and the sides forming the angle have the ratio $5:9$. Find the other two angles.

§ 43. Case IV.

Given the three sides a, b, c; find the angles A, B, C.

The angles may be found directly from the formulas established in § 37. Thus, from the formula

$$a^2 = b^2 + c^2 - 2bc \cos A$$

we have
$$\cos A = \frac{b^2 + c^2 - a^2}{2bc}.$$

From this equation formulas adapted to logarithmic work are deduced as follows:

For the sake of brevity, let $a + b + c = 2s$; then $b + c - a = 2(s - a)$, $a - b + c = 2(s - b)$, and $a + b - c = 2(s - c)$.

Then the value of $1 - \cos A$ is

$$1 - \frac{b^2 + c^2 - a^2}{2bc} = \frac{2bc - b^2 - c^2 + a^2}{2bc} = \frac{a^2 - (b - c)^2}{2bc}$$
$$= \frac{(a + b - c)(a - b + c)}{2bc} = \frac{2(s - b)(s - c)}{bc};$$

and the value of $1 + \cos A$ is

$$1 + \frac{b^2 + c^2 - a^2}{2bc} = \frac{2bc + b^2 + c^2 - a^2}{2bc} = \frac{(b + c)^2 - a^2}{2bc}$$
$$= \frac{(b + c + a)(b + c - a)}{2bc} = \frac{2s(s - a)}{bc}.$$

But from Formulas [16] and [17], § 34, it follows that

$1 - \cos A = 2 \sin^2 \frac{1}{2} A$, and $1 + \cos A = 2 \cos^2 \frac{1}{2} A$.

$\therefore\ 2 \sin^2 \frac{1}{2} A = \frac{2(s - b)(s - c)}{bc}$, and $2 \cos^2 \frac{1}{2} A = \frac{2s(s - a)}{bc}$,

whence
$$\sin \tfrac{1}{2} A = \sqrt{\frac{(s - b)(s - c)}{bc}}, \qquad [28]$$

$$\cos \tfrac{1}{2} A = \sqrt{\frac{s(s - a)}{bc}}, \qquad [29]$$

and therefore
$$\tan \tfrac{1}{2} A = \sqrt{\frac{(s - b)(s - c)}{s(s - a)}} \qquad [30]$$

By merely changing the letters,

$$\sin \tfrac{1}{2} B = \sqrt{\frac{(s-a)(s-c)}{ac}}, \quad \sin \tfrac{1}{2} C = \sqrt{\frac{(s-a)(s-b)}{ab}}.$$

$$\cos \tfrac{1}{2} B = \sqrt{\frac{s(s-b)}{ac}}, \quad \cos \tfrac{1}{2} C = \sqrt{\frac{s(s-c)}{ab}}.$$

$$\tan \tfrac{1}{2} B = \sqrt{\frac{(s-a)(s-c)}{s(s-b)}}, \quad \tan \tfrac{1}{2} C = \sqrt{\frac{(s-a)(s-b)}{s(s-c)}}.$$

There is then a choice of three different formulas for finding the value of each angle. If half the angle is very near 0°, the formula for the cosine will not give a very accurate result, because the cosines of angles near 0° differ little in value; and the same holds true of the formula for the sine when half the angle is very near 90°. Hence, in the first case the formula for the sine, in the second that for the cosine, should be used.

But, in general, the formulas for the tangent are to be preferred.

It is not necessary to compute by the formulas more than two angles; for the third may then be found from the equation

$$A + B + C = 180^\circ.$$

There is this advantage, however, in computing all three angles by the formulas, that we may then use the sum of the angles as a test of the accuracy of the results.

In case it is desired to compute all the angles, the formulas for the tangent may be put in a more convenient form.

The value of $\tan \tfrac{1}{2} A$ may be written

$$\sqrt{\frac{(s-a)(s-b)(s-c)}{s(s-a)^2}} \quad \text{or} \quad \frac{1}{s-a}\sqrt{\frac{(s-a)(s-b)(s-c)}{s}}.$$

Hence, if we put

$$\sqrt{\frac{(\mathbf{s}-\mathbf{a})(\mathbf{s}-\mathbf{b})(\mathbf{s}-\mathbf{c})}{\mathbf{s}}} = \mathbf{r}, \qquad [31]$$

we have

$$\tan \tfrac{1}{2} \mathbf{A} = \frac{\mathbf{r}}{\mathbf{s}-\mathbf{a}}. \qquad [32]$$

In like manner,

$$\tan \tfrac{1}{2} B = \frac{r}{s-b}, \qquad \tan \tfrac{1}{2} C = \frac{r}{s-c}.$$

EXAMPLES.

1. Given $a = 3.41$, $b = 2.60$, $c = 1.58$; find the angles.

Using Formula [30], and the corresponding formula for $\tan \frac{1}{2} B$, we may arrange the work as follows:

$$\begin{array}{r|r|r}
a = 3.41 & \operatorname{colog} s = 9.42079 & \operatorname{colog} s = 9.42079 - 10 \\
b = 2.60 & \operatorname{colog}(s-a) = 0.41454 & \log(s-a) = 9.58546 - 10 \\
c = 1.58 & \log(s-b) = 0.07737 & \operatorname{colog}(s-b) = 9.92263 - 10 \\
2s = 7.59 & \log(s-c) = \underline{0.34537} & \log(s-c) = \underline{0.34537} \\
s = 3.795 & 2\overline{)0.25807} & 2\overline{)19.27425 - 20} \\
s-a = 0.385 & \log\tan\tfrac{1}{2}A = 0.12903 & \log\tan\tfrac{1}{2}B = 9.63713 - 10 \\
s-b = 1.195 & \tfrac{1}{2}A = 53^\circ\, 23'\, 20'' & \tfrac{1}{2}B = 23^\circ\, 26'\, 37'' \\
s-c = 2.215 & A = 106^\circ\, 46'\, 40'' & B = 46^\circ\, 53'\, 14''
\end{array}$$

$$\therefore A + B = 153^\circ\, 39'\, 54'', \text{ and } C = 26^\circ\, 20'\, 6''.$$

2. Solve Example 1 by finding all three angles by the use of Formulas [31] and [32].

Here the work may be compactly arranged as follows, if we find $\log\tan\frac{1}{2}A$, etc., by *subtracting* $\log(s-a)$, etc., from $\log r$ instead of adding the cologarithm:

$$\begin{array}{r|r|r}
a = 3.41 & \log(s-a) = 9.58546 & \log\tan\tfrac{1}{2}A = 10.12903 \\
b = 2.60 & \log(s-b) = 0.07737 & \log\tan\tfrac{1}{2}B = 9.63713 \\
c = \underline{1.58} & \log(s-c) = 0.34537 & \log\tan\tfrac{1}{2}C = \underline{9.36912} \\
2s = \underline{7.59} & \operatorname{colog} s = \underline{9.42079} & \tfrac{1}{2}A = 53^\circ\, 23'\, 20'' \\
s = 3.795 & \log r^2 = 9.42899 & \tfrac{1}{2}B = 23^\circ\, 26'\, 37'' \\
s-a = 0.385 & \log r = 9.71450 & \tfrac{1}{2}C = \underline{13^\circ\, 10'\, 3''} \\
s-b = 1.195 & & A = 106^\circ\, 46'\, 40'' \\
s-c = \underline{2.215} & & B = 46^\circ\, 53'\, 14'' \\
2s = 7.590 \text{ (proof).} & & C = \underline{26^\circ\, 20'\, 6''}
\end{array}$$

$$\text{Proof, } A + B + C = 180^\circ\, 0'\, 0''$$

NOTE. Even if no mistakes are made in the work the sum of the three angles found as above may differ very slightly from 180° in consequence of the fact that logarithmic computation is at best only a method of close approximation. When a difference of this kind exists it should be divided among the angles according to the probable amount of error for each angle.

EXERCISE XVI.

Solve the following triangles, taking the three sides as the given parts:

	a	b	c	A	B	C
1	51	65	20	38° 52′ 48″	126° 52′ 12″	14° 15′
2	78	101	29	32° 10′ 54″	136° 23′ 50″	11° 25′ 16″
3	111	145	40	27° 20′ 32″	143° 7′ 48″	9° 31′ 40″
4	21	26	31	42° 6′ 13″	56° 6′ 36″	81° 47′ 11″
5	19	34	49	16° 25′ 36″	30° 24′	133° 10′ 24″
6	43	50	57	46° 49′ 35″	57° 59′ 44″	75° 10′ 41″
7	37	58	79	26° 0′ 29″	43° 25′ 20″	110° 34′ 11″
8	73	82	91	49° 34′ 58″	58° 46′ 58″	71° 38′ 4″
9	14.493	55.4363	66.9129	8° 20′	33° 40′	138°
10	$\sqrt{5}$	$\sqrt{6}$	$\sqrt{7}$	51° 53′ 12″	59° 31′ 48″	68° 35′

11. Given $a = 6$, $b = 8$, $c = 10$; find the angles.

12. Given $a = 6$, $b = 6$, $c = 10$; find the angles.

13. Given $a = 6$, $b = 6$, $c = 6$; find the angles.

14. Given $a = 6$, $b = 5$, $c = 12$; find the angles.

15. Given $a = 2$, $b = \sqrt{6}$, $c = \sqrt{3} - 1$; find the angles.

16. Given $a = 2$, $b = \sqrt{6}$, $c = \sqrt{3} + 1$; find the angles.

17. The distances between three cities A, B, and C are as follows: $AB = 165$ miles, $AC = 72$ miles, and $BC = 185$ miles. B is due east from A. In what direction is C from A? What two answers are admissible?

18. Under what visual angle is an object 7 feet long seen by an observer whose eye is 5 feet from one end of the object and 8 feet from the other end?

19. When Formula [28] is used for finding the value of an angle, why does the ambiguity that occurs in Case II. not exist?

20. If the sides of a triangle are 3, 4, and 6, find the sine of the largest angle.

21. Of three towns A, B, and C, A is 200 miles from B and 184 miles from C, B is 150 miles due north from C; how far is A north of C?

§ 44. AREA OF A TRIANGLE.

If F denote the area of the triangle ABC (Fig. 30 or 31, page 50), then, by Geometry,

$$F = \tfrac{1}{2} c \times CD.$$

By § 10, $CD = a \sin B$.

Therefore, $$F = \tfrac{1}{2} ac \sin B. \qquad [33]$$

And, in like manner,

$$F = \tfrac{1}{2} ab \sin C \quad \text{and} \quad F = \tfrac{1}{2} bc \sin A.$$

That is: *The area of a triangle is equal to half the product of two sides and the sine of the included angle.*

By Formula [33] the area of a triangle may be found directly when two sides and the included angle are given; in the other cases the formula may be used when these parts have been computed.

When the three sides of a triangle are given, as in Case IV., a formula for its area may be found as follows:

By § 33, $\sin B = 2 \sin \tfrac{1}{2} B \times \cos \tfrac{1}{2} B$.

By substituting for $\sin \tfrac{1}{2} B$ and $\cos \tfrac{1}{2} B$ their values in terms of the sides given in § 43,

$$\sin B = \frac{2}{ac} \sqrt{s(s-a)(s-b)(s-c)}.$$

By substituting this value of $\sin B$ in [33],

$$F = \sqrt{s(s-a)(s-b)(s-c)}. \qquad [34]$$

If R denote (as in § 36) the radius of the circumscribed circle, we have, from § 36,

$$\sin B = \frac{b}{2R}.$$

By substituting this value of $\sin B$ in [33],

$$F = \frac{abc}{4R}. \qquad [35]$$

If r denote the radius of the inscribed circle, and we divide the triangle into three triangles by lines from the centre of this circle to the vertices, the altitude of each of the three triangles is equal to r. Therefore,

$$F = \tfrac{1}{2}r(a+b+c) = rs. \qquad [36]$$

By substituting in this formula the value of F given in [34],

$$r = \sqrt{\frac{(s-a)(s-b)(s-c)}{s}};$$

whence r, in [31] § 43, is equal to the radius of the inscribed circle.

Exercise XVII.

Find the area:

1. Given $a = 4474.5$, $b = 2164.5$, $C = 116° 30' 20''$.
2. Given $b = 21.66$, $c = 36.94$, $A = 66° 4' 19''$.
3. Given $a = 510$, $c = 173$, $B = 162° 30' 28''$.
4. Given $a = 408$, $b = 41$, $c = 401$.
5. Given $a = 40$, $b = 13$, $c = 37$.
6. Given $a = 624$, $b = 205$, $c = 445$.
7. Given $b = 149$, $A = 70° 42' 30''$, $B = 39° 18' 28''$.
8. Given $a = 215.9$, $c = 307.7$, $A = 25° 9' 31''$.
9. Given $b = 8$, $c = 5$, $A = 60°$.
10. Given $a = 7$, $c = 3$, $A = 60°$.
11. Given $a = 60$, $B = 40° 35' 12''$, area $= 12$; find the radius of the inscribed circle.
12. Obtain a formula for the area of a parallelogram in terms of two adjacent sides and the included angle.
13. Obtain a formula for the area of an isosceles trapezoid in terms of the two parallel sides and an acute angle.
14. Two sides and included angle of a triangle are 2416, 1712, and 30°; and two sides and included angle of another triangle are 1948, 2848, and 150°; find the sum of their areas.
15. The base of an isosceles triangle is 20, and its area is $100 \div \sqrt{3}$; find its angles.

EXERCISE XVIII.

1. From a ship sailing down the English Channel the Eddystone was observed to bear N. 33° 45′ W.; and after the ship had sailed 18 miles S. 67° 30′ W. it bore N. 11° 15′ E. Find its distance from each position of the ship.

2. Two objects, *A* and *B*, were observed from a ship to be at the same instant in a line bearing N. 15° E. The ship then sailed north-west 5 miles, when it was found that *A* bore due east and *B* bore north-east. Find the distance from *A* to *B*.

3. A castle and a monument stand on the same horizontal plane. The angles of depression of the top and the bottom of the monument viewed from the top of the castle are 40° and 80°; the height of the castle is 140 feet. Find the height of the monument.

4. If the sun's altitude is 60°, what angle must a stick make with the horizon in order that its shadow in a horizontal plane may be the longest possible?

5. If the sun's altitude is 30°, find the length of the longest shadow cast on a horizontal plane by a stick 10 feet in length.

6. In a circle with the radius 3 find the area of the part comprised between parallel chords whose lengths are 4 and 5. (Two solutions.)

7. *A* and *B*, two inaccessible objects in the same horizontal plane, are observed from a balloon at *C* and from a point *D* directly under the balloon, and in the same horizontal plane with *A* and *B*. If $CD = 2000$ yards, $\angle ACD = 10° 15' 10''$, $\angle BCD = 6° 7' 20''$, $\angle ADB = 49° 34' 50''$, find *AB*.

8. *A* and *B* are two objects whose distance, on account of intervening obstacles, cannot be directly measured. At the summit *C* of a hill, whose height above the common horizontal plane of the objects is known to be 517.3 yards, $\angle ACB$ is found to be 15° 13′ 15″. The angles of elevation of *C* viewed from *A* and *B* are 21° 9′ 18″ and 23° 15′ 34″ respectively. Find the distance from *A* to *B*.

MISCELLANEOUS PROBLEMS.

[Selected by permission from "Problems in Plane Trigonometry," prepared by Prof. C. J. White, of Harvard College, and published by Charles W. Sever, Cambridge.]

1. The *angular distance* of any object from a horizontal plane, as observed at any point of that plane, is the angle which a line drawn from the object to the point of observation makes with the plane. If the object observed be situated above the horizontal plane (that is, if it is farther from the earth's centre than the plane is), its angular distance from the plane is called its *angle of elevation*. If the object be below the plane, its angular distance from the plane is called its *angle of depression*. These angles are evidently vertical angles.

If two objects are in the same horizontal plane with the point of observation, the angular distance of one object from the other is called its *bearing* from that object.

If two objects are not in the same horizontal plane with either each other or the point of observation, we may suppose vertical lines to be passed through the two objects, and to meet the horizontal plane of the point of observation in two points. The angular distance of these two points is the bearing of either of the objects from the other. It may also be called the *horizontal distance* of one object from the other.

NOTE. "Problems in Plane Trigonometry" can be obtained in pamphlet form of Charles W. Sever, Cambridge, Mass.

RIGHT TRIANGLES.

2. The angle of elevation of a tower is 48° 19′ 14″, and the distance of its base from the point of observation is 95 ft. Find the height of the tower, and the distance of its top from the point of observation.

3. From a mountain 1000 ft. high, the angle of depression of a ship is 77° 35′ 11″. Find the distance of the ship from the summit of the mountain.

4. A flag-staff 90 ft. high, on a horizontal plane, casts a shadow of 117 ft. Find the altitude of the sun.

5. When the moon is setting at any place, the angle at the moon subtended by the earth's radius passing through that place is 57′ 3″. If the earth's radius is 3956.2 miles, what is the moon's distance from the earth's centre?

6. The angle at the earth's centre subtended by the sun's radius is 16′ 2″, and the sun's distance is 92,400,000 miles. Find the sun's diameter in miles.

7. The latitude of Cambridge, Mass., is 42° 22′ 49″. What is the length of the radius of that parallel of latitude?

8. At what latitude is the circumference of the parallel half of that of the equator?

9. In a circle with a radius of 6.7 is inscribed a regular polygon of thirteen sides. Find the length of one of its sides.

10. A regular heptagon, one side of which is 5.73, is inscribed in a circle. Find the radius of the circle.

11. A tower 93.97 ft. high is situated on the bank of a river. The angle of depression of an object on the opposite bank is 25° 12′ 54″. Find the breadth of the river.

12. From a tower 58 ft. high the angles of depression of two objects situated in the same horizontal line with the base of the tower, and on the same side, are 30° 13′ 18″ and 45° 46′ 14″. Find the distance between these two objects.

13. Standing directly in front of one corner of a flat-roofed house, which is 150 ft. in length, I observe that the horizontal angle which the length subtends has for its cosine $\sqrt{\frac{5}{8}}$, and that the vertical angle subtended by its height has for its sine $\frac{3}{\sqrt{34}}$. What is the height of the house?

14. A regular pyramid, with a square base, has an edge 150 ft. in length, and the length of a side of its base is 200 ft. Find the inclination of the face of the pyramid to the base.

15. From one edge of a ditch 36 ft. wide, the angle of elevation of a wall on the opposite edge is 62° 39′ 10″. Find the length of a ladder which will reach from the point of observation to the top of the wall.

16. The top of a flag-staff has been broken off, and touches the ground at a distance of 15 ft. from the foot of the staff. The length of the broken part being 39 ft., find the whole length of the staff.

17. From a balloon, which is directly above one town, is observed the angle of depression of another town, 10° 14′ 9″. The towns being 8 miles apart, find the height of the balloon.

18. From the top of a mountain 3 miles high the angle of depression of the most distant object which is visible on the earth's surface is found to be 2° 13′ 50″. Find the diameter of the earth.

19. A ladder 40 ft. long reaches a window 33 ft. high, on one side of a street. Being turned over upon its foot, it reaches another window 21 ft. high, on the opposite side of the street. Find the width of the street.

20. The height of a house subtends a right angle at a window on the other side of the street; and the elevation of the top of the house, from the same point, is 60°. The street is 30 ft. wide. How high is the house?

21. A lighthouse 54 ft. high is situated on a rock. The elevation of the top of the lighthouse, as observed from a ship, is 4° 52′, and the elevation of the top of the rock is 4° 2′. Find the height of the rock, and its distance from the ship.

22. A man in a balloon observes the angle of depression of an object on the ground, bearing south, to be 35° 30′; the balloon drifts 2½ miles east at the same height, when the angle of depression of the same object is 23° 14′. Find the height of the balloon.

23. A man standing south of a tower, on the same horizontal plane, observes its elevation to be 54° 16′: he goes east 100 yds., and then finds its elevation is 50° 8′. Find the height of the tower.

24. The elevation of a tower at a place A south of it is 30°; and at a place B, west of A, and at a distance of a from it, the the elevation is 18°. Show that the height of the tower is $\frac{a}{\sqrt{(2+2\sqrt{5})}}$; the tangent of 18° being $\frac{\sqrt{5}-1}{\sqrt{(10+2\sqrt{5})}}$.

25. A pole is fixed on the top of a mound, and the angles of elevation of the top and the bottom of the pole are 60° and 30°. Prove that the length of the pole is twice the height of the mound.

26. At a distance (a) from the foot of a tower, the angle of elevation (A) of the top of the tower is the complement of the angle of elevation of a flag-staff on top of it. Show that the length of the staff is $2a \cot 2A$.

27. *A line of true level* is a line every point of which is equally distant from the centre of the earth. A line drawn

tangent to a line of true level at any point is a line of *apparent* level. If at any point both these lines be drawn, and extended one mile, find the distance they are then apart.

28. In Problem 2, determine the effect upon the computed height of the tower, of an error in either the angle of elevation or the measured distance.

OBLIQUE TRIANGLES.

29. To determine the height of an inaccessible object situated on a horizontal plane, by observing its angles of elevation at two points in the same line with its base, and measuring the distance of these two points.

30. The angle of elevation of an inaccessible tower, situated on a horizontal plane, is 63° 26′; at a point 500 ft. farther from the base of the tower the elevation of its top is 32° 14′. Find the height of the tower.

31. A tower is situated on the bank of a river. From the opposite bank the angle of elevation of the tower is 60° 13′, and from a point 40 ft. more distant the elevation is 50° 19′. Find the breadth of the river.

32. A ship sailing north sees two lighthouses 8 miles apart, in a line due west; after an hour's sailing, one lighthouse bears S.W., and the other S.S.W. Find the ship's rate.

33. To determine the height of an accessible object situated on an inclined plane.

34. At a distance of 40 ft. from the foot of a tower on an inclined plane, the tower subtends an angle of 41° 19′; at a point 60 ft. farther away, the angle subtended by the tower is 23° 45′. Find the height of the tower.

35. A tower makes an angle of 113° 12′ with the inclined plane on which it stands; and at a distance of 89 ft. from its base, measured down the plane, the angle subtended by the tower is 23° 27′. Find the height of the tower.

36. From the top of a house 42 ft. high, the angle of elevation of the top of a pole is 14° 13′; at the bottom of the house it is 23° 19′. Find the height of the pole.

37. The sides of a triangle are 17, 21, 28; prove that the length of a line bisecting the greatest side and drawn from the opposite angle is 13.

38. A privateer, 10 miles S.W. of a harbor, sees a ship sail from it in a direction S. 80° E., at a rate of 9 miles an hour. In what direction, and at what rate, must the privateer sail in order to come up with the ship in 1½ hours?

39. A person goes 70 yds. up a slope of 1 in 3½ from the edge of a river, and observes the angle of depression of an object on the opposite shore to be 2¼°. Find the breadth of the river.

40. The length of a lake subtends, at a certain point, an angle of 46° 24′, and the distances from this point to the two extremities of the lake are 346 and 290 ft. Find the length of the lake.

41. Two ships are a mile apart. The angular distance of the first ship from a fort on shore, as observed from the second ship, is 35° 14′ 10″; the angular distance of the second ship from the fort, observed from the first ship, is 42° 11′ 53″. Find the distance in feet from each ship to the fort.

42. Along the bank of a river is drawn a base line of 500 feet. The angular distance of one end of this line from an object on the opposite side of the river, as observed from the other end of the line, is 53°; that of the second extremity from the same object, observed at the first, is 79° 12′. Find the perpendicular breadth of the river.

43. A vertical tower stands on a declivity inclined 15° to the horizon. A man ascends the declivity 80 ft. from the base of the tower, and finds the angle then subtended by the tower to be 30°. Find the height of the tower.

44. The angle subtended by a tower on an inclined plane is, at a certain point, 42° 17′; 325 ft. farther down, it is 21° 47′. The inclination of the plane is 8° 53′. Find the height of the tower.

45. A cape bears north by east, as seen from a ship. The ship sails northwest 30 miles, and then the cape bears east. How far is it from the second point of observation?

46. Two observers, stationed on *opposite* sides of a cloud, observe its angles of elevation to be 44° 56′ and 36° 4′. Their distance from each other is 700 ft. What is the linear height of the cloud?

47. From a point *B* at the foot of a mountain, the elevation of the top *A* is 60°. After ascending the mountain one mile, at an inclination of 30° to the horizon, and reaching a point *C*, the angle *ACB* is found to be 135°. Find the height of the mountain in feet.

48. From a ship two rocks are seen in the same right line with the ship, bearing N. 15° E. After the ship has sailed northwest 5 miles, the first rock bears east, and the second northeast. Find the distance between the rocks.

49. From a window on a level with the bottom of a steeple the elevation of the steeple is 40°, and from a second window 18 ft. higher the elevation is 37° 30′. Find the height of the steeple.

50. To determine the distance between two inaccessible objects by observing angles at the extremities of a line of known length.

51. Wishing to determine the distance between a church *A* and a tower *B*, on the opposite side of a river, I measure a line *CD* along the river (*C* being nearly opposite *A*), and observe the angles *ACB*, 58° 20′; *ACD*, 95° 20′; *ADB*, 53° 30′; *BDC*, 98° 45′. *CD* is 600 ft. What is the distance required?

52. Wishing to find the height of a summit *A*, I measure a horizontal base line *CD*, 440 yds. At *C*, the elevation of *A* is 37° 18′, and the horizontal angle between *D* and the summit is 76° 18′; at *D*, the horizontal angle between *C* and the summit is 67° 14′. Find the height.

53. A balloon is observed from two stations 3000 ft. apart. At the first station the horizontal angle of the balloon and the other station is 75° 25′, and the elevation of the balloon is 18°. The horizontal angle of the first station and the balloon, measured at the second station, is 64° 30′. Find the height of the balloon.

54. Two forces, one of 410 pounds, and the other of 320 pounds, make an angle of 51° 37′. Find the intensity and the direction of their resultant.

55. An unknown force, combined with one of 128 pounds, produces a resultant of 200 pounds, and this resultant makes an angle of 18° 24′ with the known force. Find the intensity and direction of the unknown force.

56. At two stations, the height of a kite subtends the same angle (*A*). The angle which the line joining one station and the kite subtends at the other station is *B*; and the distance between the two stations is *a*. Show that the height of the kite is $\frac{1}{2} a \sin A \sec B$.

57. Two towers on a horizontal plane are 120 ft. apart. A person standing successively at their bases observes that the angular elevation of one is double that of the other; but, when he is half-way between them, the elevations are complementary. Prove that the heights of the towers are 90 and 40 ft.

58. To find the distance of an inaccessible point *C* from either of two points *A* and *B*, having no instruments to measure angles. Prolong *CA* to *a*, and *CB* to *b*, and join *AB*, *Ab*, and *Ba*. Measure *AB*, 500; *aA*, 100; *aB*, 560; *bB*, 100; and *Ab*, 550.

59. Two inaccessible points A and B, are visible from D, but no other point can be found whence both are visible. Take some point C, whence A and D can be seen, and measure CD 200 ft.; ADC, 89°; ACD, 50° 30′. Then take some point E, whence D and B are visible, and measure DE, 200; BDE, 54° 30′; BED, 88° 30′. At D measure ADB, 72° 30′. Compute the distance AB.

60. To compute the horizontal distance between two inaccessible points A and B, when no point can be found whence both can be seen. Take two points C and D, distant 200 yds. so that A can be seen from C, and B from D. From C measure CF, 200 yds. to F, whence A can be seen; and from D measure DE, 200 yds. to E, whence B can be seen. Measure AFC, 83°; ACD, 53° 30′; ACF, 54° 31′; BDE, 54° 30′; BDC, 156° 25′; DEB, 88° 30′.

61. A column in the north temperate zone is east-southeast of an observer, and at noon the extremity of its shadow is northeast of him. The shadow is 80 ft. in length, and the elevation of the column, at the observer's station, is 45°. Find the height of the column.

62. From the top of a hill the angles of depression of two objects situated in the horizontal plane of the base of the hill are 45° and 30°; and the horizontal angle between the two objects is 30°. Show that the height of the hill equals the distance between the objects.

63. Wishing to know the breadth of a river from A to B, I take AC, 100 yds. in the prolongation of BA, and then take CD, 200 yds. at right angles to AC. The angle BDA is 37° 18′ 30″. Find AB.

64. The sum of the sides of a triangle is 100. The angle at A is double that of B, and the angle at B is double that at C. Determine the sides.

65. If $\sin^2 A + 5\cos^2 A = 3$, find A.

66. If $\sin^2 A = m\cos A - n$, find $\cos A$.

67. Given $\sin A = m\sin B$, and $\tan A = n\tan B$, find $\sin A$ and $\cos B$.

68. If $\tan^2 A + 4\sin^2 A = 6$, find A.

69. If $\sin A = \sin 2A$, find A.

70. If $\tan 2A = 3\tan A$, find A.

71. Prove that $\tan 50° + \cot 50° = 2\sec 10°$.

72. Given a regular polygon of n sides, and calling one of them a, find expressions for the radii of the inscribed and the circumscribed circle in terms of n and a.

If P, H, D be the sides of a regular inscribed pentagon, hexagon, and decagon, prove $P^2 = H^2 + D^2$.

AREAS.

73. Obtain the formula for the area of a triangle, given two sides b, c, and the included angle A.

74. Obtain the formula for the area of a triangle, given two angles A and B, and included side c.

75. Obtain the formula for the area of a triangle, given the three sides.

76. If a is the side of an equilateral triangle, its area is $\frac{a^2\sqrt{3}}{4}$.

77. Two consecutive sides of a rectangle are 52.25 ch. and 38.24 ch. Find its area.

78. Two sides of a parallelogram are 59.8 ch. and 37.05 ch., and the included angle is 72° 10′. Find the area.

79. Two sides of a parallelogram are 15.36 ch. and 11.46 ch., and the included angle is 47° 30′. Find its area.

80. Two sides of a triangle are 12.38 ch. and 6.78 ch., and the inclined angle is 46° 24′. Find the area.

81. Two sides of a triangle are 18.37 ch. and 13.44 ch., and they form a right angle. Find the area.

§2. Two angles of a triangle are 76° 54′ and 57° 33′ 12″, and the included side is 9 ch. Find the area.

83. Two sides of a triangle are 19.74 ch. and 17.34 ch. The first bears N. 82° 30′ W.; the second, S. 24° 15′ E. Find the area.

84. The three sides of a triangle are 49 ch., 50.25 ch., and 25.69 ch. Find the area.

85. The three sides of a triangle are 10.64 ch., 12.28 ch., and 9 ch. Find the area.

86. The sides of a triangular field, of which the area is 14 acres, are in the ratio of 3, 5, 7. Find the sides.

87. In the quadrilateral *ABCD* we have *AB*, 17.22 ch.; *AD*, 7.45 ch.; *CD*, 14.10 ch.; *BC*, 5.25 ch.; and the diagonal *AC*, 15.04 ch. Required the area.

88. The diagonals of a quadrilateral are a and b, and they intersect at an angle D. The area of the quadrilateral is $\frac{1}{2}ab \sin D$.

89. The diagonals of a quadrilateral are 34 and 56, intersecting at an angle of 67°. Find the area.

90. The diagonals of a quadrilateral are 75 and 49, intersecting at an angle of 42°. Find the area.

91. The area of a regular polygon of n sides, of which one is a, is $\frac{na^2}{4} \cot \frac{180^\circ}{n}$.

92. One side of a regular pentagon is 25. Find the area.

93. One side of a regular hexagon is 32. Find the area.

94. One side of a regular decagon is 46. Find the area.

95. Find the area of a circle whose circumference is 74 ft.

96. Find the area of a circle whose radius is 125 ft.

97. In a circle with a diameter of 125 ft. find the area of a sector with an arc of 22°.

98. In a circle with a radius of 44 ft. find the area of a sector with an arc of 25°.

99. In a circle with a diameter of 50 ft. find the area of a segment with an arc of 280°.

100. Find the area of a segment (less than a semicircle), of which the chord is 20, and the distance of the chord from the middle point of the smaller arc is 2.

101. If r is the radius of a circle, the area of a regular circumscribed polygon of n sides is $nr^2 \tan \frac{180^\circ}{n}$.

The area of a regular inscribed polygon is $\frac{n}{2} r^2 \sin \frac{360^\circ}{n}$.

102. If a is a side of a regular polygon of n sides, the area of the inscribed circle is $\frac{\pi a^2}{4} \cot^2 \frac{180^\circ}{n}$.

The area of the circumscribed circle is $\frac{\pi a^2}{4} \csc^2 \frac{180^\circ}{n}$.

103. The area of a regular polygon inscribed in a circle is to that of the circumscribed polygon of the same number of sides as 3 to 4. Find the number of sides.

104. The area of a regular polygon inscribed in a circle is a geometric mean between the areas of an inscribed and a circumscribed regular polygon of half the number of sides.

105. The area of a circumscribed regular polygon is an harmonic mean between the areas of an inscribed regular polygon of the same number of sides, and of a circumscribed regular polygon of half that number.

106. The perimeter of a circumscribed regular triangle is double that of the inscribed regular triangle.

107. The square described about a circle is four-thirds the inscribed dodecagon.

108. Two sides of a triangle are 3 and 12, and the included angle is 30°. Find the hypotenuse of an isosceles right triangle of equal area.

PLANE SAILING.

109. **Plane Sailing** is that branch of Navigation in which the surface of the earth is considered a plane. The problems which arise are therefore solved by the methods of Plane Trigonometry.

The following definitions will explain the technical terms which are employed :

The *difference of latitude* of two places is the arc of a meridian comprehended between the parallels of latitude passing through those places.

The *departure* between two meridians is the arc of a parallel of latitude comprehended between those meridians. It evidently diminishes as the distance from the equator at which it is measured increases.

When a ship sails in such a manner as to cross successive meridians at the same angle, it is said to sail on a *rhumb-line.* The constant angle which this line makes with the meridians is called the *course,* and the *distance* between two places is measured on a rhumb-line.

If we neglect the curvature of the earth, and consider the distance, departure, and difference of latitude of two places to be straight lines, lying in one plane, they will form a right triangle, called *the triangle of plane sailing.* If ABD be a plane triangle, right-angled at D, and AD represent the difference of latitude of A and B, DAB will be the course from

A to *B*, *AB* the distance, and *DB* the departure, measured from *B*, between the meridian of *A* and that of *B*.

110. Taking the earth's equatorial diameter to be 7925.6 miles, find the length in feet of the arc of one minute of a great circle.*

111. A ship sails from latitude 43° 45′ S., on a course N. by E., 2345 miles. Find the latitude reached, and the departure made.

112. A ship sails from latitude 1° 45′ N., on a course S.E. by E., and reaches latitude 2° 31′ S. Find the distance, and the departure.

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113. A ship sails from latitude 13° 17′ S., on a course N.E. by E. ¾ E., until the departure is 207 miles. Find the distance, and the latitude reached.

114. A ship sails on a course between S. and E., 244 miles, leaving latitude 2° 52′ S., and reaching latitude 5° 8′ S. Find the course, and the departure.

115. A ship sails from latitude 32° 18′ N., on a course between N. and W., making a distance of 344 miles, and a departure of 103 miles. Find the course, and the latitude reached.

116. A ship sails on a course between S. and E., making a difference of latitude 136 miles, and a departure 203 miles. Find the distance, and the course.

117. A ship sails due north 15 *statute* miles an hour, for one day. What is the distance, in a straight line, from the point left to the point reached? (Take earth's radius, 3962.8 statute miles.)

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* The length of the arc of one minute of a great circle of the earth is called a *geographical mile*, or a *knot*. In the following problems, this is the distance meant by the term "mile," unless otherwise stated.

PARALLEL AND MIDDLE LATITUDE SAILING.

118. The difference of longitude of two places is the angle at the pole made by the meridians of these two places; or, it is the arc of the equator comprehended between these two meridians.

119. In **Parallel Sailing**, a vessel is supposed to sail on a parallel of latitude; that is, either due east or due west. The distance sailed is, in this case, evidently the departure made; and the difference of longitude made depends on the solution of the following problem:

120. Given the departure between any two meridians at any latitude, find the angle which those meridians make, or the difference of longitude of any point on one meridian from any point on the other. (The earth is considered to be a perfect sphere, and the solution depends on simple geometric and trigonometric principles. *Cf.* Problem 7.) The solution gives the following formula:

Diff. long. = depart. × sec. lat.

121. A ship in latitude 42° 16′ N., longitude 72° 16′ W., sails due east a distance of 149 miles. What is the position of the point reached?

122. A ship in latitude 44° 49′ S., longitude 119° 42′ E., sails due west until it reaches longitude 117° 16′ E. Find the distance made.

123. In **Middle Latitude Sailing**, the departure between two places, not on the same parallel of latitude, is considered to be, approximately, the departure between the meridians of those places, measured on that parallel of latitude which lies midway between the parallels of the two places. Except in very high latitudes or excessive runs, such an assumption produces no great error. By the formula of Art. 120, then, we shall have —

Diff. long. = depart. × sec. mid. lat.

124. A ship leaves latitude 31° 14′ N., longitude 42° 19′ W., and sails E.N.E. 325 miles. Find the position reached.

125. Find the bearing and distance of Cape Cod from Havana. (Cape Cod, 42° 2′ N., 70° 3′ W.; Havana, 23° 9′ N., 82° 22′ W.)

126. Leaving latitude 49° 57′ N., longitude 15° 16′ W., a ship sails between S. and W. till the departure is 194 miles, and the latitude is 47° 18′ N. Find the course, distance, and longitude reached.

127. Leaving latitude 42° 30′ N., longitude 58° 51′ W., a ship sails S.E. by S. 300 miles. Find the position reached.

128. Leaving latitude 49° 57′ N., longitude 30° W., a ship sails S. 39° W., and reaches latitude 47° 44′ N. Find the distance, and longitude reached.

129. Leaving latitude 37° N., longitude 32° 16′ W., a ship sails between N. and W. 300 miles, and reaches latitude 41° N. Find the course, and longitude reached.

130. Leaving latitude 50° 10′ S., longitude 30° E., a ship sails E.S.E., making 160 miles' departure. Find the distance, and position reached.

131. Leaving latitude 49° 30′ N., longitude 25° W., a ship sails between S. and E. 215 miles, making a departure of 167 miles. Find the course, and position reached.

132. Leaving latitude 43° S., longitude 21° W., a ship sails 273 miles, and reaches latitude 40° 17′ S. What are the *two* courses and longitudes, either one of which will satisfy the data?

133. Leaving latitude 17° N., longitude 119° E., a ship sails 219 miles, making a departure of 162 miles. What four sets of answers do we get?

134. A ship in latitude 30° sails due east 360 statute miles. What is the shortest distance from the point left to the point reached?

Solve the same problem for latitude 45°, 60°, etc.

TRAVERSE SAILING.

135. **Traverse Sailing** is the application of the principles of Plane and Middle Latitude Sailing to cases when the ship sails from one point to another on two or more different courses. Each course is worked up by itself, and these independent results are combined, as may be seen in the solution of the following example:

136. Leaving latitude 37° 16′ S., longitude 18° 42′ W., a ship sails N.E. 104 miles, then N.N.W. 60 miles, then W. by S. 216 miles. Find the position reached, and its bearing and distance from the point left.

We have, for the first course, difference of latitude 73.5 N., departure 73.5 E.

We have, for the second course, difference of latitude, 55.4 N., departure 23 W.

We have, for the third course, difference of latitude 42.1 S., departure 211.8 W.

On the whole, then, the ship has made 128.9 miles of north latitude, and 42.1 miles of south latitude. The place reached is therefore on a parallel of latitude 86.8 miles to the north of the parallel left; that is, in latitude 35° 49′.2 S.

The departure is, in the same way, found to be 161.3 miles W.; and the middle latitude is 36° 32′.6. With these data, and the formula of Art. 126, we find the difference of longitude to be 201 miles, or 3° 21′ W. Hence the longitude reached is 22° 3′ W.

With the difference of latitude 86.8 miles, and the departure 161.3 miles, we find the course to be N. 61° 43′ W., and the distance 183.2 miles. The ship has reached the same point that it would have reached, if it had sailed directly on a course N. 61° 43′ W., for a distance of 183.2 miles.

137. A ship leaves Cape Cod (Ex. 125), and sails S.E. by S. 114 miles, N. by E. 94 miles, W.N.W. 42 miles. Solve as in Art. 139.

138. A ship leaves Cape of Good Hope (latitude 34° 22′ S., longitude 18° 30′ E.), and sails N.W. 126 miles, N. by E. 84 miles, W.S.W. 217 miles. Solve as in Ex. 136.

EXAMINATION PAPERS.*

PLANE TRIGONOMETRY.

I.

(*Harvard College, Admission. June,* 1881. *Time,* 1½ *hours.*)

1. Define a logarithm. What is the logarithm of ⅛ in the system of which 16 is the base? Find the logarithm of 25 in the same system.

2. Compute the value of $\sqrt[5]{\frac{(0.012)^3 \times 0.27}{(64)^2 \times 0.00651}}$ by logarithms.

3. Find the functions of 127° 10′ from your trigonometric tables.

4. Prove the formula

$$(\cos A - \cos B)^2 + (\sin A - \sin B)^2 = 4 \sin^2 \frac{A-B}{2}.$$

5. Two sides of a triangle are 243 feet and 188 feet, and the angle opposite the second side is 42° 20′. Solve the triangle completely.

6. A pine tree growing on the side of a mountain, which is inclined to the horizontal at an angle of 20°, is broken by the wind but not severed at a distance of 40 feet from the ground. The top falls toward the foot of the mountain, and strikes the ground 50 feet from the base of the tree; find the height of the tree.

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* NOTE. In these papers, as in many text-books, the Greek letters α (*alpha*), β (*bayta*), γ (*gamma*), δ (*delta*), θ (*thayta*), ϕ (*phee*), are occasionally used to denote angles.

II.

(*Harvard College, Admission. June,* 1882. *Time,* 1½ *hours.*)

1. Explain the reason of the rule for finding the *characteristic* (or integral part) of the logarithm of a number.

Show that (according to this rule) the *mantissa* (or fractional part) is always *positive.*

In what cases is the logarithm, as a whole, positive, and in what cases negative?

Thus, state clearly the value of the logarithm of 36,270; of 0.003627. What decimal must be added to the latter logarithm to produce the logarithm of 0.01?

2. Find the time required to increase a sum of money a hundred fold, at *ten* per cent per annum, compound interest, payable yearly.

3. Find the formulas for the trigonometric functions of $90^\circ + a$.

4. Find by the tables the logarithms of the trigonometric functions of 290° 38′ (marking the signs).

5. An observer from a ship saw two headlands. The first bore E.N.E. (*i.e.* 67° 30′ from N. towards E.), and the second N.W. by N. (*i.e.* 33° 45′ from N. towards W.). After he had sailed 16.25 miles N. by W. (*i.e.* 11° 15′ from N. towards W.), the first headland bore due E., and the second N.W. by W. (*i.e.* 56° 15′ from N. towards W.). Find the direction and distance of the second headland from the first.

6. Prove the formulas:

$$\frac{\cos a - \cos\beta}{\cos a + \cos\beta} = -\tan\tfrac{1}{2}(a+\beta)\tan\tfrac{1}{2}(a-\beta),$$

$$\sin\theta = \frac{2\tan\frac{1}{2}\theta}{1+\tan^2\frac{1}{2}\theta}.$$

III.

(*Harvard College, Freshman Examination. April*, 1879. *Time*, 3 *hours*.)

1. Prove the relations between the sine, cosine, and tangent of $90° + \phi$ and the functions of ϕ. Draw a figure for the case where ϕ is obtuse, and show that the proof still holds good.

Confirm your results by means of the formulas for the sine and cosine of the sum of the two angles.

2. Deduce formulas for the sine, cosine, and tangent of $2a$ and $\frac{1}{2}a$, in terms of functions of a.

3. Prove the formula:

$$\cos(\alpha + \beta)\sin\beta - \cos(\alpha + \gamma)\sin\gamma = \sin(\alpha + \beta)\cos\beta - \sin(\alpha + \gamma)\cos\gamma.$$

4. Prove that in any triangle

$$a^2 = b^2 + c^2 - 2bc \cos A.$$

5. Deduce the formulas for the tangents of the half angles of a triangle, in terms of the sides.

6. Solve the triangles:

$$C = 35°, \quad a = 500, \quad c = 250,$$
$$B = 22° 22', \quad a = 67.06, \quad b = 60.03.$$

7. The Delta measures 241 yds. on Cambridge St. and 115 yds. on Quincy St., and the angle between these streets is 88° 52′. Find the other angles of the Delta.

8. Find the area of the Delta.

9. A person travelling east in a railroad train observes a tower situated south of a station A, and on the same horizontal plane with the railroad. At the station B he finds that the distance of the tower is 2 miles; and at C, 3 miles from B, its distance is 4 miles. Find the distance of the tower from A.

IV.

(*Harvard College, Freshman Examination. April*, 1880. *Time*, 3 *hours*.)

1. Deduce the formula $\sin(\alpha+\beta)=\ldots\ldots$, drawing the figure for the case in which α is in the second quadrant and $\alpha+\beta$ in the third.

2. Deduce the formulas for $\cos 2\alpha$, $\sin\frac{1}{2}\alpha$, and $\cos\frac{1}{2}\alpha$, in terms of functions of α.

3. Prove the theorem of the sines.

4. From the fundamental formulas deduce the formula

$$\frac{\tan\frac{1}{2}(A+B)}{\tan\frac{1}{2}(A-B)}=\frac{a+b}{a-b}$$

5. Prove that

$$\frac{\cos(\alpha+\beta+\gamma)}{\cos\alpha\,\cos\beta\,\cos\gamma}=1-\tan\alpha\tan\beta-\tan\beta\tan\gamma-\tan\gamma\tan\alpha.$$

6. In a triangle $B=4°13.4'$ and $a=2001$, give all the solutions in the following cases:

(1) $b=150$,
(2) $b=200$,
(3) $b=2001$.

7. A, B, and C are the corners of a triangular field. A is 40 ft. W. of B and 400 ft. S.W. of C. What is the area of the field? What is the length of the fence which encloses it?

8. From two corners of the Delta, A and B, lines which make angles of $19°52'$ and $57°32'$ respectively with the side AB meet directly under Memorial Hall tower. The length of AB is 345.1 ft., and the angle of elevation of the tower at A is $32°26'$. Find the height of the tower, and its angle of elevation at B.

V.

(*Harvard College, Freshman Examination. April,* 1881. *Time,* 3 *hours.*)

1. Deduce the formulas which connect the functions of $(90° + \phi)$ and ϕ.

2. Prove the fundamental formula for $\cos(\alpha + \beta)$.

3. From the formula just found, obtain three values for $\cos 2\alpha$.

4. Find the values of $\sin\frac{\alpha}{2}$ and $\cos\frac{\alpha}{2}$, in terms of $\cos\alpha$.

5. Prove the formula

$$(\cos A - \cos B)^2 + (\sin A - \sin B)^2 = 4\sin^2\frac{A-B}{2}$$

6. Solve the following triangles:

$b = 2434,\quad c = 1881,\quad C = 42° 22'.$

$a = 0.00543,\quad c = 0.07003,\quad A = 4° 27'.$

7. The sides of a triangle are 715, 541, and 368; find one angle and the area.

8. The height of Memorial Hall tower is 190 feet. From its top the angles of depression of the corners of the Delta which lie on Cambridge St. are 57° 44′ and 16° 59′, and the angle subtended by the line joining these corners is 99° 30′. Find the length of the Delta on Cambridge St.

VI.

(*Harvard College, Freshman Examination. April,* 1882. *Time,* 3 *hours.*)

1. Obtain the formulas which connect the sine, cosine, and tangent of $(180° + \phi)$ with the functions of ϕ.

2. Assuming the formulas for the sine and cosine of the sum of two angles, prove that

(1) $\tan(\alpha + \beta) =$

(2) $\sin\frac{1}{2}\alpha = \sqrt{\frac{1}{2}(1 - \cos\alpha)}.$

3. Find all the values of x, between 0° and 360°, which will satisfy the equations

$$(1)\quad \tan x = 2\sin 2x,$$
$$(2)\quad (\sin x + \cos x)^2 = 2\sin 2x.$$

4. The length of each side of a regular dodecagon is 24 feet; find the radius of the inscribed circle and the area of the polygon.

5. In a certain triangle, $a = 20$, $B = 3°\ 24'$, $C = 85°\ 31'$. Find c by aid of the table containing the values of S and T.

6. Prove the Theorem of Sines, and solve the triangles

$$(1)\quad b = 468,\qquad c = 327,\qquad C = 34°\ 15';$$
$$(2)\quad a = 0.003641,\quad c = 0.08091,\quad A = 5°\ 20'.$$

7. Given $a^2 = b^2 + c^2 - 2bc\cos A$; obtain the formula

$$\sin\tfrac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{bc}}.$$

The sides of a triangle are $a = 2408$, $b = 2028$, $c = 1884$; find the angle A.

8. Hingham is 12 miles south-east of Boston; Quincy is $5\frac{3}{4}$ miles west of Hingham. How far is Quincy from Boston?

9. A person ascending Memorial Hall tower stops to rest at a window, and notices that the angle of elevation of the vane on Appleton Chapel is 3° 34'. When he reaches the top of the tower, 190 feet above the ground, he finds that the height of the Chapel subtends an angle of 13° 9'. The horizontal distance between the two towers being 492 feet, find the height of Appleton Chapel and the distance of the window above the ground.

VII.*

(*Cambridge, Eng. 2nd Previous Exam., Dec.* 7, 1876. *Time,* 2½ *hours.*)

1.* Assuming that the angle subtended at the centre of any circle by an arc equal to its radius is a constant angle, show that any angle may be expressed by the fraction $\frac{\text{arc}}{\text{radius}}$, the constant angle being taken as the unit.

Find the length of the arc subtended by an angle of 60° in a circle whose radius is 3 feet.

2. The sine of a certain angle is $\frac{1}{4}$; find the other trigonometrical ratios of the angle.

3. Trace the change in sign and magnitude in the tangent of an angle, as the angle increases from 0° to 360°.

4. Find, by a geometrical construction, the cosine of 60° and of 45°, and deduce the value of $\cos 3360°$ and $\cos 2565°$.

5. Prove the formulas:

$$(1)\quad \sin(A-B)=\sin A\cos B-\cos A\sin B,$$

$$(2)\quad \cos 2A=\frac{1-\tan^2 A}{1+\tan^2 A},$$

$$(3)\quad \frac{\sin 2A+\sin 4A}{\cos 2A+\cos 4A}=\tan 3A.$$

6. Express the cosine of half an angle in terms of the sine of the angle, and explain the double sign.

Employ the formula to find the value of $\cos 75°$, having given $\sin 150°=\frac{1}{2}$.

7. If A, B, C be the angles of a triangle, and a, b, c the sides respectively opposite to them, show that

$$\cos\tfrac{1}{2}A=\sqrt{\frac{s(s-a)}{bc}},$$

where s = one-half the sum of the sides.

8. Find the greatest angle in a triangle whose sides are 7 feet, 8 feet, and 9 feet.

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* For aid in solving this and similar questions, see Wentworth & Hill's Tables, pages xi and xii.

VIII.

(*Cambridge, Eng. 2nd Previous Exam., Dec.* 7, 1877. *Time,* 2½ *hours.*)

1. Define the cosine, cotangent, and cosecant of an angle, and prove that these ratios remain unchanged so long as the angle is the same.

Find the value of these three ratios for an angle of 45°.

2. Prove the formulas:

$$(1)\quad \sin A = \sqrt{1-\cos^2 A},$$

$$(2)\quad \cos A = \frac{1}{\sqrt{1+\tan^2 A}}.$$

If $\sec A = \sqrt{2}$, find $\tan A$. *Ans.* 1.

3. Prove that

$$\sin(90° + A) = \cos A, \text{ and } \cos(90° + A) = -\sin A.$$

Hence show that $\cos(180° + A) = -\cos A$.

4. Show that $\cos^2 A \tan^2 A + \sin^2 A \cot^2 A = 1$.

5. Prove that $\cos(A+B) = \cos A \cos B - \sin A \sin B$. Hence show that

$$\frac{\cos(A+B+C)}{\sin A \sin B \sin C} = \cot A \cot B \cot C - \cot A - \cot B - \cot C.$$

6. Given that $\sin\frac{1}{2}A = \frac{3}{5}$, find the value of $\tan A$.

Ans. $\frac{24}{7}$.

7. Prove that the sides of any plane triangle are proportional to the sines of the angles opposite to these sides.

If $2s =$ the sum of the three sides (a, b, c) of a triangle, and if A be the angle opposite to the side a, prove that

$$\sin A = \frac{2}{bc}\sqrt{s(s-a)(s-b)(s-c)}.$$

8. Prove that in any plane triangle

$$\tan\tfrac{1}{2}(A-B) = \frac{a-b}{a+b}\cot\tfrac{1}{2}C.$$

9. If the side a and the angles A and B of a triangle be known, prove that the side b may be found by means of the formula,

$$\log b = \log a + \log \sin B - \log \sin A.$$

Find b, having given that $a = 1000$ yards, $A = 50°$, $B = 64°$.
Ans. 1173.29 yards.

10. The minute-hand of a clock is 3 feet 6 inches in length; find how far its point will move in a quarter of an hour, it being assumed that $\pi = \frac{22}{7}$. *Ans.* 5 feet 6 inches.

IX.

(*Cambridge, Eng. 2nd Previous Exam., Dec.* 10, 1878. *Time,* 2½ *hours.*)

1. Define sine, cotangent; and prove that $\sin^2 A + \cos^2 A = 1$. Express the other trigonometrical ratios in terms of the cosine.

2. What is meant by the circular measure of an angle? How is the number of degrees in an angle found from its circular measure? How many degrees are in the unit of circular measure?

3. Prove that

$$(1) \quad \sin(180° + A) = -\sin A,$$

$$(2) \quad \tan(90° + A) = -\cot A.$$

What is the use of these equations?

4. Find the general form of all the angles whose sine is the same as $\sin \theta$.

Write down the sines of all the angles which are multiples of 30° and less than 360°.

5. Prove the following relations:

(1) $\cos(A-B)=\cos A\cos B+\sin A\sin B$,

(2) $\sin A+\sin B=2\sin\frac{1}{2}(A+B)\cos\frac{1}{2}(A-B)$,

(3) $\tan^2 A=\dfrac{1-\cos 2A}{1+\cos 2A}$.

6. Find $\cos 30°$, $\tan 45°$, $\sin 15°$.

7. If $\tan A+\sec A=2$, prove that $\sin A=\frac{3}{5}$ when A is less than 90°.

If $\sin A=\frac{4}{5}$, prove that $\tan A+\sec A=3$ when A is less than 90°.

8. Prove that $\cos 3A=4\cos^3 A-3\cos A$, and find $\tan 3A$ in terms of $\tan A$.

9. In a triangle A, B, C, whose sides are respectively a, b, c, prove that

(1) $\sin\frac{1}{2}A=\sqrt{\dfrac{(s-b)(s-c)}{bc}}$,

(2) $\dfrac{\sin A}{a}=\dfrac{\sin B}{b}=\dfrac{\sin C}{c}$.

10. Solve a triangle, having given two sides and the angle opposite one of them.

Find A, B, b, having given $a=25$, $c=24$, $C=65°59'$.

X.

(*Cambridge, Eng. 2nd Previous Exam., Dec.* 10, 1879. *Time*, 2½ *hours.*)

1. Define 1°. Assuming that $\frac{22}{7}$ is the circular measure of two right angles, express the angle $A°$ in circular measure.

2. Define the sine, secant, and cotangent of an angle, and express any two of these ratios in terms of the third.

Find the trigonometrical ratios of the angle whose cosine is $\frac{3}{5}$.

3. Prove that

(1) $\cos(180^\circ + A) = \cos(180^\circ - A)$,

(2) $\tan\ (90^\circ + A) = \cot(180^\circ - A)$.

4. Express the cosine of the difference of two angles in terms of the sines and cosines of these angles.

Prove that

[*] $$\tan^{-1}x + \tan^{-1}y = \tan^{-1}\frac{x+y}{1-xy}.$$

5. Prove the formulas:

(1) $\cos x + \cos y = 2\cos\frac{x+y}{2}\cos\frac{x-y}{2}$,

(2) $\sin\frac{1}{2}x + \cos\frac{1}{2}x = \pm\sqrt{1+\sin x}$,

(3) $\sin x(2\cos x - 1) = 2\sin\frac{1}{2}x\ \cos\frac{3}{2}x$.

6. Trace the changes in sign and magnitude of

$$\frac{2\sin\theta - \sin 2\theta}{2\sin\theta + \sin 2\theta},$$

as θ changes from 0 to 2π.

7. Express the cosine of any angle of a triangle in terms of the sides of the triangle.

If the angle opposite the side a be 60°, and if b, c be the remaining sides of the triangle, prove that

$$(a+b+c)(b+c-a) = 3bc.$$

8. Solve a triangle, having given the three sides.

Given $A = 36^\circ$, $B = 72^\circ$, and $a = 1$; solve the triangle.

9. The sides of a triangle are 2, 3, 4; find the least angle.

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[*] $\tan^{-1}x =$ arc whose tangent is x.

XI.

(*Cambridge, Eng. 2nd Previous Exam., Dec.* 10, 1880. *Time, 2½ hours.*)

1. Express in degrees, minutes, etc., (i.) the angle whose circular measure is $\frac{1}{20}\pi$; (ii.) the angle whose circular measure is 5.

If the angle subtended at the centre of a circle by the side of a regular pentagon be the unit of angular measurement, by what number is a right angle represented?

2. Find, by geometrical constructions, the cosine of 45° and the sine of 120°.

Prove that

$$(\sin 30° + \cos 30°)\,(\sin 120° + \cos 120°) = \sin 30°.$$

3. If $\csc A = 9$, find $\cot A$ and $\sec A$.

4. Prove that

$$\cos(180° + A) = -\cos A.$$

Find the value of (i.) $\cot 840°$; (ii.) $\sec 3\pi$.

5. Assuming the formula for the sine of the sum of two angles in terms of the sines and cosines of the separate angles, find (i.) $\sin 75°$; (ii.) $\sin 3A$ in terms of $\sin A$.

6. Prove the formulas:

(1) $\cos^2(A-B) - \sin^2(A+B) = \cos 2A \cos 2B$,

(2) $1 + \tan x \tan \frac{1}{2}x = \sec x$.

7. Prove that

$$\cos A + \cos B = 2\cos\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}(A-B),$$

and express $\dfrac{\cos 5\theta + \cos\theta}{\cos 5\theta - \cos\theta}$ as a single term.

8. Solve the equations:

(1) $5\tan^2 x + \sec^2 x = 7$,

(2) $\cos 5\theta + \cos 3\theta = \sqrt{2}\cos 4\theta$.

9. Prove that in any triangle $\cos A = \frac{b^2 + c^2 - a^2}{2bc}$. Obtain the formula for $\tan \frac{1}{2} A$ in terms of the sides.

10. Find an expression for the area of a triangle in terms of its sides. The lengths of the sides of a triangle are 3 feet, 5 feet, and 6 feet; what is its area?

11. Given that

$$\sin 38° 25' = 0.6213757, \quad \sin 38° 26' = 0.6216036;$$

find the angle whose sine is 0.6215000.

XII.

(*Cambridge, Eng. 2nd Previous Exam., Dec.* 10, 1881. *Time,* 2½ *hours.*)

1. Define the unit of circular measure. The ratio of the circumference of a circle to its diameter being 3.14159, find the circular measure of an angle of 126°.

2. Define the tangent, cotangent, and cosecant of an angle. Find the tangent and cotangent of an angle whose cosecant is 1.25.

3. Trace the changes in sign and magnitude of $\sin A$ as A changes from 90° to 270°.

4. Prove the following:

$$(1)\quad \tan(\pi + A) = \tan A,$$

$$(2)\quad \tan(A - B) = \frac{\tan A - \tan B}{1 + \tan A \tan B},$$

$$(3)\quad \frac{\sin A + \sin B}{\cos A - \cos B} = \cot \frac{B - A}{2}.$$

5. Determine the value of $\cos 18°$, and prove that

$$\cos 36° = \cos 60° + \cos 72°.$$

6. Show that for certain values of the angles

$$2 \cos \tfrac{1}{2} A = \sqrt{1 + \sin A} - \sqrt{1 - \sin A}.$$

Is this formula true for values of A lying between 200° and 220°? and if not, how must it be modified?

7. Prove that in any triangle, with the usual notation,

$$\cos \tfrac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}},$$

and that the area is equal to

$$\sqrt{s(s-a)(s-b)(s-c)}.$$

Show, also, that

$$\sin^2 A = \cos^2 B + \cos^2 C + 2 \cos A \cos B \cos C.$$

8. When one side of a triangle and the two adjacent angles are given, show how to solve the triangle.

Find the greatest side of the triangle, of which one side is 2183 feet, and the adjacent angles are 78° 14′ and 71° 24′.

SPHERICAL TRIGONOMETRY.

CHAPTER V.

THE RIGHT SPHERICAL TRIANGLE.

§ 45. INTRODUCTION.

The object of *Spherical Trigonometry* is to show how spherical triangles are solved. To *solve* a spherical triangle is to compute any three of its parts when the other three parts are given.

The sides of a spherical triangle are arcs of great circles. They are measured in degrees, minutes, and seconds, and therefore by the plane angles formed by radii of the sphere drawn to the vertices of the triangle. Hence, their measures are independent of the length of the radius, which may be assumed to have any convenient numerical value; as, for example, unity.

The angles of the triangle are measured by the angles made by the planes of the sides. Each angle is also measured by the number of degrees in the arc of a great circle, described from the vertex of the angle as a pole, and included between its sides.

The sides may have any values from 0° to 360°; but in this work only sides that are less than 180° will be considered. The angles may have any values from 0° to 180°.

If any two parts of a spherical triangle are either both less than 90° or both greater than 90°, they are said to be **alike in kind**; but if one part is less than 90°, and the other part greater than 90°, they are said to be **unlike in kind**.

Spherical triangles are said to be isosceles, equilateral, equiangular, right, and oblique, under the same conditions as plane triangles. A *right* spherical triangle, however, may have one, two, or three right angles.

When a spherical triangle has one or more of its sides equal to a quadrant, it is called a **quadrantal triangle.**

It is shown in Solid Geometry, that in every spherical triangle

I. *The sum of the sides is less than* 360°.

II. *The sum of the angles is greater than* 180°.

III. *If, from the vertices as poles, arcs of great circles are described, another spherical triangle is formed so related to the first triangle that the sides of each triangle are supplements of the angles opposite to them in the other triangle.*

Two such triangles are said to be *polar* with respect to each other.

Let A, B, C (Fig. 35) denote the angles of one triangle; a, b, c the sides opposite these angles respectively; and let A', B', C' and a', b', c' denote the corresponding sides and angles of the polar triangle. Then the above theorem gives the six following equations:

$$\begin{aligned} A + a' &= 180°, \\ B + b' &= 180°, \\ C + c' &= 180°, \\ A' + a &= 180°, \\ B' + b &= 180°, \\ C' + c &= 180° \end{aligned}$$

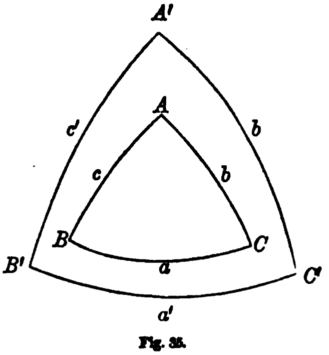

Fig. 35.

EXERCISE XIX.

1. The angles of a triangle are 70°, 80°, and 100°; find the sides of the polar triangle.

2. The sides of a triangle are 40°, 90°, and 125°; find the angles of the polar triangle.

3. Prove that the polar of a quadrantal triangle is a right triangle.

4. Prove that, if a triangle have three right angles, the sides of the triangle are quadrants.

5. Prove that, if a triangle have two right angles, the sides opposite these angles are quadrants, and the third angle is measured by the number of degrees in the opposite side.

6. How can the sides of a spherical triangle be found in units of length, when the length of the radius of the sphere is known?

7. Find the lengths of the sides of the triangle in Example 2, if the radius of the sphere is 4 feet.

§ 46. FORMULAS RELATING TO RIGHT TRIANGLES.

As is evident from § 45, Examples 4 and 5, the only kind of right triangle requiring further investigation is that which contains *only one* right angle.

Let ABC (Fig. 36) be such a right triangle, and let A, B, C denote the angles of the triangle; a, b, c, respectively, the opposite sides.

Let C be the right angle, and for the present suppose that each of the other parts is less than 90°.

Let planes be passed through the sides, intersecting in the radii OA, OB, and OC; and for the sake of simplicity let the radius of the sphere be taken equal to 1.

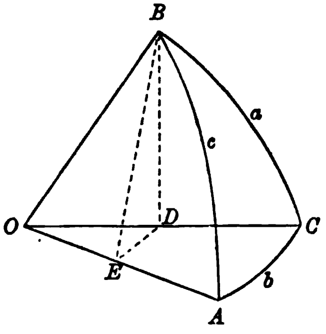

Fig. 36.

Also, let a plane perpendicular to OA be passed through B, cutting OA at E and OC at D. Join BE, BD, and DE.

BE and DE are each $\perp OA$ (Geom. § 454); therefore $\angle BED = A$. The plane BDE is $\perp$ the plane AOC (Geom. § 472); hence BD, which is the intersection of the planes BDE and BOC, is $\perp$ the plane AOC (Geom. § 475), therefore $\perp$ OC and DE. Now

$$\cos c = OE = OD \times \cos b,$$

and $OD = \cos a$.

$$\therefore \cos c = \cos a \cos b. \qquad [37]$$

$$\sin a = BD = BE \times \sin A,$$

and $BE = \sin c$.

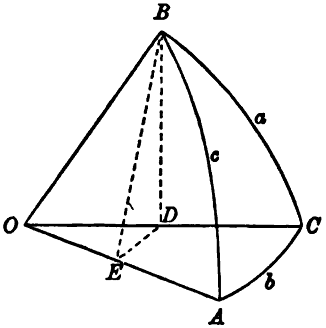

Fig. 38 (bis).

$$\left.\begin{array}{ll}\text{Therefore,} & \sin a = \sin c \sin A \\ \text{changing letters,} & \sin b = \sin c \sin B\end{array}\right\}. \qquad [38]$$

$$\begin{array}{ll}\text{Again,} & DE = BE \times \cos A, \\ \text{and also} & DE = OD \times \sin b; \\ \text{hence,} & BE \times \cos A = OD \times \sin b; \\ \text{that is,} & \sin c \cos A = \cos a \sin b; \\ \text{whence} & \cos A = \cos a \sin b \csc c.^{*}\end{array}$$

By substituting in this formula the value of $\cos a$, obtained from [37], we obtain

$$\left.\begin{array}{ll} & \cos A = \tan b \cot c \\ \text{In like manner,} & \cos B = \tan a \cot c\end{array}\right\}. \qquad [39]$$

And by substituting in the same formula the value of $\sin b$, as given in [38], we obtain

$$\left.\begin{array}{ll} & \cos A = \cos a \sin B \\ \text{In like manner,} & \cos B = \cos b \sin A\end{array}\right\}. \qquad [40]$$

$$\begin{array}{ll}\text{Also,} & BD = DE \times \tan A, \\ & BD = \sin a, \\ & DE = \cos a \sin b; \\ \text{therefore,} & \sin a = \cos a \sin b \tan A;\end{array}$$

---

[*] To avoid fractions, $\csc c$ is written in place of its equal, $\frac{1}{\sin c}$.

$$\begin{array}{ll}\text{whence,} & \left.\begin{aligned}\sin b &= \tan a \cot A\\ \sin a &= \tan b \cot B\end{aligned}\right\}. \qquad [41]\\ \text{and, similarly,} & \end{array}$$

If in [37] we substitute for $\cos a$ and $\cos b$ their values from [40], we obtain

$$\cos c = \cot A \cot B. \qquad [42]$$

In deducing these formulas, it has been assumed that all the parts of the triangle, except the right angle, are less than 90°. But the formulas also hold true when this hypothesis is not fulfilled.

Let one of the legs a be greater than 90°, and construct a figure for this case (Fig. 37) in the same manner as Fig. 36.

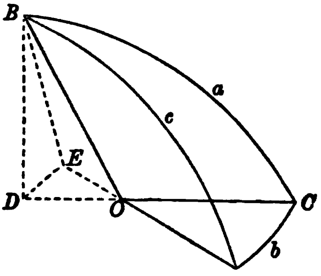

Fig. 37.

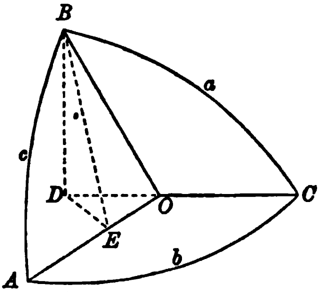

Fig. 38.

The auxiliary plane BDE will now cut both CO and AO produced beyond the centre O; and we have

$$\cos(180 - c) = OE = OD \times \cos b = \cos(180 - a) \cos b,$$

a result which reduces to [37] if we substitute $-\cos c$ in place of $\cos(180 - c)$ and $-\cos a$ in place of $\cos(180 - a)$. Likewise, the other formulas, [38]-[42], hold true in this case.

Again, suppose that both the legs a and b are greater than 90°. In this case the plane BDE (Fig. 38) will cut CO produced beyond O, and AO between A and O; and we have

$$\begin{aligned}\cos c = OE = OD \times \cos(180 - b)\\ = \cos(180 - a) \cos(180 - b)\\ = \cos a \cos b,\end{aligned}$$

a result agreeing with [37]. And the remaining formulas may be easily shown to hold true.

Like results follow in all cases; in other words, Formulas [37]–[42] are universally true.

EXERCISE XX.

1. Prove, by aid of Formula [37], that the hypotenuse of a right triangle is *less than* or *greater than* 90°, according as the two legs are *alike* or *unlike* in kind.

2. Prove, by aid of Formula [40], that in a right spherical triangle each leg and the opposite angle are always alike in kind.

3. What inferences may be drawn respecting the values of the other parts: (i.) if $c = 90°$; (ii.) if $a = 90°$; (iii.) if $c = 90°$ and $a = 90°$; (iv.) if $a = 90°$ and $b = 90°$?

Deduce from [37]–[42] the following formulas:

4. $\tan^2 \frac{1}{2} b = \tan \frac{1}{2}(c - a) \tan \frac{1}{2}(c + a)$.
5. $\tan^2(45° - \frac{1}{2} A) = \tan \frac{1}{2}(c - a) \cot \frac{1}{2}(c + a)$.
6. $\tan^2 \frac{1}{2} B = \sin(c - a) \csc(c + a)$.
7. $\tan^2 \frac{1}{2} c = -\cos(A + B) \sec(A - B)$.
8. $\tan^2 \frac{1}{2} a = \tan[\frac{1}{2}(A + B) - 45°] \tan[\frac{1}{2}(A - B) + 45°]$.

§ 47. NAPIER'S RULES.

The formulas deduced in § 46 express the relations between five parts of a right triangle, — the three sides and the two oblique angles. All these relations may be shown to follow from two very useful Rules, devised by Baron Napier, the inventor of Logarithms.

For this purpose the right angle (not entering the formulas) is left out of account, and instead of the hypotenuse and the two oblique angles, their respective *complements* are employed; so that the five parts considered by the Rules are: a, b, $co.\,c$, $co.\,A$, $co.\,B$. Any one of these parts may be called a *middle* part; and then the two parts immediately adjacent are called *adjacent* parts, and the other two are called *opposite* parts.

Rule I. *The sine of the middle part is equal to the product of the tangents of the adjacent parts.*

Rule II. *The sine of the middle part is equal to the product of the cosines of the opposite parts.*

These Rules are easily remembered by the expressions, tan. ad. and cos. op.

The correctness of these Rules may be shown by taking each of the five parts as middle part, and comparing the resulting equations with the equations contained in Formulas [37]–[42].

For example, let *co. c* be taken as middle part, then *co. A* and *co. B* are the adjacent parts, and *a* and *b* the opposite parts, — as is very plainly seen in Fig. 39, in which the order of the parts is shown by arranging them around the circumference of a circle. Then, by Napier's Rules:

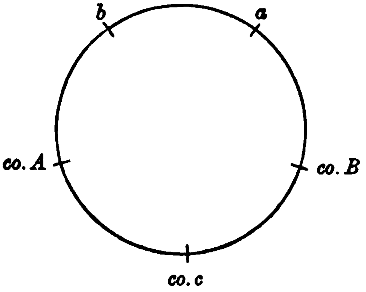

Fig. 39.

$$\sin(co.\,c) = \tan(co.\,A)\,\tan(co.\,B),$$

or

$$\cos c = \cot A\ \cot B;$$

$$\sin(co.\,c) = \cos a\ \cos b,$$

or

$$\cos c = \cos a\ \cos b;$$

results which agree with Formulas [37] and [42] respectively.

Exercise XXI.

1. Show that Napier's Rules lead to the equations contained in Formulas [38], [39], [40], and [41].

2. What will Napier's Rules become, if we take as the five parts of the triangle, the hypotenuse, the two oblique angles, and the *complements* of the two legs?

§ 48. SOLUTION OF RIGHT TRIANGLES.

By means of Formulas [37]–[42] we can solve a right triangle in all possible cases. In every case two parts besides the right angle must be given.

CASE I. *Given the two legs a and b.*
The solution is contained in Formulas [37] and [41]; viz:

$$\begin{aligned}\cos c &= \cos a \cos b,\\ \tan A &= \tan a \csc b,\\ \tan B &= \tan b \csc a.\end{aligned}$$

For example, let $a = 27^\circ\, 28'\, 36''$, $b = 51^\circ\, 12'\, 8''$; then the solution by logarithms is as follows:

$$\begin{array}{r@{\;=\;}l} \log\cos a & 9.94802\\ \log\cos b & 9.79697\\ \hline \log\cos c & 9.74499\\ c & 56^\circ\, 13'\, 40'' \end{array}$$

$$\begin{array}{r@{\;=\;}l|r@{\;=\;}l} \log\tan a & 9.71604 & \log\tan b & 10.09477\\ \log\csc b & 0.10826 & \log\csc a & 0.33593\\ \hline \log\tan A & 9.82430 & \log\tan B & 10.43070\\ A & 33^\circ\, 42'\, 50'' & B & 69^\circ\, 38'\, 54'' \end{array}$$

CASE II. *Given the hypotenuse c and the leg a.*
From Formulas [37], [38], and [39] we obtain

$$\begin{aligned}\cos b &= \cos c \sec a,\\ \sin A &= \sin a \csc c,\\ \cos B &= \tan a \cot c.\end{aligned}$$

Although two angles in general correspond to $\sin A$, one acute the other obtuse, yet in this case the indetermination is removed by the fact that A and a must be alike in kind (see Exercise XX., Example 2).

CASE III. *Given the leg a and the opposite angle A.*

By means of Formulas [38], [40], and [41], we find, that

$$\begin{aligned}\sin c &= \sin a \csc A,\\ \sin b &= \tan a \cot A,\\ \sin B &= \sec a \cos A;\end{aligned}$$

or, from [37] and [39],

$$\begin{aligned}\cos b &= \cos c \sec a,\\ \cos B &= \tan a \cot c.\end{aligned}$$

When c has been computed, b and B are determined by these values of their cosines; but, since c must be found from its sine, c may have in general two values which are supplements of one another. This case, therefore, really admits of two solutions.

CASE IV. *Given the leg a and the adjacent angle B.*

Formulas [39], [40], and [41] give

$$\begin{aligned}\tan c &= \tan a \sec B,\\ \tan b &= \sin a \tan B,\\ \cos A &= \cos a \sin B.\end{aligned}$$

CASE V. *Given the hypotenuse c and the oblique angle A.* From Formulas [38], [39], and [42] it follows that

$$\begin{aligned}\sin a &= \sin c \sin A,\\ \tan b &= \tan c \cos A,\\ \cot B &= \cos c \tan A.\end{aligned}$$

Here a is determined by $\sin a$, since a and A must be alike in kind (see Exercise XX., Example 2).

CASE VI. *Given the two oblique angles A and B.*

By means of Formulas [40] and [42] we obtain

$$\begin{aligned}\cos c &= \cot A \cot B,\\ \cos a &= \cos A \csc B,\\ \cos b &= \cos B \csc A.\end{aligned}$$

NOTE 1. In Case I. (a and b given) the formula for computing c fails to give accurate results when c is very near 0° or 180°; in this case it may be found with greater accuracy by first computing B, and then computing c, as in Case IV.

NOTE 2. In Case II. (c and a given), if b is very near 0° or 180°, it may be computed more accurately by means of the derived formula

$$\tan^2 \tfrac{1}{2} b = \tan \tfrac{1}{2}(c + a) \tan \tfrac{1}{2}(c - a).$$

And if A is so near 90° that it cannot be found accurately in the Tables, it may be computed from the derived formula

$$\tan^2(45° - \tfrac{1}{2} A) = \tan \tfrac{1}{2}(c - a) \cot \tfrac{1}{2}(c + a).$$

In like manner, when B cannot be accurately found from its cosine we may make use of the formula

$$\tan^2 \tfrac{1}{2} B = \sin(c - a) \csc(c + a).$$

NOTE 3. In Case III. (a and A given), when the formulas for the required parts do not give accurate results, we may employ the derived formulas

$$\begin{aligned}
\tan^2(45° - \tfrac{1}{2} c) &= \tan \tfrac{1}{2}(A - a) \cot \tfrac{1}{2}(A + a),\\
\tan^2(45° - \tfrac{1}{2} b) &= \sin(A - a) \csc(A + a),\\
\tan^2(45° - \tfrac{1}{2} B) &= \tan \tfrac{1}{2}(A - a) \tan \tfrac{1}{2}(A + a).
\end{aligned}$$

NOTE 4. In Case IV. (a and B given), if A is near 0° or 180°, it may be more accurately found by first computing b and then finding A.

NOTE 5. In Case V. (c and A given), if a is near 90°, it may be found by first computing b, and then computing a by means of Formula [41].

NOTE 6. In Case VI. (A and B given), for unfavorable values of the sides greater accuracy may be obtained by means of the derived formulas

$$\begin{aligned}
\tan^2 \tfrac{1}{2} c &= -\cos(A + B) \sec(A - B),\\
\tan^2 \tfrac{1}{2} a &= \tan[\tfrac{1}{2}(A + B) - 45°] \tan[45° + \tfrac{1}{2}(A - B)],\\
\tan^2 \tfrac{1}{2} b &= \tan[\tfrac{1}{2}(A + B) - 45°] \tan[45° - \tfrac{1}{2}(A - B)].
\end{aligned}$$

NOTE 7. In Cases I., IV., and V., the solution is always possible; in Case II., in order that the solution should be possible, it is necessary and sufficient that $\sin a < \sin c$; in Cases III. and VI., the conditions of possibility follow obviously from the equations employed; in Case III., it is also necessary that a and A should be alike in kind.

NOTE 8. It is easy to trace analogies between the formulas for solving right spherical triangles and those for solving right plane triangles. The former, in fact, become identical with the latter if we suppose the radius of the sphere to be infinite in length; in which case the cosines of the sides become each equal to 1, and the ratios of the sines of the sides and of the tangents of the sides must be taken as equal to the ratios of the sides themselves.

If the formula required for any case is not remembered, it is always easy to find it by means of Napier's Rules. In applying these Rules we must choose for the middle part that one of the three parts considered—the two given and the one required—which will make the other two either adjacent parts or opposite parts.

For example: *given a and B; solve the triangle.*

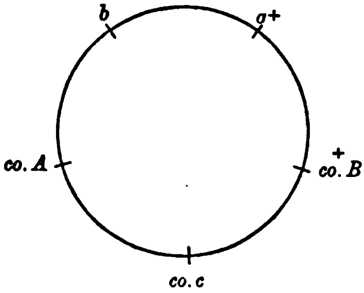

Fig. 40.

First, represent the parts as in Fig. 40, and to prevent mistakes mark each of the given parts with a cross. To find b, take a as the middle part; then b and $co.\,B$ are adjacent parts; and by Rule I.,

$$\sin a = \tan b \cot B;$$

whence, $\tan b = \sin a \tan B.$

To find c, take $co.\,B$ as middle part; then a and $co.\,c$ are adjacent parts; and by Rule I.,

$$\cos B = \tan a \cot c;$$

whence, $\tan c = \tan a \sec B.$

To find A, take $co.\,A$ as middle part; then a and $co.\,B$ are the opposite parts; and by Rule II.,

$$\cos A = \cos a \sin B.$$

In like manner, every case of a right spherical triangle may be solved.

Exercise XXII.

Solve the following right triangles, taking for the given parts in each case those printed in columns I. and II.:

	I.	II.	III.	IV.	V.
	a	*b*	*c*	*A*	*B*
1	36° 27′	43° 32′ 31″	54° 20′	46° 59′ 43.2″	57°59′19.3″
2	86° 40′	32° 40′	87° 11′ 39.8″	88° 11′ 57.8″	32°42′38.7″
3	50°	36° 54′ 49″	59° 4′ 25.7″	63° 15′ 13.1″	44°26′21.6″
4	120° 10′	150° 59′ 44″	63° 55′ 43.2″	105° 44′ 21.25″	147°19′47.14″
	c	*a*	*b*	*A*	*B*
5	55° 9′ 32″	22° 15′ 7″	51° 53′	27° 28′ 25.7″	73° 27′ 11.16″
6	23° 49′ 51″	14° 16′ 35″	19° 17′	37° 36′ 49.4″	54° 49′ 23.3″
7	44° 33′ 17″	32° 9′ 17″	32° 41′	49° 20′ 16.4″	50° 19′ 16″
8	97° 13′ 4″	132° 14′ 12″	79° 13′ 38.2″	131° 43′ 50″	81° 58′ 53.3″
	a	*A*	*c*	*b*	*B*
9	77° 21′ 50″	83° 56′ 40″	78° 53′ 20″	28° 14′ 31.8″	28° 49′ 57.4″
			101° 6′ 40″	151° 45′ 28.7″	151° 10′ 2.6″
10	77° 21′ 50″	40° 40′ 40″	impossible;	why?	
	a	*B*	*c*	*b*	*A*
11	92° 47′ 32″	50° 2′ 1″	91° 47′ 40″	50°	92° 8′ 23″
12	2° 0′ 55″	12° 40′	2° 3′ 55.7″	0° 27′ 10.2″	77° 20′ 28.4″
13	20° 20′ 20″	38° 10′ 10″	25° 14′ 38.2″	15° 16′ 50.4″	54° 35′ 16.7″
14	54° 30′	35° 30′	59° 51′ 20.8″	30° 8′ 39.2″	70° 17′ 35″
	c	*A*	*a*	*b*	*B*
15	69° 25′ 11″	54° 54′ 42″	50°	56° 50′ 49.3″	63° 25′ 4″
16	112° 48′	56° 11′ 56″	50°	127° 4′ 30″	120° 3′ 50″
17	46° 40′ 12″	37° 46′ 9″	26° 27′ 24″	39° 57′ 41.5″	62° 0′ 4″
18	118° 40′ 1″	128° 0′ 4″	136° 15′ 32.3″	48° 23′ 38.4″	58° 27′ 4.3″
	A	*B*	*a*	*b*	*c*
19	63° 15′ 12″	135° 33′ 39″	49° 59′ 56″	143° 5′ 12″	120° 55′ 34.3″
20	116° 43′ 12″	116° 31′ 25″	120° 10′ 3″	119° 59′ 46″	75° 26′ 58″
21	46° 59′ 42″	57° 59′ 17″	36° 27′	43° 32′ 30″.	54° 20′
22	90°	88° 24′ 35″	90°	88° 24′ 35″	90°

23. Define a quadrantal triangle, and show how its solution may be reduced to that of the right triangle.

24. Solve the quadrantal triangle whose sides are:

$$a = 174° 12' 49.1'', \quad b = 94° 8' 20'', \quad c = 90°.$$

25. Solve the quadrantal triangle in which

$$c = 90°, \quad A = 110° 47' 50'', \quad B = 135° 35' 34.5''.$$

26. Given in a spherical triangle A, C, and $c = 90°$; solve the triangle.

27. Given $A = 60°$, $C = 90°$, and $c = 90°$; solve the triangle.

28. Given in a right spherical triangle, $A = 42° 24' 9''$, $B = 9° 4' 11''$; solve the triangle.

29. In a right triangle, given $a = 119° 11'$, $B = 126° 54'$; solve the triangle.

30. In a right triangle, given $c = 50°$, $b = 44° 18' 39''$; solve the triangle.

31. In a right triangle, given $A = 156° 20' 30''$, $a = 65° 15' 45''$; solve the triangle.

32. If the legs a and b of a right spherical triangle are equal, prove that $\cos a = \cot A = \sqrt{\cos c}$.

33. In a right triangle prove that $\cos^2 A \times \sin^2 c = \sin (c - a) \sin (c + a)$.

34. In a right triangle prove that $\tan a \cos c = \sin b \cot B$.

35. In a right triangle prove that

$$\sin^2 A = \cos^2 B + \sin^2 a \sin^2 B.$$

36. In a right triangle prove that

$$\sin (b + c) = 2 \cos^2 \tfrac{1}{2} A \cos b \sin c.$$

37. In a right triangle prove that

$$\sin (c - b) = 2 \sin^2 \tfrac{1}{2} A \cos b \sin c.$$

38. If, in a right triangle, p denote the arc of the great circle passing through the vertex of the right angle and perpendicular to the hypotenuse, m and n the segments of the hypotenuse made by this arc adjacent to the legs a and b respectively, prove that (i.) $\tan^2 a = \tan c \tan m$, (ii.) $\sin^2 p = \tan m \tan n$.

§ 49. SOLUTION OF THE ISOSCELES SPHERICAL TRIANGLE.

If an arc of a great circle is passed through the vertex of an isosceles spherical triangle and the middle point of its base, the triangle will be divided into two symmetrical right triangles. In this way the solution of an isosceles spherical triangle may be reduced to that of a right spherical triangle.

In a similar manner the solution of a regular spherical polygon may be reduced to that of a right spherical triangle. Arcs of great circles, passed through the centre of the polygon and its vertices, divide it into a series of equal isosceles triangles; and each one of these may be divided into two equal right triangles.

EXERCISE XXIII.

1. In an isosceles spherical triangle, given the base b and the side a; find A the angle at the base, B the angle at the vertex, and h the altitude.

2. In an equilateral spherical triangle, given the side a; find the angle A.

3. Given the side a of a regular spherical polygon of n sides; find the angle A of the polygon, the distance R from the centre of the polygon to one of its vertices, and the distance r from the centre to the middle point of one of its sides.

4. Compute the dihedral angles made by the faces of the five regular polyhedrons.

5. A spherical square is a spherical quadrilateral which has equal sides and equal angles. Its two diagonals divide it into four equal right triangles. Find the angle A of the square, having given the side a.

CHAPTER VI.

THE OBLIQUE SPHERICAL TRIANGLE.

§ 51. FUNDAMENTAL FORMULAS.

Let ABC (Fig. 41) be an oblique spherical triangle, a, b, c its three sides, A, B, C the angles opposite to them, respectively.

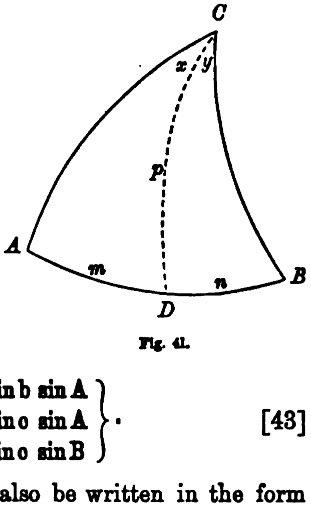

Fig. 41.

Through C draw an arc CD of a great circle, perpendicular to the side AB, meeting AB at D. For brevity let $CD=p$, $AD=m$, $BD=n$, $\angle ACD=x$, $\angle BCD=y$.

1. By § 46 [38], in the right triangles BDC and ADC,

$$\sin p = \sin a \sin B,$$

and $$\sin p = \sin b \sin A.$$

Therefore, similarly, and

$$\left.\begin{aligned} \sin a \sin B &= \sin b \sin A \\ \sin a \sin C &= \sin c \sin A \\ \sin b \sin C &= \sin c \sin B \end{aligned}\right\}. \qquad [43]$$

These equations may of course also be written in the form of proportions; as, for example,

$$\sin a : \sin b = \sin A : \sin B.$$

In Fig. 41 the arc of the great circle CD cuts the side AB within the triangle. In case it cut AB produced without the triangle, $\sin(180° - A)$, $\sin(180° - B)$, or $\sin(180° - C)$, would be employed in the above proof instead of $\sin A$, $\sin B$, or $\sin C$. These sines, however, are equal to $\sin A$, $\sin B$, and $\sin C$, respectively, so that the Formulas [43] hold true in all cases.

2. In the right triangle BDC, by § 46 [37],

$$\cos a = \cos p \cos n = \cos p \cos(c - m),$$

or (§ 32) $\quad \cos a = \cos p \cos c \cos m + \cos p \sin c \sin m.$

Now, $\quad \cos p \cos m = \cos b;$ (§ 46 [37])

whence, $\quad \cos p = \cos b \sec m,$

and $\quad \cos p \sin m = \cos b \tan m$

$\quad = \cos b \tan b \cos A$ (§ 46 [39])

$\quad = \sin b \cos A.$

Substituting these values of $\cos p \cos m$ and $\cos p \sin m$ in the value of $\cos a$, we obtain

$$\left.\begin{aligned} \cos a &= \cos b \cos c + \sin b \sin c \cos A \\ \text{and similarly, } \cos b &= \cos a \cos c + \sin a \sin c \cos B \\ \cos c &= \cos a \cos b + \sin a \sin b \cos C \end{aligned}\right\} . \qquad [44]$$

6 3. In the right triangle ADC, by § 46 [41],

$$\cos A = \cos p \sin x = \cos p \sin(C - y),$$

or (§ 32) $\quad \cos A = \cos p \sin C \cos y - \cos p \cos C \sin y.$

Now, $\quad \cos p \sin y = \cos B;$ (§ 46 [40])

whence, $\quad \cos p = \cos B \csc y,$

and $\quad \cos p \cos y = \cos B \cot y$

$\quad = \cos B \tan B \cos a$ (§ 46 [42])

$\quad = \sin B \cos a.$

Substituting these values of $\cos p \sin y$ and $\cos p \cos y$ in the value of $\cos A$, we obtain

$$\left.\begin{aligned} \cos A &= -\cos B \cos C + \sin B \sin C \cos a \\ \text{and similarly, } \cos B &= -\cos A \cos C + \sin A \sin C \cos b \\ \cos C &= -\cos A \cos B + \sin A \sin B \cos c \end{aligned}\right\} . \qquad [45]$$

Formulas [44] and [45] are also universally true; for the same equations are obtained when the arc CD cuts the side AB without the triangle.

EXERCISE XXIV.

1. What do Formulas [43] become if $A = 90°$? if $B = 90°$? if $C = 90°$? if $a = 90°$? if $A = B = 90°$? if $a = b = 90°$?

2. What does the first of [44] become if $A = 0°$? if $A = 90°$? if $A = 180°$?

3. From Formulas [44] deduce Formulas [45], by means of the relations between polar triangles (§ 45).

§ 52. FORMULAS FOR THE HALF ANGLES AND SIDES.

From the first equation of [44],

$$\cos A = \frac{\cos a - \cos b \cos c}{\sin b \sin c};$$

whence,

$$1 - \cos A = \frac{\sin b \sin c + \cos b \cos c - \cos a}{\sin b \sin c}$$

$$= \frac{\cos (b - c) - \cos a}{\sin b \sin c},$$

$$1 + \cos A = \frac{\sin b \sin c - \cos b \cos c + \cos a}{\sin b \sin c}$$

$$= \frac{\cos a - \cos (b + c)}{\sin b \sin c};$$

or, by § 34 [16] and [17], and § 35 [23],

$$\sin^2 \tfrac{1}{2} A = \sin \tfrac{1}{2} (a + b - c) \sin \tfrac{1}{2} (a - b + c) \csc b \csc c,$$

$$\cos^2 \tfrac{1}{2} A = \sin \tfrac{1}{2} (a + b + c) \sin \tfrac{1}{2} (b + c - a) \csc b \csc c.$$

Now, let $\tfrac{1}{2}(a + b + c) = s;$

whence, $\tfrac{1}{2}(b + c - a) = s - a,$

$\tfrac{1}{2}(a - b + c) = s - b,$

$\tfrac{1}{2}(a + b - c) = s - c.$

Then, by substitution and extraction of the square root,

$$\left.\begin{aligned}\sin\tfrac{1}{2}A &= \sqrt{\sin(s-b)\sin(s-c)\csc b\csc c}\\ \cos\tfrac{1}{2}A &= \sqrt{\sin s\sin(s-a)\csc b\csc c}\\ \tan\tfrac{1}{2}A &= \sqrt{\csc s\csc(s-a)\sin(s-b)\sin(s-c)}\end{aligned}\right\}. \quad [46]$$

In like manner it may be shown that

$$\begin{aligned}\sin\tfrac{1}{2}B &= \sqrt{\sin(s-a)\sin(s-c)\csc a\csc c},\\ \cos\tfrac{1}{2}B &= \sqrt{\sin s\sin(s-b)\csc a\csc c},\\ \tan\tfrac{1}{2}B &= \sqrt{\csc s\csc(s-b)\sin(s-a)\sin(s-c)}.\end{aligned}$$

$$\begin{aligned}\sin\tfrac{1}{2}C &= \sqrt{\sin(s-a)\sin(s-b)\csc a\csc b},\\ \cos\tfrac{1}{2}C &= \sqrt{\sin s\sin(s-c)\csc a\csc b},\\ \tan\tfrac{1}{2}C &= \sqrt{\csc s\csc(s-c)\sin(s-a)\sin(s-b)}.\end{aligned}$$

Again, from the first equation of [45],

$$\cos a = \frac{\cos B\cos C + \cos A}{\sin B\sin C};$$

whence,

$$1 - \cos a = \frac{\sin B\sin C - \cos B\cos C - \cos A}{\sin B\sin C},$$

$$1 + \cos a = \frac{\sin B\sin C + \cos B\cos C + \cos A}{\sin B\sin C}.$$

If we place $\tfrac{1}{2}(A+B+C)=S$, and proceed in the same manner as before, we obtain the following results:

$$\left.\begin{aligned}\sin\tfrac{1}{2}a &= \sqrt{-\cos S\cos(S-A)\csc B\csc C}\\ \cos\tfrac{1}{2}a &= \sqrt{\cos(S-B)\cos(S-C)\csc B\csc C}\\ \tan\tfrac{1}{2}a &= \sqrt{-\cos S\cos(S-A)\sec(S-B)\sec(S-C)}\end{aligned}\right\}. \quad [47]$$

And, in like manner,

$$\sin\tfrac{1}{2}\mathrm{b} = \sqrt{-\cos\mathrm{S}\cos(\mathrm{S}-\mathrm{B})\csc\mathrm{A}\csc\mathrm{C}},$$
$$\cos\tfrac{1}{2}\mathrm{b} = \sqrt{\cos(\mathrm{S}-\mathrm{A})\cos(\mathrm{S}-\mathrm{C})\csc\mathrm{A}\csc\mathrm{C}},$$
$$\tan\tfrac{1}{2}\mathrm{b} = \sqrt{-\cos\mathrm{S}\cos(\mathrm{S}-\mathrm{B})\sec(\mathrm{S}-\mathrm{A})\sec(\mathrm{S}-\mathrm{C})}.$$

$$\sin\tfrac{1}{2}\mathrm{c} = \sqrt{-\cos\mathrm{S}\cos(\mathrm{S}-\mathrm{C})\csc\mathrm{A}\csc\mathrm{B}},$$
$$\cos\tfrac{1}{2}\mathrm{c} = \sqrt{\cos(\mathrm{S}-\mathrm{A})\cos(\mathrm{S}-\mathrm{B})\csc\mathrm{A}\csc\mathrm{B}},$$
$$\tan\tfrac{1}{2}\mathrm{c} = \sqrt{-\cos\mathrm{S}\cos(\mathrm{S}-\mathrm{C})\sec(\mathrm{S}-\mathrm{A})\sec(\mathrm{S}-\mathrm{B})}.$$

§ 53. GAUSS'S EQUATIONS AND NAPIER'S ANALOGIES.

By § 31 [5],

$$\cos\tfrac{1}{2}(A+B) = \cos\tfrac{1}{2}A\cos\tfrac{1}{2}B - \sin\tfrac{1}{2}A\sin\tfrac{1}{2}B;$$

or, by substituting for $\cos\frac{1}{2}A$, $\cos\frac{1}{2}B$, $\sin\frac{1}{2}A$, $\sin\frac{1}{2}B$, their values given in § 52, and reducing,

$$\begin{aligned}\cos\tfrac{1}{2}(A+B) &= \sqrt{\frac{\sin s\sin(s-a)}{\sin b\sin c}} \times \sqrt{\frac{\sin s\sin(s-b)}{\sin a\sin c}}\\ &\quad - \sqrt{\frac{\sin(s-b)\sin(s-c)}{\sin b\sin c}} \times \sqrt{\frac{\sin(s-a)\sin(s-c)}{\sin a\sin c}}\\ &= \frac{\sin s - \sin(s-c)}{\sin c} \times \sqrt{\frac{\sin(s-a)\sin(s-b)}{\sin a\sin b}}.\end{aligned}$$

This value, by applying §§ 33 [12], 35 [21], and observing that the quantity under the radical is equal to $\sin\frac{1}{2}C$, becomes

$$\cos\tfrac{1}{2}(A+B) = \frac{2\sin\frac{1}{2}c\cos(s-\frac{1}{2}c)}{2\sin\frac{1}{2}c\cos\frac{1}{2}c}\sin\tfrac{1}{2}C,$$

which, by cancelling common factors, multiplying by $\cos\frac{1}{2}c$, and observing that $s-\frac{1}{2}c = \frac{1}{2}(a+b)$, reduces to the form

$$\cos\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}c = \cos\tfrac{1}{2}(a+b)\sin\tfrac{1}{2}C.$$

By proceeding in like manner with the values of

$$\sin\tfrac{1}{2}(A+B),\quad \cos\tfrac{1}{2}(A-B),\quad \text{and } \sin\tfrac{1}{2}(A-B),$$

three analogous equations are obtained.

The four equations,

$$\left.\begin{aligned}
\cos\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}c &= \cos\tfrac{1}{2}(a+b)\sin\tfrac{1}{2}C\\
\sin\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}c &= \cos\tfrac{1}{2}(a-b)\cos\tfrac{1}{2}C\\
\cos\tfrac{1}{2}(A-B)\sin\tfrac{1}{2}c &= \sin\tfrac{1}{2}(a+b)\sin\tfrac{1}{2}C\\
\sin\tfrac{1}{2}(A-B)\sin\tfrac{1}{2}c &= \sin\tfrac{1}{2}(a-b)\cos\tfrac{1}{2}C
\end{aligned}\right\} \qquad [48]$$

are called Gauss's Equations.

By dividing the second of Gauss's Equations by the first, the fourth by the third, the third by the first, and the fourth by the second, we obtain

$$\left.\begin{aligned}
\tan\tfrac{1}{2}(A+B) &= \frac{\cos\tfrac{1}{2}(a-b)}{\cos\tfrac{1}{2}(a+b)}\cot\tfrac{1}{2}C\\
\tan\tfrac{1}{2}(A-B) &= \frac{\sin\tfrac{1}{2}(a-b)}{\sin\tfrac{1}{2}(a+b)}\cot\tfrac{1}{2}C\\
\tan\tfrac{1}{2}(a+b) &= \frac{\cos\tfrac{1}{2}(A-B)}{\cos\tfrac{1}{2}(A+B)}\tan\tfrac{1}{2}c\\
\tan\tfrac{1}{2}(a-b) &= \frac{\sin\tfrac{1}{2}(A-B)}{\sin\tfrac{1}{2}(A+B)}\tan\tfrac{1}{2}c
\end{aligned}\right\}. \qquad [49]$$

These equations are called Napier's Analogies.

In the first equation the factors $\cos\tfrac{1}{2}(a-b)$ and $\cot\tfrac{1}{2}C$ are always positive; therefore, $\tan\tfrac{1}{2}(A+B)$ and $\cos\tfrac{1}{2}(a+b)$ must always have like signs. Hence, if $a+b<180°$, and therefore $\cos\tfrac{1}{2}(a+b)>0$, then, also, $\tan\tfrac{1}{2}(A+B)>0$, and therefore $A+B<180°$. Similarly, it follows that if $a+b>180°$, then, also, $A+B>180°$. If $a+b=180°$, and therefore $\cos\tfrac{1}{2}(a+b)=0$, then $\tan\tfrac{1}{2}(A+B)=\infty$; whence $\tfrac{1}{2}(A+B)=90°$, and $A+B=180°$.

Conversely, it may be shown from the third equation, that $a+b$ is less than, greater than, or equal to 180°, according as $A+B$ is less than, greater than, or equal to 180°.

§ 54. CASE I.

Given two sides, a and b, and the included angle C.

The angles A and B may be found by the first two of Napier's Analogies; viz.:

$$\tan \tfrac{1}{2}(A+B) = \frac{\cos \frac{1}{2}(a-b)}{\cos \frac{1}{2}(a+b)} \cot \tfrac{1}{2} C.$$

$$\tan \tfrac{1}{2}(A-B) = \frac{\sin \frac{1}{2}(a-b)}{\sin \frac{1}{2}(a+b)} \cot \tfrac{1}{2} C.$$

After A and B have been found, the side c may be found by [43]; but it is better to use for this purpose Gauss's Equations, because they involve functions of the same angles that occur in working Napier's Analogies. Any one of the equations may be used; for example, from the first we have

$$\cos \tfrac{1}{2} c = \frac{\cos \frac{1}{2}(a+b)}{\cos \frac{1}{2}(A+B)} \sin \tfrac{1}{2} C.$$

EXAMPLE. $a = 73° 58' 54''$, $b = 38° 45' \ 0''$, $C = 46° 33' 41''$, therefore, $\tfrac{1}{2}(a-b) = 17° 36' 57''$, $\tfrac{1}{2}(a+b) = 56° 21' 57''$, $\tfrac{1}{2}C = 23° 16' 50.5''$

$$\begin{array}{ll}
\log \cos \frac{1}{2}(a-b) & = 9.97914 \\
\log \sec \frac{1}{2}(a+b) & = 0.25658 \\
\log \cot \frac{1}{2} C & = 0.36626 \\
\hline
\log \tan \frac{1}{2}(A+B) & = 0.60198 \\
\hline
\log \sec \frac{1}{2}(A+B) & = 0.61547 \\
\log \cos \frac{1}{2}(a+b) & = 9.74342 \\
\log \sin \frac{1}{2} C & = 9.59686 \\
\hline
\log \cos \frac{1}{2} c & = 9.95575 \\
\frac{1}{2} c & = 25° 25' 40''
\end{array}$$

$$\begin{array}{ll}
\log \sin \frac{1}{2}(a-b) & = 9.48092 \\
\log \csc \frac{1}{2}(a+b) & = 0.07956 \\
\log \cot \frac{1}{2} C & = 0.36626 \\
\hline
\log \tan \frac{1}{2}(A-B) & = 9.92674 \\
\hline
\frac{1}{2}(A+B) & = 75° 57' 40.7'' \\
\frac{1}{2}(A-B) & = 40° 11' 25.6'' \\
A & = 116° \ 9' \ 6.3'' \\
B & = 35° 46' 15.1'' \\
c & = 50° 51' 20''
\end{array}$$

If the side c only is desired, it may be found from [44], without previously computing A and B. But the Formulas [44] are not adapted to logarithmic work. Instead of changing them to forms suitable for logarithms, we may use the following method, which leads to the same results, and has the advantage that, in applying it, nothing has to be remembered except Napier's Rules:

Make the triangle (Fig. 42), as in § 51, equal to the sum (or the difference) of two right triangles. For this purpose, through B (or A, but *not* C) draw an arc of a great circle perpendicular to AC, cutting AC at D. Let $BD = p$, $CD = m$, $AD = n$; and mark with crosses the given parts.

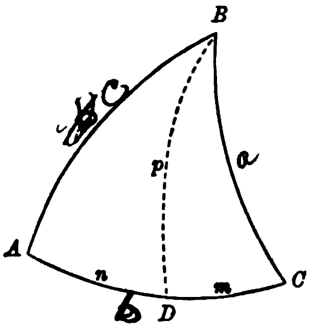

Fig. 42.

By Rule I.,

$$\cos C = \tan m \cot a,$$

whence $\tan m = \tan a \cos C$.

By Rule II.,

$$\cos a = \cos m \cos p, \text{ whence } \cos p = \cos a \sec m.$$
$$\cos c = \cos n \cos p, \text{ whence } \cos p = \cos c \sec n.$$

Therefore, $\cos c \sec n = \cos a \sec m$;

or, since $n = b - m$, $\cos c = \cos a \sec m \cos (b - m)$.

It is evident that c may be computed, with the aid of logarithms, from the two equations

$$\tan m = \tan a \cos C,$$
$$\cos c = \cos a \sec m \cos (b - m).$$

EXAMPLE. Given $a = 97° 30' 20''$, $b = 55° 12' 10''$, $C = 39° 58'$; find c.

$\log \tan a = 0.88025 (n)$	$\log \cos a = 9.11602 (n)$
$\log \cos C = 9.88447$	$\log \cos (b - m) = 9.85286$
$\log \tan m = 0.76472 (n)$	$\log \sec m = 0.77103 (n)$
$m = 99° 45' 14''$	$\log \cos c = 9.73991$
$b - m = -44° 33' 4''$	$c = 56° 40' 20''$

EXERCISE XXV.

1. Write formulas for finding, by Napier's Rules, the side a when b, c, and A are given, and for finding the side b when a, c, and B are given.

2. Given $a = 88^\circ\, 12'\, 20''$, $b = 124^\circ\, 7'\, 17''$, $C = 50^\circ\, 2'\, 1''$; find $A = 63^\circ\, 15'\, 11''$, $B = 132^\circ\, 17'\, 59''$, $c = 59^\circ\, 4'\, 18''$.

3. Given $a = 120^\circ\, 55'\, 35''$, $b = 88^\circ\, 12'\, 20''$, $C = 47^\circ\, 42'\, 1''$; find $A = 129^\circ\, 58'\, 3''$, $B = 63^\circ\, 15'\, 9''$, $c = 55^\circ\, 52'\, 40''$.

4. Given $b = 63^\circ\, 15'\, 12''$, $c = 47^\circ\, 42'\, 1''$, $A = 59^\circ\, 4'\, 25''$; find $B = 88^\circ\, 12'\, 24''$, $C = 55^\circ\, 52'\, 42''$, $a = 50^\circ\, 1'\, 40''$.

5. Given $b = 69^\circ\, 25'\, 11''$, $c = 109^\circ\, 46'\, 19''$, $A = 54^\circ\, 54'\, 42''$; find $B = 56^\circ\, 11'\, 57''$, $C = 123^\circ\, 21'\, 12''$, $a = 67^\circ\, 13'$.

§ 55. CASE II.

Given two angles, A and B, and the included side c.

The sides a and b may be found by the third or fourth of Napier's Analogies,

$$\tan \tfrac{1}{2}(a+b) = \frac{\cos \frac{1}{2}(A-B)}{\cos \frac{1}{2}(A+B)} \tan \tfrac{1}{2} c,$$

$$\tan \tfrac{1}{2}(a-b) = \frac{\sin \frac{1}{2}(A-B)}{\sin \frac{1}{2}(A+B)} \tan \tfrac{1}{2} c,$$

and then the angle C may be found by one of Gauss's equations; as, for instance, the second, which gives

$$\cos \tfrac{1}{2} C = \frac{\sin \frac{1}{2}(A+B)}{\cos \frac{1}{2}(a-b)} \cos \tfrac{1}{2} c.$$

EXAMPLE.

$$\begin{aligned} A &= 107^\circ\, 47'\, 7'' \\ B &= 38^\circ\, 58'\, 27'' \\ c &= 51^\circ\, 41'\, 14'' \end{aligned}$$

$$\begin{aligned} \log\cos \tfrac{1}{2}(A-B) &= 9.91648 \\ \log\sec \tfrac{1}{2}(A+B) &= 0.54359 \\ \log\tan \tfrac{1}{2} c &= 9.68517 \\ \hline \log\tan \tfrac{1}{2}(a+b) &= 0.14524 \\ \hline \log\sin \tfrac{1}{2}(A+B) &= 9.98146 \\ \log\sec \tfrac{1}{2}(a-b) &= 0.01703 \\ \log\cos \tfrac{1}{2} c &= 9.95423 \\ \hline \log\cos \tfrac{1}{2} C &= 9.95272 \\ \tfrac{1}{2} C &= 26^\circ\, 14'\, 52.5'' \end{aligned}$$

$$\begin{aligned} \tfrac{1}{2}(A-B) &= 34^\circ\, 24'\, 20'' \\ \tfrac{1}{2}(A+B) &= 73^\circ\, 22'\, 47'' \\ \tfrac{1}{2} c &= 25^\circ\, 50'\, 37'' \end{aligned}$$

$$\begin{aligned} \log\sin \tfrac{1}{2}(A-B) &= 9.75208 \\ \log\csc \tfrac{1}{2}(A+B) &= 0.01854 \\ \log\tan \tfrac{1}{2} c &= 9.68517 \\ \hline \log\tan \tfrac{1}{2}(a-b) &= 9.45579 \\ \hline \tfrac{1}{2}(a+b) &= 54^\circ\, 24'\, 24.4'' \\ \tfrac{1}{2}(a-b) &= 15^\circ\, 56'\, 25.6'' \end{aligned}$$

$$\left\{ \begin{aligned} a &= 70^\circ\, 20'\, 50'' \\ b &= 38^\circ\, 27'\, 59'' \\ C &= 52^\circ\, 29'\, 45'' \end{aligned} \right.$$

If the angle C alone is wanted, the best way is to decompose the triangle into two right triangles, and then apply Napier's Rules, as in Case I., when the side c alone is desired.

Let (Fig. 43) $\angle ABD = x$, $\angle CBD = y$, $BD = p$; then,

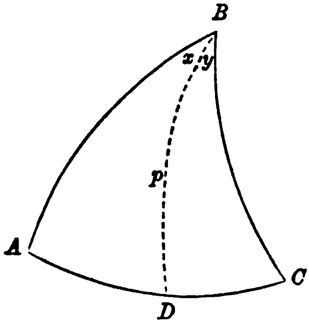

Fig. 43.

By Rule I.,

$$\cos c = \cot x \cot A,$$

whence $\cot x = \tan A \cos c$.

By Rule II.,

$$\cos A = \cos p \sin x,$$

whence $\cos p = \cos A \csc x$.

$$\cos C = \cos p \sin y,$$

whence $\cos p = \cos C \csc y$.

Therefore,

$$\cos C = \cos A \csc x \sin y = \cos A \csc x \sin (B - x).$$

It is clear that C may be computed from the equations

$$\cot x = \tan A \cos c,$$

$$\cos C = \cos A \csc x \sin (B - x).$$

EXAMPLE. Given $A = 35° 46' 15''$, $B = 115° 9' 7''$, $c = 51° 2'$; find C.

$\log \tan A = 9.85760$	$\log \cos A = 9.90992$
$\log \cos c = 9.79856$	$\log \sin (B - x) = 9.88122$
$\log \cot x = 9.65616$	$\log \csc x = 0.04055$
$x = 65° 37' 35''$	$\log \cos C = 9.83099$
$B - x = 49° 31' 32''$	$C = 47° 20' 30''$

EXERCISE XXVI.

1. What are the formulas for computing A when B, C, and a are given; and for computing B when A, C, and b are given?

2. Given $A = 26° 58' 46''$, $B = 39° 45' 10''$, $c = 154° 46' 48''$; find $a = 37° 14' 10''$, $b = 121° 28' 10''$, $C = 161° 22' 11''$.

3. Given $A = 128° 41' 49''$, $B = 107° 33' 20''$, $c = 124° 12' 31''$; find $a = 125° 41' 44''$, $b = 82° 47' 34''$, $C = 127° 22'$.

4. Given $B = 153° 17' 6''$, $C = 78° 43' 36''$, $a = 86° 15' 15''$; find $b = 152° 43' 51''$, $c = 88° 12' 21''$, $A = 78° 15' 48''$.

5. Given $A = 125° 41' 44''$, $C = 82° 47' 35''$, $b = 52° 37' 57''$; find $a = 128° 31' 46''$, $c = 107° 33' 20''$, $B = 55° 47' 40''$.

§ 56. CASE III.

Given two sides a and b, and the angle A opposite to one of them.

The angle B is found from [43], whence we have

$$\sin B = \sin A \sin b \csc a.$$

When B has been found, C and c may be found from the fourth and the second of Napier's Analogies, from which we obtain

$$\tan \tfrac{1}{2} c = \frac{\sin \frac{1}{2}(A+B)}{\sin \frac{1}{2}(A-B)} \tan \tfrac{1}{2}(a-b),$$

$$\cot \tfrac{1}{2} C = \frac{\sin \frac{1}{2}(a+b)}{\sin \frac{1}{2}(a-b)} \tan \tfrac{1}{2}(A-B).$$

The third and the first of Napier's Analogies may also be used for the same purpose.

NOTE 1. Since B is determined from its sine, the problem in general has two solutions; and, moreover, in case $\sin B > 1$, the problem is impossible. By geometric construction it may be shown, as in the corresponding case in Plane Trigonometry, under what conditions the problem really has two solutions, one solution, and no solution. But in practical applications a general knowledge of the shape of the triangle is known beforehand; so that it is easy to see, without special investigation, which solution (if any) corresponds to the circumstances of the question.

It can be shown that there are two solutions, when

$$A < 90°, \quad a + b < 180°, \quad \text{and } a < b,$$

or, when

$$A > 90°, \quad a + b > 180°, \quad \text{and } a > b.$$

NOTE 2. The side c or the angle C may be computed, without first finding B, by means of the formulas

$$\tan m = \cos A \tan b, \text{ and } \cos(c - m) = \cos a \times \sec b \times \cos m,$$
$$\cot x = \tan A \cos b, \text{ and } \cos(C - x) = \cot a \times \tan b \times \cos x.$$

These formulas may be obtained by resolution of the triangle into right triangles, and applying Napier's Rules; m is equal to that part of the side c included between the foot of the perpendicular from C and the vertex A, and x is equal to the corresponding portion of the angle C.

EXAMPLE. Given $a = 57°36'$, $b = 31°12'$, $A = 104°25'30''$.

In this case $A > 90°$,
and $a + b < 180°$;
therefore, $A + B < 180°$;
hence, $B < 90°$,
and only one solution.

$\log \sin A = 9.98609$
$\log \sin b = 9.71435$
$\log \csc a = 0.07349$
$\log \sin B = 9.77393$
$B = 36° 27' 20''$

$a + b = 88° 50'$
$a - b = 26° 26'$
$A + B = 140° 51' 53''$
$A - B = 67° 59' 7''$
$\log \sin \frac{1}{2}(A + B) = 9.97416$
$\log \csc \frac{1}{2}(A - B) = 0.25252$
$\log \tan \frac{1}{2}(a - b) = 9.37080$
$\log \tan \frac{1}{2}c = 9.59748$
$\frac{1}{2}c = 21° 35' 38''$
$c = 43° 11' 16''$

$\frac{1}{2}(a + b) = 44° 25'$
$\frac{1}{2}(a - b) = 13° 13'$
$\frac{1}{2}(A + B) = 70° 26' 25''$
$\frac{1}{2}(A - B) = 33° 59' 5''$
$\log \sin \frac{1}{2}(a + b) = 9.84502$
$\log \csc \frac{1}{2}(a - b) = 0.64086$
$\log \tan \frac{1}{2}(A - B) = 9.82873$
$\log \cot \frac{1}{2}C = 0.31461$
$\frac{1}{2}C = 25° 51' 15''$
$C = 51° 42' 30''$

EXERCISE XXVII.

1. Given $a = 73° 49' 38''$, $b = 120° 53' 35''$, $A = 88° 52' 42''$; find $B = 116° 42' 30''$, $c = 120° 57' 27''$, $C = 116° 47' 4''$.

2. Given $a = 150° 57' 5''$, $b = 134° 15' 54''$, $A = 144° 22' 42''$; find $B_1 = 120° 47' 45''$, $c_1 = 55° 42' 8''$, $C_1 = 97° 42' 55.4''$;
$B_2 = 59° 12' 15''$, $c_2 = 23° 57' 17.4''$, $C_2 = 29° 8' 39''$.

3. Given $a = 79° 0' 54.5''$, $b = 82° 17' 4''$, $A = 82° 9' 25.8''$; find $B = 90°$, $c = 45° 12' 19''$, $C = 45° 44'$.

4. Given $a = 30° 52' 36.6''$, $b = 31° 9' 16''$, $A = 87° 34' 12''$; show that the triangle is impossible.

§ 57. CASE IV.

Given two angles A and B, and the side a opposite to one of them.

The side b is found from [43], whence

$$\sin b = \sin a \sin B \csc A.$$

The values of c and C may then be found by means of Napier's Analogies, the fourth and second of which give

$$\tan \tfrac{1}{2} c = \frac{\sin \frac{1}{2}(A+B)}{\sin \frac{1}{2}(A-B)} \tan \tfrac{1}{2}(a-b),$$

$$\cot \tfrac{1}{2} C = \frac{\sin \frac{1}{2}(a+b)}{\sin \frac{1}{2}(a-b)} \tan \tfrac{1}{2}(A-B).$$

NOTE 1. In this case, also, an unknown part is found from its sine; and it may be shown that, under certain conditions, the problem is impossible, or that it admits of two solutions. In practice, the ambiguity is usually removed by the circumstances of the question. If $\sin b > 1$ the problem of course is impossible; and it may be shown that there are two solutions, when

$a < 90°$, $A + B < 180°$, and $A < B$,
or $a > 90°$, $A + B > 180°$, and $A > B$.

NOTE 2. By proceeding as indicated in Case III., Note 2, formulas for computing c or C, independent of the side b, may be found; viz.:

$\tan m = \tan a \cos B$, and $\sin(c - m) = \cot A \tan B \sin m$,
$\cot x = \cos a \tan B$, and $\sin(C - x) = \cos A \sec B \sin x$.

In these formulas $m = BD$, $x = \angle BCD$, D being the foot of the perpendicular from the vertex C.

EXERCISE XXVIII.

1. Given $A = 110° 10'$, $B = 133° 18'$, $a = 147° 5' 32''$; find $b = 155° 5' 18''$, $c = 33° 1' 36''$, $C = 70° 20' 40''$.

2. Given $A = 113° 39' 21''$, $B = 123° 40' 18''$, $a = 65° 39' 46''$; find $b = 124° 7' 20''$, $c = 159° 53' 2''$, $C = 159° 43' 35''$.

3. Given $A = 100° 2' 11.3''$, $B = 98° 30' 28''$, $a = 95° 20' 38.7''$; find $b = 90°$, $c = 147° 41' 43''$, $C = 148° 5' 33''$.

4. Given $A = 24° 33' 9''$, $B = 38° 0' 12''$, $a = 65° 20' 13''$; show that the triangle is impossible.

§ 58. CASE V.

Given the three sides, a, b, and c.

The angles are computed by means of Formulas [46], and the corresponding formulas for the angles B and C.

The formulas for the tangent are in general to be preferred.

If we multiply the equation

$$\tan \tfrac{1}{2} A = \sqrt{\csc s \, \csc(s-a) \sin(s-b) \sin(s-c)}$$

by the equation $\qquad 1 = \dfrac{\sin(s-a)}{\sin(s-a)}$,

and put

$$\sqrt{\csc s \, \sin(s-a) \sin(s-b) \sin(s-c)} = \tan r,$$

and also make analogous changes in the equations for $\tan \tfrac{1}{2} B$ and $\tan \tfrac{1}{2} C$, we obtain

$$\begin{aligned} \tan \tfrac{1}{2} A &= \tan r \ \csc(s-a), \\ \tan \tfrac{1}{2} B &= \tan r \ \csc(s-b), \\ \tan \tfrac{1}{2} C &= \tan r \ \csc(s-c), \end{aligned}$$

which are the most convenient formulas to employ when all three angles have to be computed.

EXAMPLE 1.

$a = 50° 54' 32''$	$\log \csc s = 0.00448$
$b = 37° 47' 18''$	$\log \csc(s-a) = 0.28978$
$c = 74° 51' 50''$	$\log \sin(s-b) = 9.84171$
$2s = 163° 33' 40''$	$\log \sin(s-c) = 9.08072$
$s = 81° 46' 50''$	$2 \overline{)19.21669}$
$s-a = 30° 52' 18''$	$\log \tan \tfrac{1}{2} A = 9.60835$
$s-b = 43° 59' 32''$	$\tfrac{1}{2} A = 22° 5' 20''$
$s-c = 6° 55' 0''$	$A = 44° 10' 40''$

EXAMPLE 2.

$a = 124° 12' 31''$
$b = 54° 18' 16''$
$c = 97° 12' 25''$
$2s = 275° 43' 12''$

$\log \sin (s - a) = 9.37293$
$\log \sin (s - b) = 9.99725$
$\log \sin (s - c) = 9.81390$
$\log \csc s = 0.17331$
$\log \tan^2 r = 9.35739$
$\log \tan r = 9.67870$

$s = 137° 51' 36''$
$s - a = 13° 39' 5''$
$s - b = 83° 33' 20''$
$s - c = 40° 39' 11''$

$\log \tan \frac{1}{2} A = 0.30577$
$\log \tan \frac{1}{2} B = 9.68145$
$\log \tan \frac{1}{2} C = 9.86480$
$\frac{1}{2} A = 63° 41' 3.8''$
$\frac{1}{2} B = 25° 39' 5.6''$
$\frac{1}{2} C = 36° 13' 20.1''$
$A = 127° 22' 7''$
$B = 51° 18' 11''$
$C = 72° 26' 40''$

EXERCISE XXIX.

1. Given $a = 120° 55' 35''$, $b = 59° 4' 25''$, $c = 106° 10' 22''$; find $A = 116° 44' 49''$, $B = 63° 15' 14''$, $C = 91° 7' 21''$.

2. Given $a = 50° 12' 4''$, $b = 116° 44' 48''$, $c = 129° 11' 42''$; find $A = 59° 4' 28''$, $B = 94° 23' 12''$, $C = 120° 4' 52''$.

3. Given $a = 131° 35' 4''$, $b = 108° 30' 14''$, $c = 84° 46' 34''$; find $A = 132° 14' 21''$, $B = 110° 10' 40''$, $C = 99° 42' 24''$.

4. Given $a = 20° 16' 38''$, $b = 56° 19' 40''$, $c = 66° 20' 44''$; find $A = 20° 9' 54''$, $B = 55° 52' 31''$, $C = 114° 20' 17''$.

§ 59. CASE VI.

Given the three angles, A, B, and C.

The sides are computed by means of Formulas [47], and the corresponding formulas for the angles B and C. The formulas for the tangents are in general to be preferred.

If we multiply the equation

$$\tan \tfrac{1}{2} a = \sqrt{- \cos S \cos (S - A) \sec (S - B) \sec (S - C)}$$

by the equation $\qquad 1 = \dfrac{\sec (S - A)}{\sec (S - A)}$,

and put

$$\sqrt{- \cos S \sec (S - A) \sec (S - B) \sec (S - C)} = \tan R,$$

and also make analogous changes in the equations for $\tan\frac{1}{2}b$ and $\tan\frac{1}{2}c$, we obtain

$$\begin{aligned}\tan\tfrac{1}{2}a &= \tan R\cos(S-A),\\ \tan\tfrac{1}{2}b &= \tan R\cos(S-B),\\ \tan\tfrac{1}{2}c &= \tan R\cos(S-C),\end{aligned}$$

which are the most convenient formulas to use in case all three angles have to be computed.

EXAMPLE I.

$$\begin{aligned}A &= 220^\circ\\ B &= 130^\circ\\ C &= 150^\circ\\ \hline 2S &= 500^\circ\\ S &= 250^\circ\\ S-A &= 30^\circ\\ S-B &= 120^\circ\\ S-C &= 100^\circ\end{aligned}$$

$$\begin{aligned}\log\cos S &= 9.53405\ (n)\\ \log\cos(S-A) &= 9.93753\\ \log\sec(S-B) &= 0.30103\ (n)\\ \log\sec(S-C) &= 0.76033\ (n)\\ &\ 2\overline{)0.53294}\\ \log\tan\tfrac{1}{2}a &= 0.26647\\ \tfrac{1}{2}a &= 61^\circ 34'\ 6''\\ a &= 123^\circ\ 8' 12''\end{aligned}$$

NOTE. Here the effect, as regards algebraic sign, of three negative factors, is cancelled by the negative sign belonging to the whole fraction.

EXAMPLE II.

$$\begin{aligned}A &= 20^\circ\ 9' 56''\\ B &= 55^\circ 52' 32''\\ C &= 114^\circ 20' 14''\\ \hline 2S &= 190^\circ 22' 42''\end{aligned}$$

$$\begin{aligned}S &= 95^\circ 11' 21''\\ S-A &= 75^\circ\ 1' 25''\\ S-B &= 39^\circ 18' 49''\\ S-C &= -19^\circ\ 8' 53''\end{aligned}$$

$$\begin{aligned}\log\cos S &= 8.95638\ (n)\\ \log\sec(S-A) &= 0.58768\\ \log\sec(S-B) &= 0.11143\\ \log\sec(S-C) &= 0.02472\\ \hline \log\tan^2 R &= 9.68021\\ \log\tan R &= 9.84010\end{aligned}$$

$$\begin{aligned}\log\tan\tfrac{1}{2}a &= 9.25242\\ \log\tan\tfrac{1}{2}b &= 9.72867\\ \log\tan\tfrac{1}{2}c &= 9.81538\\ \hline \tfrac{1}{2}a &= 10^\circ\ 8' 18.9''\\ \tfrac{1}{2}b &= 28^\circ\ 9' 50.4''\\ \tfrac{1}{2}c &= 33^\circ 10' 21.3''\\ \hline a &= 20^\circ 16' 38''\\ b &= 56^\circ 19' 41''\\ c &= 66^\circ 20' 43''\end{aligned}$$

EXERCISE XXX.

1. Given $A=130^\circ$, $B=110^\circ$, $C=80^\circ$; find $a=139^\circ 21' 22''$, $b=126^\circ 57' 52''$, $c=56^\circ 51' 48''$.

2. Given $A=59^\circ 55' 10''$, $B=85^\circ 36' 50''$, $C=59^\circ 55' 10''$; find $a=$ ~~128° 42' 20''~~, $b=64^\circ 2' 47''$, $c=$ ~~128° 42' 20''.~~

51°17' 31'' 51° 17' 31''

3. Given $A = 102^\circ\, 14'\, 12''$, $B = 54^\circ\, 32'\, 24''$, $C = 89^\circ\, 5'\, 46''$; find $a = 104^\circ\, 25'\, 9''$, $b = 53^\circ\, 49'\, 25''$, $c = 97^\circ\, 44'\, 24''$.

4. Given $A = 4^\circ\, 23'\, 35''$, $B = 8^\circ\, 28'\, 20''$, $C = 172^\circ\, 17'\, 56''$; find $a = 31^\circ\, 9'\, 11''$, $b = 84^\circ\, 18'\, 23''$, $c = 115^\circ\, 9'\, 56''$.

§ 60. Area of a Spherical Triangle.

I. *When the three angles A, B, C, are given.*

Let R = radius of sphere,
E = the spherical excess $= A + B + C - 180^\circ$,
F = area of triangle;

then, by Solid Geometry,

$$F = \frac{E}{180^\circ}\pi R^2. \qquad [50]$$

II. *When the three sides a, b, c, are given.*

A formula for computing the area is deduced as follows: From the first of [48],

$$\frac{\cos\frac{1}{2}(A+B)}{\cos(90^\circ - \frac{1}{2}C)} = \frac{\cos\frac{1}{2}(a+b)}{\cos\frac{1}{2}c};$$

whence, by the Theory of Proportions,

$$\frac{\cos\frac{1}{2}(A+B) - \cos(90^\circ - \frac{1}{2}C)}{\cos\frac{1}{2}(A+B) + \cos(90^\circ - \frac{1}{2}C)} = \frac{\cos\frac{1}{2}(a+b) - \cos\frac{1}{2}c}{\cos\frac{1}{2}(a+b) + \cos\frac{1}{2}c}. \qquad \text{(a)}$$

Now, in § 35, the division of [23] by [22] gives

$$\frac{\cos A - \cos B}{\cos A + \cos B} = -\tan\tfrac{1}{2}(A+B)\tan\tfrac{1}{2}(A-B), \qquad \text{(b)}$$

in which for A and B we may substitute any other two angular magnitudes, as for example, $\frac{1}{2}(A+B)$ and $(90 - \frac{1}{2}C)$, or $\frac{1}{2}(a+b)$ and $\frac{1}{2}c$.

If we use in place of A and B the values $\frac{1}{2}(A+B)$ and $(90^\circ - \frac{1}{2}C)$, the first side of equation (b) becomes

$$\frac{\cos\frac{1}{2}(A+B) - \cos(90^\circ - \frac{1}{2}C)}{\cos\frac{1}{2}(A+B) + \cos(90^\circ - \frac{1}{2}C)};$$

and the second side becomes

$$-\tan\tfrac{1}{2}(\tfrac{1}{2}A+\tfrac{1}{2}B+90^\circ-\tfrac{1}{2}C)\tan\tfrac{1}{2}(\tfrac{1}{2}A+\tfrac{1}{2}B-90^\circ+\tfrac{1}{2}C);$$

or,

$$-\tan\tfrac{1}{4}(A+B-C+180^\circ)\tan\tfrac{1}{4}(A+B+C-180^\circ).$$

If we remember that $E=A+B+C-180^\circ$, and observe that

$$\begin{aligned}\tan\tfrac{1}{4}(A+B-C+180^\circ)&=\tan\tfrac{1}{4}(360^\circ-2C+A+B+C-180^\circ)\\&=\tan\tfrac{1}{4}(360^\circ-2C+E)\\&=\tan[90^\circ-\tfrac{1}{4}(2C-E)]\\&=\cot\tfrac{1}{4}(2C-E),\end{aligned}$$

it will be evident that equation (b) may be written

$$\frac{\cos\frac{1}{2}(A+B)-\cos(90^\circ-\frac{1}{2}C)}{\cos\frac{1}{2}(A+B)+\cos(90^\circ-\frac{1}{2}C)}=-\cot\tfrac{1}{4}(2C-E)\tan\tfrac{1}{4}E. \qquad \text{(c)}$$

If we substitute, in equation (b), for A and B, the values $\frac{1}{2}(a+b)$ and $\frac{1}{2}c$, and also substitute s for $\frac{1}{2}(a+b+c)$ and $s-c$ for $\frac{1}{2}(a+b-c)$, equation (b) will become

$$\frac{\cos\frac{1}{2}(a+b)-\cos\frac{1}{2}c}{\cos\frac{1}{2}(a+b)+\cos\frac{1}{2}c}=-\tan\tfrac{1}{2}s\tan\tfrac{1}{2}(s-c). \qquad \text{(d)}$$

Comparing (a), (c), and (d), we obtain

$$\cot\tfrac{1}{4}(2C-E)\tan\tfrac{1}{4}E=\tan\tfrac{1}{2}s\tan\tfrac{1}{2}(s-c). \qquad \text{(e)}$$

By beginning with the second equation of [48], and treating it in the same way, we obtain as the result,

$$\tan\tfrac{1}{4}(2C-E)\tan\tfrac{1}{4}E=\tan\tfrac{1}{2}(s-a)\tan\tfrac{1}{2}(s-b). \qquad \text{(f)}$$

By taking the product of (e) and (f), we obtain the elegant formula,

$$\tan^2\tfrac{1}{4}\mathrm{E}=\tan\tfrac{1}{2}\mathrm{s}\tan\tfrac{1}{2}(\mathrm{s}-\mathrm{a})\tan\tfrac{1}{2}(\mathrm{s}-\mathrm{b})\tan\tfrac{1}{2}(\mathrm{s}-\mathrm{c}), \qquad [51]$$

which is known as l'Huilier's Formula.

By means of it E may be computed from the three sides, and then the area of the triangle may be found by [50].

III. *In all other cases*, the area may be found by first solving the triangle so far as to obtain the angles or the sides, whichever may be more convenient, and then applying [50] or [51].

EXAMPLE I.

$$\begin{aligned} A &= 102^\circ\,14'\,12'' \\ B &= 54^\circ\,32'\,24'' \\ C &= 89^\circ\,5'\,46'' \\ \hline &\ 245^\circ\,52'\,22'' \\ E &= 65^\circ\,52'\,22'' \\ &= 237142'' \\ 180^\circ &= 648000'' \end{aligned}$$

$$\begin{aligned} \log E &= 5.37501 \\ {}^*\log\frac{\pi}{648000} &= 4.68557 - 10 \\ \hline &\ 0.06058 \\ F &= 1.1497\,R^2 \end{aligned}$$

EXAMPLE II.

$$\begin{aligned} a &= 133^\circ\,26'\,19'' \\ b &= 64^\circ\,50'\,53'' \\ c &= 144^\circ\,13'\,45'' \\ \hline 2s &= 342^\circ\,30'\,57'' \\ \hline s &= 171^\circ\,15'\,28.5'' \\ s-a &= 37^\circ\,49'\,9.5'' \\ s-b &= 106^\circ\,24'\,35.5'' \\ s-c &= 27^\circ\,1'\,43.5'' \end{aligned}$$

$$\begin{aligned} \tfrac{1}{2}s &= 85^\circ\,37'\,44'' \\ \tfrac{1}{2}(s-a) &= 18^\circ\,54'\,35'' \\ \tfrac{1}{2}(s-b) &= 53^\circ\,12'\,18'' \\ \tfrac{1}{2}(s-c) &= 13^\circ\,30'\,52'' \\ \hline \log\tan\tfrac{1}{2}s &= 1.11669 \\ \log\tan\tfrac{1}{2}(s-a) &= 9.53474 \\ \log\tan\tfrac{1}{2}(s-b) &= 0.12612 \\ \log\tan\tfrac{1}{2}(s-c) &= 9.38083 \\ \hline \log\tan^2\tfrac{1}{4}E &= 0.15838 \\ \log\tan\tfrac{1}{4}E &= 0.07919 \\ \tfrac{1}{4}E &= 50^\circ\,11'\,43'' \\ E &= 200^\circ\,46'\,52'' \end{aligned}$$

EXERCISE XXXI.

1. Given $A = 84^\circ\,20'\,19''$, $B = 27^\circ\,22'\,40''$, $C = 75^\circ\,33'$; find $E = 26159''$, $F = 0.12685\,R^2$.

2. Given $a = 69^\circ\,15'\,6''$, $b = 120^\circ\,42'\,47''$, $c = 159^\circ\,18'\,33''$; find $E = 216^\circ\,40'\,18''$.

3. Given $a = 33^\circ\,1'\,45''$, $b = 155^\circ\,5'\,18''$, $C = 110^\circ\,10'$; find $E = 133^\circ\,48'\,53''$.

4. Find the spherical excess of a triangle on the earth's surface (regarded as spherical), if each side of the triangle is equal to 1°.

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* See Wentworth & Hill's Tables, page 20.

CHAPTER VII.

APPLICATIONS OF SPHERICAL TRIGONOMETRY.

§ 61. PROBLEM.

To reduce an angle measured in space to the horizon.

Let O (Fig. 44) be the position of the observer on the ground, $AOB = h$ the angle measured in space (for example, the angle between the tops of two church spires), OA' and OB' the projections of the sides of the angle upon the horizontal plane HR, $AOA' = m$ and $BOB' = n$ the angles of inclination of OA and OB respectively to the horizon. Required the angle $A'OB' = x$ made by the projections on the horizon.

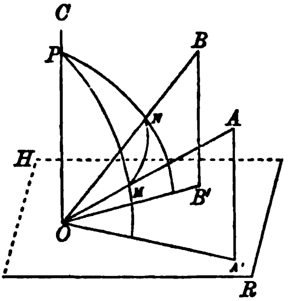


Fig. 44.

The planes of the angles of inclination AOA' and BOB' produced intersect in the line OC, which is perpendicular to the horizontal plane (Geom. § 475).

From O as a centre describe a sphere, and let its surface cut the ~~edges of~~ the trihedral angle $O\text{-}ABC$ in the points M, N, and P. In the spherical triangle MNP the three sides $MN = h$, $MP = 90^\circ - m$, $NP = 90^\circ - n$, are known, and the spherical angle P is equal to the required angle x.

From § 52 we obtain

$$\cos \tfrac{1}{2} x = \sqrt{\cos s \cos (s - h) \sec m \sec n},$$

where $\tfrac{1}{2}(m + n + h) = s$.

§ 62. PROBLEM.

To find the distance between two places on the earth's surface (regarded as spherical), given the latitudes of the places and the difference of their longitudes.

Let M and N (Fig. 45) be the places; then their distance MN is an arc of the great circle passing through the places. Let P be the pole, AB the equator. The arcs MR and NS are the latitudes of the places, and the arc RS, or the angle MPN, is the difference of their longitudes. Let $MR = a$, $NS = b$, $RS = l$; then in the spherical triangle MNP two sides, $MP = 90 - a$, $NP = 90 - b$, and the included angle $MPN = l$, are given, and we have (from § 54)

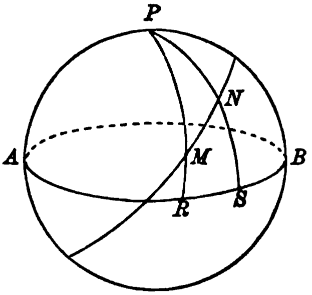


Fig. 45.

$$\tan m \quad = \cot a \cos l,$$
$$\cos MN = \sin a \sec m \sin (b + m).$$

From these equations first find m, then the arc MN, and then reduce MN to geographical miles, of which there are 60 in each degree.

§ 63. THE CELESTIAL SPHERE.

The **Celestial Sphere** is an imaginary sphere of indefinite radius, upon the concave surface of which all the heavenly bodies appear to be situated.

The **Celestial Equator,** or **Equinoctial,** is the great circle in which the plane of the earth's equator produced intersects the surface of the celestial sphere.

The **Poles** of the equinoctial are the points where the earth's axis produced cuts the surface of the celestial sphere.

The **Celestial Meridian** of an observer is the great circle in which the plane of his terrestrial meridian produced meets the surface of the celestial sphere.

Hour Circles, or **Circles of Declination,** are great circles passing through the poles, and perpendicular to the equinoctial.

The **Horizon** of an observer is the great circle in which a plane tangent to the earth's surface, at the place where he is, meets the surface of the celestial sphere.

The **Zenith** of an observer is that pole of his horizon which is exactly above his head.

Vertical Circles are great circles passing through the zenith of an observer, and perpendicular to his horizon.

The vertical circle passing through the east and west points of the horizon is called the **Prime Vertical;** that passing through the north and south points coincides with the celestial meridian.

The **Ecliptic** is a great circle of the celestial sphere, apparently traversed by the sun in one year from west to east, in consequence of the motion of the earth around the sun.

The **Equinoxes** are the points where the ecliptic cuts the equinoctial. They are distinguished as the *Vernal* equinox and the *Autumnal* equinox; the sun in his annual journey passes through the former on March 21, and through the latter on September 21.

Circles of Latitude are great circles passing through the poles of the ecliptic, and perpendicular to the plane of the ecliptic.

The angle which the ecliptic makes with the equinoctial is called the **obliquity** of the ecliptic; it is equal to 23°27′, nearly, and is often denoted by the letter e.

These definitions are illustrated in Figs. 46 and 47. In Fig. 46, $AVBU$ is the equinoctial, P and P' its poles, $NPZS$ the celestial meridian of an observer, $NESW$ his horizon, Z his zenith, M a star, PMP' the hour circle passing through the star, $ZMDZ'$ the vertical through the star.

In Fig. 47, *AVBU* represents the equinoctial, *EVFU* the ecliptic, *P* and *Q* their respective poles, *V* the vernal equinox, *U* the autumnal equinox, *M* a star, *PMR* the hour circle through the star, *QMT* the circle of latitude through the star, and $\angle TVR = e$.

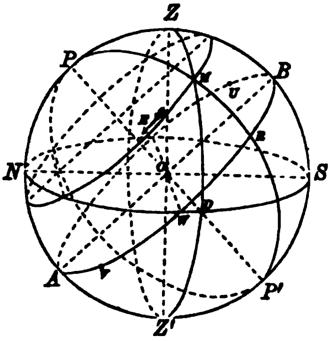


Fig. 46.

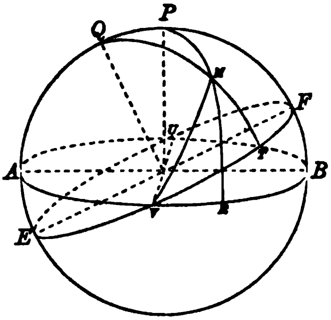


Fig. 47.

The earth's diurnal motion causes all the heavenly bodies to appear to rotate from east to west at the uniform rate of 15° per hour. If in Fig. 46 we conceive the observer placed at the centre *O*, and his zenith, horizon, and celestial meridian fixed in position, and all the heavenly bodies rotating around *PP′* as an axis from east to west at the rate of 15° per hour, we form a correct idea of the apparent diurnal motions of these bodies. When the sun or a star in its diurnal motion crosses the meridian, it is said to make a *transit* across the meridian; when it passes across the part *NWS* of the horizon, it is said to *set;* and when it passes across the part *NES*, it is said to *rise* (the effect of refraction being here neglected). Each star, as *M*, describes daily a small circle of the sphere parallel to the equinoctial, and called the **Diurnal Circle** of the star. The diurnal circle is the smaller the nearer the star is to the pole; and if there were stars at the poles *P* and *P′*, they would have no diurnal motion. To an observer north of the equator, the north pole P is *elevated* above the horizon (as shown in Fig. 46); to an observer south of the equator, the south pole P' is the elevated pole.

§ 64. SPHERICAL CO-ORDINATES.

Several systems of fixing the position of a star on the surface of the celestial sphere at any instant are in use. In each system a great circle and its pole are taken as standards of reference, and the position of the star is determined by means of two quantities called its *spherical co-ordinates.*

I. *If the horizon and the zenith* are chosen, the co-ordinates of the star are called its altitude and its azimuth.

The **Altitude** of a star is its angular distance, measured on a vertical circle, above the horizon. The complement of the altitude is called the **Zenith Distance.**

The **Azimuth** of a star is the angle at the zenith formed by the meridian of the observer and the vertical circle passing through the star, and is measured therefore by an arc of the horizon. It is usually reckoned from the north point of the horizon in north latitudes, and from the south point in south latitudes; and east or west according as the star is east or west of the meridian.

II. *If the equinoctial and its pole* are chosen, then the position of the star may be fixed by means of its declination and its hour angle.

The **Declination** of a star is its angular distance from the equinoctial, measured on an hour circle. The angular distance of the star, measured on the hour circle, *from the elevated pole* is called its **Polar Distance.**

The declination of a star, like the latitude of a place on the earth's surface, may be either north or south; but, in practical problems, while latitude is always to be considered positive, declination, if of a different name from the latitude, must be regarded as *negative.*

If the declination is negative, the polar distance is equal numerically to 90° + the declination.

The **Hour Angle** of a star is the angle at the pole formed by the meridian of the observer and the hour circle passing through the star. On account of the diurnal rotation, it is constantly changing at the rate of 15° per hour. Hour angles are reckoned from the celestial meridian, positive towards the west, and negative towards the east.

III. The *equinoctial and its pole* being still retained, we may employ as the co-ordinates of the star its declination and its right ascension.

The **Right Ascension** of a star is the arc of the equinoctial included between the vernal equinox and the point where the hour circle of the star cuts the equinoctial Right ascension is reckoned from the vernal equinox eastward from 0° to 360°.

IV. *The ecliptic and its pole* may be taken as the standards of reference. The co-ordinates of the star are then called its latitude and its longitude.

The **Latitude** of a star is its angular distance from the ecliptic measured on a circle of latitude.

The **Longitude** of a star is the arc of the ecliptic included between the vernal equinox and the point where the circle of latitude through the star cuts the ecliptic.

In problems it is useful to employ certain letters to denote these various co-ordinates. For a star M (Fig. 46), let

$l =$ latitude of the observer,
$h = DM$ = the altitude of the star,
$z = ZM$ = the zenith distance of the star,
$a = \angle PZM =$ the azimuth of the star,
$t = \angle ZPM =$ the hour angle of the star,
$d = RM$ = the declination of the star,
$p = PM$ = the polar distance of the star,
$r = VR$ = the right ascension of the star,
$u = MT$ (Fig. 47) = the latitude of the star,
$v = VT$ (Fig. 47) = the longitude of the star.

In many problems, a simple way of representing the magnitudes involved, is to project the sphere on the plane of the horizon, as shown in Fig. 48.

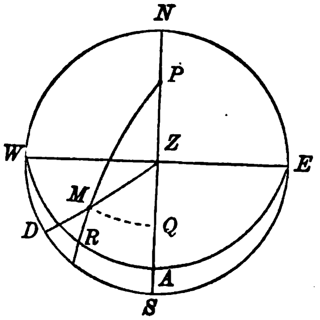


Fig. 48.

$NESW$ is the horizon, Z the zenith, NZS the meridian, WZE the prime vertical, WAE the equinoctial projected on the plane of the horizon, P the elevated pole, M a star, DM its altitude, ZM its zenith distance, $\angle PZM$ its azimuth, MR its declination, PM its polar distance, $\angle ZPM$ its hour angle.

§ 65. THE ASTRONOMICAL TRIANGLE.

The triangle ZPM (Figs. 46 and 48) is often called the *astronomical triangle*, on account of its importance in problems in Nautical Astronomy.

The side PZ is equal to the complement of the latitude of the observer. For (Fig. 46) the angle ZOB between the zenith of the observer and the celestial equator is obviously equal to his latitude, and the angle POZ is the complement of ZOB. The arc NP being the complement of PZ, it follows that *the altitude of the elevated pole is equal to the latitude of the place of observation.*

The triangle ZPM then (however much it may vary in shape for different positions of the star M), always contains the following five magnitudes:

PZ = co-latitude of observer = $90° - l$,
ZM = zenith distance of star = z,
PZM = azimuth of star = a,
PM = polar distance of star = p,
ZPM = hour angle of star = t.

A very simple relation exists between the hour angle of the sun and the local (apparent) time of day. Since the hourly rate at which the sun appears to move from east to west is 15°, and it is apparent noon when the sun is on the meridian of a place, it is evident that if hour angle $= 0°, 15°, -15°$, etc., time of day is noon, 1 o'clock P.M., 11 o'clock A.M., etc.

In general, if t denote the absolute value of the hour angle,

$$\text{time of day} = \frac{t}{15}\text{ P.M., or } 12 - \frac{t}{15}\text{ A.M.},$$

according as the sun is west or east of the meridian.

§ 66. PROBLEM.

Given the latitude of the observer and the altitude and azimuth of a star, to find its declination and its hour angle.

In the triangle ZPM (Fig. 48),

given $PZ = 90° - l = \text{co-latitude}$,
$ZM = 90° - h = \text{co-altitude}$,
$\angle PZM = a = \text{azimuth}$;
to find $PM = 90° - d = \text{polar distance}$,
$\angle ZPM = t = \text{hour angle}$.

Draw $MQ \perp NS$, and put $ZQ = m$,
then, if $a < 90°$, $PQ = 90° - (l + m)$,
and if $a > 90°$, $PQ = 90° - (l - m)$;

and, by Napier's Rules,

$$\cos a = \pm \tan m \tan h,$$
$$\sin d = \cos PQ \cos MQ,$$
$$\sin h = \cos m \cos MQ;$$

whence,

$$\tan m = \pm \cot h \cos a,$$
$$\sin d = \sin h \sin(l \pm m) \sec m,$$

in which the $-$ sign is to be used if $a > 90°$. The hour angle may then be found by means of [43], whence we have

$$\sin t = \sin a \cos h \sec d.$$

§ 67. PROBLEM.

To find the hour angle of a heavenly body when its declination, its altitude, and the latitude of the place are known.

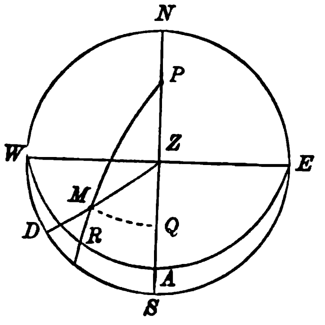


Fig. 49.

In the triangle ZPM (Fig. 49),

given
$$PZ = 90° - l,$$
$$PM = 90° - d = p,$$
$$ZM = 90° - h;$$

required
$$\angle ZPM = t.$$

If, in the first formula of [46],

$$\sin \tfrac{1}{2} A = \sqrt{\sin(s-b) \sin(s-c) \csc b \csc c},$$

we put

$$A = t, \quad a = 90° - h, \quad b = p, \quad c = 90° - l,$$

we have

$$s - b = 90° - \tfrac{1}{2}(l + p + h), \quad s - c = \tfrac{1}{2}(l + p - h),$$

and the formula becomes

$$\sin \tfrac{1}{2} t = \pm \left[\cos \tfrac{1}{2}(l + p + h) \sin \tfrac{1}{2}(l + p - h) \sec l \csc p\right]^{\frac{1}{2}}$$

in which the − sign is to be taken when the body is east of the meridian.

If the body is the sun, how can the local time be found when the hour angle has been computed? (See § 65.)

§ 68. PROBLEM.

To find the altitude and azimuth of a celestial body, when its declination, its hour angle, and the latitude of the place are known.

In the triangle ZPM (Fig. 49),

given $PZ = 90° - l,$

$PM = 90° - d = p,$

$\angle ZPM = t;$

required $ZM = 90° - h,$

$\angle PZM = a.$

Here there are given two sides and the included angle. Placing $PQ = m$, and proceeding as in § 66, we obtain

$$\tan m = \cot d \cos t,$$
$$\sin h = \sin(l + m) \sin d \sec m,$$
$$\tan a = \sec(l + m) \tan t \sin m,$$

in the last of which formulas a must be marked E. or W., to agree with the hour angle.

§ 69. PROBLEM.

To find the latitude of the place when the altitude of a celestial body, its declination, and its hour angle are known.

In the triangle ZPM (Fig. 49),

given $ZM = 90° - h,$

$PM = 90° - d,$

$\angle ZPM = t;$

required $PZ = 90° - l.$

Let $PQ = m, \quad ZQ = n.$

Then, by Napier's Rules,

$$\cos t = \tan m \tan d,$$
$$\sin h = \cos n \cos MQ,$$
$$\sin d = \cos m \cos MQ;$$

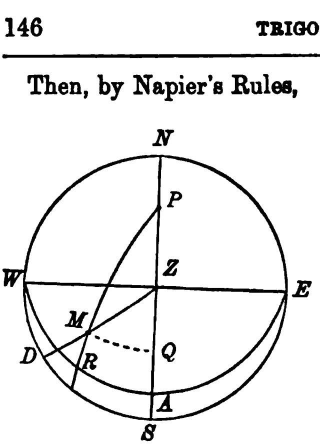


Fig. 49.

whence,

$$\tan m = \cot d \cos t,$$
$$\cos n = \cos m \sin h \csc d,$$

and it is evident from the figure that

$$l = 90^\circ - (m \pm n),$$

in which the sign + or the sign − is to be taken according as the body and the elevated pole are *on the same side* of the prime vertical or *on opposite sides.*

In fact, both values of l may be possible for the same altitude and hour angle; but, unless n is very small, the two values will differ largely from each other, so that the observer has no difficulty in deciding which of them should be taken.

§ 70. Problem.

Given the declination, the right ascension of a star, and the obliquity of the ecliptic, to find the latitude and the longitude of the star.

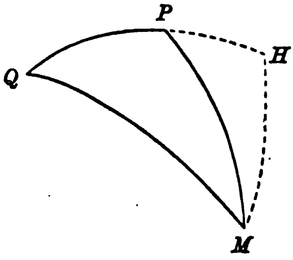


Fig. 50.

Let M (Fig. 50) be the star, P be the pole of the equinoctial, and Q the pole of the ecliptic.

Then, on the triangle PMQ,

given $PQ = e = 23^\circ 27'$,

$$PM = 90^\circ - d,$$
$$\angle MPQ = 90^\circ + r \text{ (see Fig. 47)};$$

required $QM = 90^\circ - u$, and $\angle PQM = 90^\circ - v$ (see Fig. 47).

In this case, also, two sides and the included angle are given. Draw $MH \perp PQ$, and meeting it produced at H, and let $PH = n$.

By Napier's Rules,

$$\begin{aligned}
&\sin r = \tan n \tan d,\\
&\sin u = \cos(e + n) \cos MH,\\
&\sin d = \cos n \cos MH,\\
&\sin(e + n) = \tan v \tan MH,\\
&\sin n = \tan r \tan MH;
\end{aligned}$$

whence,

$$\begin{aligned}
&\tan n = \cot d \sin r,\\
&\sin u = \sin d \cos(e + n) \sec n,\\
&\tan v = \tan r \sin(e + n) \csc n.
\end{aligned}$$

To avoid obtaining u from its sine we may proceed as follows:

From the last two equations we have, by division,

$$\sin u = \tan v \cot(e + n) \sin d \cot r \tan n.$$

By taking MH as middle part, successively, in the triangles MQH and MPH, we obtain

$$\cos u \cos v = \cos d \cos r;$$

whence, $\cos u = \sec v \cos d \cos r.$

From these values of $\sin u$ and $\cos u$ we obtain, by division,

$$\tan u = \sin v \cot(e + n) \tan d \csc r \tan n.$$

From the relation

$$\sin r = \tan n \tan d,$$

it follows that $\tan d \csc r \tan n = 1.$

Therefore $\tan u = \sin v \cot(e + n),$

a formula by which u can be easily found after v has been computed.

EXERCISE XXXII.

1. Find the dihedral angle made by the lateral faces of a regular ten-sided pyramid; given the angle $A = 18°$, made at the vertex by two adjacent lateral edges.

2. Through the foot of a rod which makes the angle A with a plane, a straight line is drawn in the plane. This line makes the angle B with the projection of the rod upon the plane. What angle does this line make with the rod?

3. Find the volume V of an oblique parallelopipedon; given the three unequal edges a, b, c, and the three angles l, m, n, which the edges make with one another.

4. The continent of Asia has nearly the shape of an equilateral triangle, the vertices being the East Cape, Cape Romania, and the Promontory of Baba. Assuming each side of this triangle to be 4800 geographical miles, and the earth's radius to be 3440 geographical miles, find the area of the triangle: (i.) regarded as a plane triangle; (ii.) regarded as a spherical triangle.

5. A ship sails from a harbor in latitude l, and keeps on the arc of a great circle. Her *course* (or angle between the direction in which she sails and the meridian) at starting is a. Find where she will cross the equator, her course at the equator, and the distance she has sailed.

6. Two places have the same latitude l, and their distance apart, measured on an arc of a great circle, is d. How much greater is the arc of the parallel of latitude between the places than the arc of the great circle? Compute the results for $l = 45°$, $d = 90°$.

7. The shortest distance d between two places and their latitudes l and l' are known. Find the difference between their longitudes.

8. Given the latitudes and longitudes of three places on the earth's surface, and also the radius of the earth; show how to find the area of the spherical triangle formed by arcs of great circles passing through the places.

9. The distance between Paris and Berlin (that is, the arc of a great circle between these places) is equal to 472 geographical miles. The latitude of Paris is 48° 30′ 13″; that of Berlin, 52° 30′ 16″. When it is noon at Paris what time is it at Berlin?

NOTE. Owing to the apparent motion of the sun, the local time over the earth's surface at any instant varies at the rate of one hour for 15° of longitude; and the more *easterly* the place, the *later* the local time.

10. The altitude of the pole being 45°, I see a star on the horizon and observe its azimuth to be 45°; find its polar distance.

11. Given the latitude l of the observer, and the declination d of the sun; find the local time (apparent solar time) of sunrise and sunset, and also the azimuth of the sun at these times (refraction being neglected). When and where does the sun rise on the longest day of the year (at which time $d = +23° 27′$) in Boston ($l = 42° 21′$), and what is the length of the day from sunrise to sunset? Also, find when and where the sun rises in Boston on the shortest day of the year (when $d = -23° 27′$), and the length of this day.

12. When is the solution of the problem in Example 11 impossible, and for what places is the solution impossible?

13. Given the latitude of a place and the sun's declination; find his altitude and azimuth at 6 o'clock A.M. (neglecting refraction). Compute the results for the longest day of the year at Munich ($l = 48° 9′$).

14. How does the altitude of the sun at 6 A.M. *on a given day* change as we go from the equator to the pole? At what time of the year is it a maximum *at a given place?* (Given $\sin h = \sin l \sin d$.)

15. Given the latitude of a place north of the equator, and the declination of the sun; find the time of day when the sun bears due east and due west. Compute the results for the longest day at St. Petersburg ($l = 59° 56′$).

16. Apply the general result in Example 15 ($\cos t = \cot l \tan d$) to the case when the days and nights are equal in length (that is, when $d = 0°$). Why can the sun in summer never be due east before 6 A.M., or due west after 6 P.M.? How does the time of bearing due east and due west change with the declination of the sun? Apply the general result to the cases where $l < d$ and $l = d$. What does it become at the north pole?

17. Given the sun's declination and his altitude when he bears due east; find the latitude of the observer.

18. At a point O in a horizontal plane MN a staff OA is fixed, so that its angle of inclination AOB with the plane is equal to the latitude of the place, 51° 30′ N., and the direction OB is due north. What angle will OB make with the shadow of OA on the plane, at 1 P.M., when the sun is on the equinoctial?

19. What is the direction of a wall in latitude 52° 30′ N. which casts no shadow at 6 A.M. on the longest day of the year?

20. At a certain place the sun is observed to rise exactly in the north-east point on the longest day of the year; find the latitude of the place.

21. Find the latitude of the place at which the sun sets at 10 o'clock on the longest day.

22. To what does the general formula for the hour angle, in § 67, reduce when (i.) $h = 0°$, (ii.) $l = 0°$ and $d = 0°$, (iii.) l or $d = 90°$?

23. What does the general formula for the azimuth of a celestial body, in § 68, become when $t = 90° = 6$ hours?

24. Show that the formulas of § 69, if $t = 90°$, lead to the equation $\sin l = \sin h \csc d$; and that if $d = 0°$, they lead to the equation $\cos l = \sin h \sec t$.

25. Given latitude of place 52° 30′ 16″, declination of star 38°, its hour angle 28° 17′ 15″; find its altitude.

26. Given latitude of place 51° 19′ 20″, polar distance of star 67° 59′ 5′, its hour angle 15° 8′ 12″; find its altitude and its azimuth.

27. Given the declination of a star 7° 54′, its altitude 22° 45′ 12″, its azimuth 129° 45′ 37″; find its hour angle and the latitude of the observer.

28. Given the longitude v of the sun, and the obliquity of the ecliptic $e = 23° 27'$; find the declination d, and the right ascension r.

29. Given the obliquity of the ecliptic $e = 23° 27'$, the latitude of a star 51°, its longitude 315°; find its declination and its right ascension.

30. Given the latitude of place 44° 50′ 14″, the azimuth of a star 138° 58′ 43″, and its hour angle 20°; find its declination.

31. Given latitude of place 51° 31′ 48″, altitude of sun west of the meridian 35° 14′ 27″, its declination +21° 27′; find the local apparent time.

32. Given latitude of place l, the polar distance p of a star, and its altitude h; find its azimuth a.

APPENDIX.

FORMULAS.

$$\left.\begin{array}{ll} \textbf{1.} & \sin^2 A+\cos^2 A=1.\\ \textbf{2.} & \tan A=\dfrac{\sin A}{\cos A}.\\ \textbf{3.} & \left\{\begin{array}{l}\sin A\times\csc A=1.\\ \cos A\times\sec A=1.\\ \tan A\times\cot A=1.\end{array}\right.\end{array}\right\}\text{§ 5.}$$

$$\left.\begin{array}{ll} \textbf{4.} & \sin(x+y)=\sin x\cos y+\cos x\sin y.\\ \textbf{5.} & \cos(x+y)=\cos x\cos y-\sin x\sin y.\\ \textbf{6.} & \tan(x+y)=\dfrac{\tan x+\tan y}{1-\tan x\tan y}.\\ \textbf{7.} & \cot(x+y)=\dfrac{\cot x\cot y-1}{\cot x+\cot y}.\end{array}\right\}\text{§ 31.}$$

$$\left.\begin{array}{ll} \textbf{8.} & \sin(x-y)=\sin x\cos y-\cos x\sin y.\\ \textbf{9.} & \cos(x-y)=\cos x\cos y+\sin x\sin y.\\ \textbf{10.} & \tan(x-y)=\dfrac{\tan x-\tan y}{1+\tan x\tan y}.\\ \textbf{11.} & \cot(x-y)=\dfrac{\cot x\cot y+1}{\cot y-\cot x}.\end{array}\right\}\text{§ 32.}$$

$$\left.\begin{array}{ll} \textbf{12.} & \sin 2x=2\sin x\cos x.\\ \textbf{13.} & \cos 2x=\cos^2 x-\sin^2 x.\end{array}\right\}\text{§ 33.}$$

$$\left.\begin{array}{ll}\textbf{14.} & \tan 2x = \dfrac{2\tan x}{1-\tan^2 x}. \\[2ex] \textbf{15.} & \cot 2x = \dfrac{\cot^2 x - 1}{2\cot x}. \end{array}\right\}\ \S\ 33.$$

$$\left.\begin{array}{ll}\textbf{16.} & \sin \tfrac{1}{2} z = \pm\sqrt{\dfrac{1-\cos z}{2}}. \\[2ex] \textbf{17.} & \cos \tfrac{1}{2} z = \pm\sqrt{\dfrac{1+\cos z}{2}}. \\[2ex] \textbf{18.} & \tan \tfrac{1}{2} z = \pm\sqrt{\dfrac{1-\cos z}{1+\cos z}}. \\[2ex] \textbf{19.} & \cot \tfrac{1}{2} z = \pm\sqrt{\dfrac{1+\cos z}{1-\cos z}}. \end{array}\right\}\ \S\ 34.$$

$$\left.\begin{array}{ll}\textbf{20.} & \sin A + \sin B = 2\sin\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}(A-B). \\[2ex] \textbf{21.} & \sin A - \sin B = 2\cos\tfrac{1}{2}(A+B)\sin\tfrac{1}{2}(A-B). \\[2ex] \textbf{22.} & \cos A + \cos B = 2\cos\tfrac{1}{2}(A+B)\cos\tfrac{1}{2}(A-B). \\[2ex] \textbf{23.} & \cos A - \cos B = -2\sin\tfrac{1}{2}(A+B)\sin\tfrac{1}{2}(A-B). \\[2ex] \textbf{24.} & \dfrac{\sin A + \sin B}{\sin A - \sin B} = \dfrac{\tan\tfrac{1}{2}(A+B)}{\tan\tfrac{1}{2}(A-B)}. \end{array}\right\}\ \S\ 35.$$

25. $\dfrac{a}{b} = \dfrac{\sin A}{\sin B}.$ § 36.

26. $a^2 = b^2 + c^2 - 2bc\cos A.$ § 37.

27. $\dfrac{a-b}{a+b} = \dfrac{\tan\tfrac{1}{2}(A-B)}{\tan\tfrac{1}{2}(A+B)}.$ § 38.

28. $\sin\tfrac{1}{2}A = \sqrt{\dfrac{(s-b)(s-c)}{bc}}.$ § 43.

$$\left.\begin{array}{ll}
\textbf{29.} & \cos\tfrac{1}{2}A = \sqrt{\dfrac{s(s-a)}{bc}}. \\[2ex]
\textbf{30.} & \tan\tfrac{1}{2}A = \sqrt{\dfrac{(s-b)(s-c)}{s(s-a)}}. \\[2ex]
\textbf{31.} & \sqrt{\dfrac{(s-a)(s-b)(s-c)}{s}} = r. \\[2ex]
\textbf{32.} & \tan\tfrac{1}{2}A = \dfrac{r}{s-a}.
\end{array}\right\}\ \S\ 43.$$

$$\left.\begin{array}{ll}
\textbf{33.} & F = \tfrac{1}{2}ac\sin B. \\[1ex]
\textbf{34.} & F = \sqrt{s(s-a)(s-b)(s-c)}. \\[1ex]
\textbf{35.} & F = \dfrac{abc}{4R}. \\[1ex]
\textbf{36.} & F = \tfrac{1}{2}r(a+b+c) = rs.
\end{array}\right\}\ \S\ 44.$$

SPHERICAL TRIGONOMETRY.

$$\left.\begin{array}{ll}
\textbf{37.} & \cos c = \cos a \cos b. \\[1ex]
\textbf{38.} & \left\{\begin{array}{l} \sin a = \sin c \sin A. \\ \sin b = \sin c \sin B. \end{array}\right. \\[2ex]
\textbf{39.} & \left\{\begin{array}{l} \cos A = \tan b \cot c. \\ \cos B = \tan a \cot c. \end{array}\right. \\[2ex]
\textbf{40.} & \left\{\begin{array}{l} \cos A = \cos a \sin B. \\ \cos B = \cos b \sin A. \end{array}\right. \\[2ex]
\textbf{41.} & \left\{\begin{array}{l} \sin b = \tan a \cot A. \\ \sin a = \tan b \cot B. \end{array}\right. \\[2ex]
\textbf{42.} & \cos c = \cot A \cot B.
\end{array}\right\}\ \S\ 46.$$

$$\textbf{43.}\ \left\{\begin{array}{l}
\sin a \sin B = \sin b \sin A. \\
\sin a \sin C = \sin c \sin A. \\
\sin b \sin C = \sin c \sin B.
\end{array}\right\}\ \S\ 51.$$

$$\text{44.}\ \begin{cases} \cos a = \cos b \cos c + \sin b \sin c \cos A. \\ \cos b = \cos a \cos c + \sin a \sin c \cos B. \\ \cos c = \cos a \cos b + \sin a \sin b \cos C. \end{cases}$$

$$\text{45.}\ \begin{cases} \cos A = -\cos B \cos C + \sin B \sin C \cos a. \\ \cos B = -\cos A \cos C + \sin A \sin C \cos b. \\ \cos C = -\cos A \cos B + \sin A \sin B \cos c. \end{cases}$$

§ 51.

$$\text{46.}\ \begin{cases} \sin \frac{1}{2} A = \sqrt{\sin (s-b) \sin (s-c) \csc b \csc c}. \\ \cos \frac{1}{2} A = \sqrt{\sin s \sin (s-a) \csc b \csc c}. \\ \tan \frac{1}{2} A = \sqrt{\csc s \csc (s-a) \sin (s-b) \sin (s-c)}. \end{cases}$$

$$\text{47.}\ \begin{cases} \sin \frac{1}{2} a = \sqrt{-\cos S \cos (S-A) \csc B \csc C}. \\ \cos \frac{1}{2} a = \sqrt{\cos (S-B) \cos (S-C) \csc B \csc C}. \\ \tan \frac{1}{2} a = \sqrt{-\cos S \cos (S-A) \sec (S-B) \sec (S-C)}. \end{cases}$$

§ 52.

$$\text{48.}\ \begin{cases} \cos \frac{1}{2}(A+B) \cos \frac{1}{2} c = \cos \frac{1}{2}(a+b) \sin \frac{1}{2} C. \\ \sin \frac{1}{2}(A+B) \cos \frac{1}{2} c = \cos \frac{1}{2}(a-b) \cos \frac{1}{2} C. \\ \cos \frac{1}{2}(A-B) \sin \frac{1}{2} c = \sin \frac{1}{2}(a+b) \sin \frac{1}{2} C. \\ \sin \frac{1}{2}(A-B) \sin \frac{1}{2} c = \sin \frac{1}{2}(a-b) \cos \frac{1}{2} C. \end{cases}$$

$$\text{49.}\ \begin{cases} \tan \frac{1}{2}(A+B) = \dfrac{\cos \frac{1}{2}(a-b)}{\cos \frac{1}{2}(a+b)} \cot \frac{1}{2} C. \\ \tan \frac{1}{2}(A-B) = \dfrac{\sin \frac{1}{2}(a-b)}{\sin \frac{1}{2}(a+b)} \cot \frac{1}{2} C. \\ \tan \frac{1}{2}(a+b) = \dfrac{\cos \frac{1}{2}(A-B)}{\cos \frac{1}{2}(A+B)} \tan \frac{1}{2} c. \\ \tan \frac{1}{2}(a-b) = \dfrac{\sin \frac{1}{2}(A-B)}{\sin \frac{1}{2}(A+B)} \tan \frac{1}{2} c. \end{cases}$$

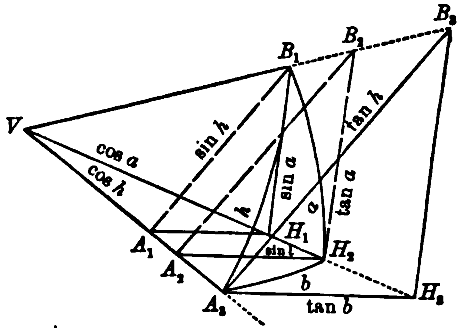
§ 53.

50. $F = \dfrac{E}{180^\circ} \pi R^2.$

51. $\tan^2 \frac{1}{4} E = \tan \frac{1}{2}(s-a) \tan \frac{1}{2}(s-b) \tan \frac{1}{2}(s-c).$

§ 60.

PROF. BLAKSLEE's construction by which the direction ratios for plane right triangles give directly from a figure the analogies for a right trihedral or for a right spherical triangle.



The construction consists of two parts.

(*a*) Lay off from the vertex V a unit's distance on each edge.

(*b*) Pass through the three extremities of these distances three planes perpendicular to one of the edges, as VA. Now these three parallel planes will cut out three similar right triangles. The first being constructed in either of the two usual ways, the construction of the others is evident.

Since the plane angles A_1, A_2, A_3 all equal the dihedral A, and the nine right triangles in the three faces give the values in the figure, we have:

(1) $\sin A = \sin a : \sin h$; similarly, $\sin B = \sin b : \sin h$.

(2) $\cos A = \tan b : \tan h$; similarly, $\cos B = \tan a : \tan h$.

(3) $\tan A = \tan a : \sin b$; similarly, $\tan B = \tan b : \sin a$.

(4) $\cos h = \cos a \ \cos b$; (by 3) $= \cot A \cot B$.

(5) $\sin A = \cos B : \cos b$; $\sin B = \cos A : \cos a$.

NOTE. If a sphere of unit radius be described about V as a centre, the three faces will cut out a right spherical triangle, having the sides a, b, and h, and angles A, B, and H. The above formulas are thus seen to be the analogies of:

(1) $\sin A = a : h$; $\sin B = b : h$.

(2) $\cos A = b : h$; $\cos B = a : h$.

(3) $\tan A = a : b$; $\tan B = b : a$.

(4) $h^2 = a^2 + b^2$; $1 = \sin^2 + \cos^2$; $1 = \cot A \cot B$.

(5) $\sin A = \cos B$; $\sin B = \cos A$.

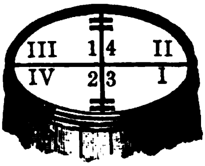
Napier's rules give only the following, which follow from the analogies as numbered:

$$\begin{array}{l}\text{By}\\(1)\end{array}\left\{\begin{array}{l}\sin a = \sin A \sin h = \tan b \cot B\\ \sin b = \sin B \sin h = \tan a \cot A\end{array}\right\}(3)$$

$$(5)\left\{\begin{array}{l}\cos A = \sin B \cos a = \tan b \cot h\\ \cos B = \sin A \cos b = \tan a \cot h\end{array}\right\}(2)$$

$$(4)\ \{\cos h = \cos a \cos b = \cot A \cot B\}\ (4)$$

The Gauss Equations.



$$\cos \tfrac{1}{2}(A + B) \cos \tfrac{1}{2} c = \cos \tfrac{1}{2}(a + b) \sin \tfrac{1}{2} C.$$

$$\sin \tfrac{1}{2}(A + B) \cos \tfrac{1}{2} c = \cos \tfrac{1}{2}(a - b) \cos \tfrac{1}{2} C.$$

$$\cos \tfrac{1}{2}(A - B) \sin \tfrac{1}{2} c = \sin \tfrac{1}{2}(a + b) \sin \tfrac{1}{2} C.$$

$$\sin \tfrac{1}{2}(A - B) \sin \tfrac{1}{2} c = \sin \tfrac{1}{2}(a - b) \cos \tfrac{1}{2} C.$$

$$f \tfrac{1}{2}(A \pm B)\ \ f \tfrac{1}{2} c = \ f \tfrac{1}{2}(a \pm b)\ \ f \tfrac{1}{2} C.$$

Rule I. sin in (I.) gives − in (3), and conversely.
cos in (I.) gives + in (3), and conversely.

Rule II. Functions have same names in (2) and (3).
Functions have co-names in (4) and (1).

ANSWERS.

PLANE TRIGONOMETRY.

EXERCISE I.

1. $\sin B = \frac{b}{c}$, $\cos B = \frac{a}{c}$, $\tan B = \frac{b}{a}$, $\cot B = \frac{a}{b}$, $\sec B = \frac{c}{a}$, $\csc B = \frac{c}{b}$.

3. (i.) $\sin = \frac{3}{5}$, $\cos = \frac{4}{5}$, $\tan = \frac{3}{4}$, $\cot = \frac{4}{3}$, $\sec = \frac{5}{4}$, $\csc = \frac{5}{3}$.
(ii.) $\sin = \frac{5}{13}$, etc.
(iii.) $\sin = \frac{8}{17}$, etc.
(iv.) $\sin = \frac{9}{41}$, etc.
(v.) $\sin = \frac{11}{61}$, etc.
(vi.) $\sin = \frac{119}{169}$, etc.

4. The required condition is that $a^2 + b^2 = c^2$. It is.

5. (i.) $\sin = \frac{2mn}{m^2 + n^2}$, etc. (iii.) $\sin = \frac{q}{s}$, etc.
(ii.) $\sin = \frac{2xy}{x^2 + y^2}$, etc. (iv.) $\sin = \frac{ms}{qr}$, etc.

7. In (iii.) $p^2q^2 + q^2s^2 = p^2s^2$; in (iv.) $m^2n^2s^2 + m^2p^2v^2 = n^2q^2r^2$.

8. $c = 145$; whence, $\sin A = \frac{24}{145} = \cos B$; $\cos A = \frac{143}{145} = \sin B$;
$\tan A = \frac{24}{143} = \cot B$; $\cot A = \frac{143}{24} = \tan B$; $\sec A = \frac{145}{143} = \csc B$; etc.

9. $b = 0.023$; whence, $\tan A = \cot B = \frac{23}{264}$; $\cot A = \tan B = \frac{264}{23}$, etc.

10. $a = 16.8$; whence, $\sin A = \frac{168}{185} = \cos B$, etc.

11. $c = p + q$; whence, $\sin A = \frac{\sqrt{p^2 + q^2}}{p + q} = \cos B$; etc.

12. $b = \sqrt{q(p + q)}$; whence, $\tan A = \sqrt{\frac{p}{q}} = \cot B$; etc.

13. $a = p - q$; whence, $\sin A = \frac{p - q}{p + q} = \cos B$; etc.

14. $\sin A = \frac{2}{5}\sqrt{5} = 0.89443$; etc. 15. $\sin A = \frac{3}{5}$; etc.

16. $\sin A = \frac{1}{8}(5 + \sqrt{7}) = 0.95572$; etc.

17. $\cos A = \frac{1}{8}(\sqrt{31} - 1) = 0.57097$; $\sin A = \frac{1}{8}(\sqrt{31} + 1) = 0.82097$; etc.

18. $a = 12.2$. 20. $a = 9$. 22. $c = 40$.

19. $b = 1.54$. 21. $b = 68$. 23. $c = 229.62$.

24. Construct a rt. △ with legs equal to 3 and 2 respectively; then construct a similar △ with hypotenuse equal to 6.
In like manner, 25, 26, 27, may be solved.

28. $a = 1.5$ miles; $b = 2$ miles. 31. 400,000 miles.

30. $a = 0.342$, $b = 0.940$; $a = 1.368$, $b = 3.760$. 32. 142.926 yards.

EXERCISE II..

5. Through A (Fig. 3) draw a tangent, and take $AT = 3$; the angle AOT is the required angle.

6. From O (Fig. 3) as a centre, with a radius = 2, describe an arc cutting at S the tangent drawn through B; the angle SOA is the required angle.

7. In Fig. 3, take $OM = \frac{1}{4}$, and erect $MP \perp OA$ and intersecting the circumference at P; the angle POM is the required angle.

8. Since $\sin x = \cos x$, $OM = PM$ (Fig. 3), and $x = 45°$; hence, construct $x = 45°$.

9. Construct a rt. Δ with one leg = twice the other; the angle opposite the longer leg is the required angle.

10. Divide OA (Fig. 3) into four equal parts; at the first point of division from O erect a perpendicular to meet the circumference at some point P. Join OP; the angle AOP is the required angle.

21. $r \sin x$. 22. Leg adjacent to $A = nc$, leg opposite to $A = mc$.

EXERCISE III.

1. cos 60°. cot 1°. sec 71° 50′. tan 7° 41′.
   sin 45°. tan 75°. sin 52° 36′. sec 35° 14′.

2. cos 30°. cot 33°. sec 20° 58′. tan 0° 1′.
   sin 15°. tan 6°. sin 4° 21′. sec 44° 59.

3. $\frac{1}{3}\sqrt{3}$.

4. $\tan A = \cot A = \cot(90° - A)$; hence, $A = 90° - A$ and $A = 45°$.

5. 30°. 7. 90°. 9. 22° 30′. 11. 10°.

6. 30° 8. 60°. 10. 18°. 12. $\frac{90°}{n+1}$

EXERCISE V.

1. $\cos A = \frac{5}{13}$, $\tan A = \frac{12}{5}$, $\cot A = \frac{5}{12}$, $\sec A = \frac{13}{5}$, $\csc A = \frac{13}{12}$.

2. $\cos A = 0.6$, $\tan A = 1.3333$, $\cot A = 0.75$, $\sec A = 1.6667$, $\csc A = 1.25$.

3. $\sin A = \frac{11}{61}$, $\tan A = \frac{11}{60}$, $\cot A = \frac{60}{11}$, $\sec A = \frac{61}{60}$, $\csc A = \frac{61}{11}$.

4. $\sin A = 0.96$, $\tan A = 3.42854$, $\cot A = 0.29167$, $\sec A = 3.5714$.

5. $\sin A = 0.8$, $\cos A = 0.6$, $\cot A = 0.75$, $\sec A = 1.6667$, $\csc A = 1.25$.

6. $\sin A = \frac{1}{2}\sqrt{2}$, $\cos A = \frac{1}{2}\sqrt{2}$, $\tan A = 1$, $\sec A = \sqrt{2}$, $\csc A = \sqrt{2}$.

7. $\tan A = 2$, $\sin A = 0.90$, $\cos A = 0.45$, $\sec A = 2.22$, $\csc A = 1.11$.

8. $\cos A = \frac{1}{2}$, $\sin A = \frac{1}{2}\sqrt{3}$, $\tan A = \sqrt{3}$, $\cot A = \frac{1}{3}\sqrt{3}$, $\csc A = \frac{2}{3}\sqrt{3}$.

9. $\sin A = \frac{1}{2}\sqrt{2}$, $\cos A = \frac{1}{2}\sqrt{2}$, $\tan A = 1$, $\cot A = 1$, $\sec A = \sqrt{2}$.

10. $\cos A = \sqrt{1 - m^2}$, $\tan A = \frac{m}{1 - m^2}\sqrt{1 - m^2}$, $\cot A = \frac{1}{m}\sqrt{1 - m^2}$.

11. $\cos A = \frac{1 - m^2}{1 + m^2}$, $\tan A = \frac{2m}{1 - m^2}$, $\cot A = \frac{1 - m^2}{2m}$, $\sec A = \frac{1 + m^2}{1 - m^2}$.

12. $\sin A = \frac{m^2 - n^2}{m^2 + n^2}$, $\tan A = \frac{m^2 - n^2}{2mn}$, $\sec A = \frac{m^2 + n^2}{2mn}$.

13. $\cot = 1$, $\sin = \frac{1}{2}\sqrt{2}$, $\cos = \frac{1}{2}\sqrt{2}$, $\sec = \sqrt{2}$, $\csc = \sqrt{2}$.

14. $\cos = \frac{1}{2}\sqrt{3}$, $\tan = \frac{1}{3}\sqrt{3}$, $\cot = \sqrt{3}$, $\sec = \frac{2}{3}\sqrt{3}$, $\csc = 2$.

15. $\sin = \frac{1}{2}\sqrt{3}$, $\cos = \frac{1}{2}$, $\tan = \sqrt{3}$, $\cot = \frac{1}{3}\sqrt{3}$, $\sec = 2$.

16. $\sin = \frac{1}{2}\sqrt{2 - \sqrt{3}}$, $\cos = \frac{1}{2}\sqrt{2 + \sqrt{3}}$, $\cot = 2 + \sqrt{3}$.

17. $\sin = \frac{1}{2}\sqrt{2 - \sqrt{2}}$, $\cos = \frac{1}{2}\sqrt{2 + \sqrt{2}}$, $\tan = \sqrt{2} - 1$.

18. $\cos = 1$, $\tan = 0$, $\cot = \infty$, $\sec = 1$, $\csc = \infty$.

19. $\cos = 0$, $\tan = \infty$, $\cot = 0$, $\sec = \infty$, $\csc = 1$.

20. $\sin = 1$, $\cos = 0$, $\cot = 0$, $\sec = \infty$, $\csc = 1$.

21. $\cos A = \sqrt{1 - \sin^2 A}$, $\tan A = \frac{\sin A}{\sqrt{1 - \sin^2 A}}$, $\csc A = \frac{1}{\sin A}$.

22. $\sin A = \sqrt{1 - \cos^2 A}$, $\tan A = \frac{\sqrt{1 - \cos^2 A}}{\cos A}$, $\cot A = \frac{\cos A}{\sqrt{1 - \cos^2 A}}$,
$\sec A = \frac{1}{\cos A}$, $\csc A = \frac{1}{\sqrt{1 - \cos^2 A}}$.

23. $\sin A = \frac{\tan A}{\sqrt{1 + \tan^2 A}}$, $\cos A = \frac{1}{\sqrt{1 + \tan^2 A}}$, $\cot A = \frac{1}{\tan A}$,
$\sec A = \sqrt{1 + \tan^2 A}$, $\csc A = \frac{\sqrt{1 + \tan^2 A}}{\tan A}$.

24. $\tan A = \frac{1}{\cot A}$, $\csc A = \sqrt{1 + \cot^2 A}$, $\sin A = \frac{1}{\sqrt{1 + \cot^2 A}}$,
$\cos A = \frac{\cot A}{\sqrt{1 + \cot^2 A}}$, $\sec A = \frac{\sqrt{1 + \cot^2 A}}{\cot A}$.

25. $\sin A = \frac{1}{5}\sqrt{5}$, $\cos A = \frac{2}{5}\sqrt{5}$.

26. $\sin A = \frac{1}{4}\sqrt{15}$, $\tan A = \sqrt{15}$.

27. $\sin A = \frac{9}{41}$, $\cos A = \frac{40}{41}$.

28. $\frac{1 - 3\cos^2 A + 3\cos^4 A}{\cos^2 A - \cos^4 A}$.

EXERCISE VI.

1. $\frac{b}{c}=\cos A$; $\therefore c=\frac{b}{\cos A}$.

5. $A=90^\circ-B$, $a=c\cos B$, $b=c\sin B$.

39. $c=7.8112$, $A=39^\circ 48'$, $B=50^\circ 12'$.

40. $b=70.007$, $A=30' 12''$, $B=89^\circ 29' 48''$.

41. $a=1.1886$, $A=43^\circ 20'$, $B=46^\circ 40'$.

42. $b=21.249$, $c=22.372$, $B=71^\circ 46'$.

43. $a=6.6882$, $c=13.738$, $B=60^\circ 52'$.

44. $a=63.89$, $b=23.369$, $B=20^\circ\ 6'$.

45. $a=19.40$, $b=18.778$, $A=45^\circ 56'$.

46. $b=53.719$, $c=71.377$, $A=41^\circ 11'$.

47. $a=12.981$, $c=15.796$, $A=55^\circ 16'$.

48. $a=0.58046$, $b=8.442$, $A=\ 3^\circ 56'$.

49. $F=\frac{1}{4}(c^2\sin A\cos A)$.

50. $F=\frac{1}{2}(a^2\cot A)$.

51. $F=\frac{1}{2}(b^2\tan A)$.

52. $F=\frac{1}{2}(a\sqrt{c^2-a^2})$.

53. $b=11.6$, $c=15.315$, $A=40^\circ 45' 48''$, $B=49^\circ 14' 12''$.

54. $a=7.2$, $c=8.766$, $B=34^\circ 46' 40''$, $A=55^\circ 13' 20''$.

55. $a=3.6474$, $b=6.58$, $c=7.5233$, $B=61^\circ$.

56. $a=10.283$, $b=19.449$, $A=27^\circ 52'$, $B=62^\circ 8'$.

57. 19° 28′ and 70° 32′.

58. 3 and 5.1961.

59. $a=c\cos\frac{90^\circ}{n+1}$,

$b=c\sin\frac{90^\circ}{n+1}$.

60. 36° 52′ 12″ and 53° 7′ 48″.

61. 212.1 feet.

62. 732.22 feet.

63. 3270 feet.

64. 37.3 feet, 96 feet.

65. $\tan A=\frac{a}{b}$, $A=59^\circ 45'$.

66. $a=b\tan A$, 95.34.

67. 1° 25′ 56″.

68. 7.0712 miles in each direction.

69. 20.88 feet.

70. 56.65 feet.

71. 228.63 yards.

72. 136.6 feet.

73. 140 feet.

74. 84.74 feet.

EXERCISE VII.

1. $C=2(\ 90^\circ-A)$, $c=2a\cos A$, $h=a\sin A$.

2. $A=\frac{1}{2}(180^\circ-C)$, $c=2a\cos A$, $h=a\sin A$.

3. $C=2(\ 90^\circ-A)$, $a=c+2\cos A$, $h=a\sin A$.

4. $A = \frac{1}{2}(180^\circ - C)$, $a = c + 2\cos A$, $h = a \sin A$.
5. $C = 2\ (90^\circ - A)$, $a = h + \sin A$, $c = 2a\cos A$.
6. $A = \frac{1}{2}(180^\circ - C)$, $a = h + \sin A$, $c = 2a\cos A$.
7. $\sin A = h + a$, $C = 2(90^\circ - A)$, $c = 2a\cos A$.
8. $\tan A = h + \frac{1}{2}c$, $C = 2(90^\circ - A)$, $a = h + \sin A$.
9. $A = 67^\circ\, 22'\, 50''$, $C = 45^\circ\, 14'\, 20''$, $h = 13.2$.
10. $c = 0.21943$, $h = 0.27384$, $F = 0.03004$.
11. $a = 2.055$, $h = 1.6852$, $F = 1.9819$.
12. $a = 7.705$, $c = 3.6676$, $F = 13.73$.
13. $A = 79^\circ\, 36'\, 30''$, $C = 20^\circ\, 45'\, 30''$, $c = 2.4206$.
14. $A = 77^\circ\, 19'\, 11''$, $C = 25^\circ\, 21'\, 38''$, $a = 20.5$.
15. $A = 25^\circ\, 28'$, $C = 129^\circ\, 4'$, $a = 81.388$, $h = 35$.
16. $A = 81^\circ\, 12'\, 9''$, $C = 17^\circ\, 35'\, 42''$, $a = 17$, $c = 5.2$.

17. $F = \frac{1}{4}c\sqrt{4a^2 - c^2}$.
18. $F = a^2 \sin\frac{1}{2}C \cos\frac{1}{2}C$.
19. $F = a^2 \sin A \cos A$.
20. $F = h^2 \tan\frac{1}{2}C$.
21. 28.284 feet, 4525.44 sq. feet.
22. 0.76537.
23. 94° 20′.
24. 2.7261.
25. 38° 56′ 33″.
26. 37.7

EXERCISE VIII.

1. $r = 1.618$, $h = 1.5388$, $F = 7.694$.
2. $r = 11.269$, $h = 10.886$, $F = 381.04$.
3. $h = 0.9848$, $p = 6.2514$, $F = 3.0782$.
4. $h = 19.754$, $c = 6.2537$, $F = 1236$.
5. $r = 1.0824$, $c = 0.8284$, $F = 3.3137$.
6. $r = 2.592$, $h = 2.488$, $c = 1.4615$.
7. $r = 1.5994$, $h = 1.441$, $p = 9.716$.

8. 0.6181.
9. 0.64984.
10. 0.51764.
11. $b = \dfrac{c}{2\cos\dfrac{90^\circ}{n}}$.
12. 0.2238.
13. 0.31.
14. 0.82842.
15. 94.63.
16. 415.
17. 11.636.
18. 99.64.
19. 1.0235.
20. 0.635.

EXERCISE IX.

5. Two angles: one in Quadrant I., the other in Quadrant II.

6. Four values: two in Quadrant I., two in Quadrant IV.

7. x may have two values in the first case, and one value in each of the other cases.

8. If $\cos x = -\frac{2}{3}$, x is between 90° and 270°; if $\cot x = 4$, x is between 0° and 90° or 180° and 270°; if $\sec x = 80$, x is between 0° and 90° or between 270° and 360°; if $\csc x = -3$, x is between 180° and 360°.

9. In Quadrant III.; in Quadrant II.; in Quadrant III.

10. 40 angles; 20 positive and 20 negative.

11. +, when x is known to be in Quadrant I. or IV.; −, when x is known to be in Quadrant II. or III.

14. $\sin x = -\frac{4}{7}\sqrt{3}$, $\tan x = -4\sqrt{3}$, $\cot x = -\frac{1}{12}\sqrt{3}$, $\csc x = -\frac{7}{12}\sqrt{3}$.

15. $\sin x = \pm\frac{1}{10}\sqrt{10}$, $\cos x = \mp\frac{3}{10}\sqrt{10}$, $\tan x = -\frac{1}{3}$, $\sec x = \mp\frac{1}{3}\sqrt{10}$.
$\csc x = \pm\sqrt{10}$.

16. The cosine, the tangent, the cotangent, and the secant are negative when the angle is obtuse.

17. Sine and cosecant leave it doubtful whether the angle is an acute angle or an obtuse angle; the other functions, if + determine an acute angle, if − an obtuse angle.

20. $\sin 450 = \sin(360 + 90) = \sin 90 = 1$; $\tan 540° = \tan 180° = 0$;
$\cos 630° = \cos 270° = 0$; $\cot 720° = \cot 0° = \infty$;
$\sin 810° = \sin 90° = 1$; $\csc 900° = \csc 180° = \infty$.

21. 45°, 135°, 225°, 315°. 22. 0. 23. 0. 24. 0.

25. $a^2 - b^2 + 4ab$.

EXERCISE X.

2. $\sin 172° = \sin 8°$.
3. $\cos 100° = -\sin 10°$.
4. $\tan 125° = -\cot 35°$.
5. $\cot 91° = -\tan 1°$.
6. $\sec 110° = -\csc 20°$.
7. $\csc 157° = \csc 23°$.
8. $\sin 204° = -\sin 24°$.
9. $\cos 359° = \cos 1°$.
10. $\tan 300° = -\cot 30°$.
11. $\cot 264° = \tan 6°$.
12. $\sec 244° = -\csc 26°$.
13. $\csc 271° = -\sec 1°$.
14. $\sin 163° 49' = \sin 16° 11'$.
15. $\cos 195° 33' = -\cos 15° 33'$.
16. $\tan 269° 15' = \cot 0° 45'$.
17. $\cot 139° 17' = -\cot 40° 43'$.
18. $\sec 299° 45' = \csc 29° 45'$.
19. $\csc 92° 25' = \sec 2° 25'$.

20. $\sin(-75^\circ) = -\sin 75^\circ = -\cos 15^\circ$, $\cos(-75^\circ) = \cos 75^\circ = \sin 15^\circ$, etc.

21. $\sin(-127^\circ) = -\sin 127^\circ = -\cos 37^\circ$, $\cos(-127^\circ) = \cos 127^\circ = -\sin 37^\circ$, etc.

22. $\sin(-200^\circ) = \sin 160^\circ = \sin 20^\circ$, $\cos(-200^\circ) = \cos 200^\circ = -\cos 20^\circ$, etc.

23. $\sin(-345^\circ) = -\sin 345^\circ = \sin 15^\circ$, $\cos(-345^\circ) = \cos 345^\circ = \cos 15^\circ$. etc.

24. $\sin(-52^\circ 37') = -\sin 52^\circ 37' = -\cos 37^\circ 23'$,
$\cos(-52^\circ 37') = \cos 52^\circ 37' = \sin 37^\circ 23'$, etc.

25. $\sin(-196^\circ 54') = \sin 196^\circ 54' = \cos 16^\circ 54'$,
$\cos(-196^\circ 54') = \cos 196^\circ 54' = -\cos 16^\circ 54'$, etc.

26. $\sin 120^\circ = \frac{1}{2}\sqrt{3}$, $\cos 120^\circ = -\frac{1}{2}$, etc.

27. $\sin 135^\circ = +\frac{1}{2}\sqrt{2}$, $\cos 135^\circ = -\frac{1}{2}\sqrt{2}$, etc.

28. $\sin 150^\circ = +\frac{1}{2}$, $\cos 150^\circ = -\frac{1}{2}\sqrt{3}$, etc.

29. $\sin 210^\circ = -\frac{1}{2}$, $\cos 210^\circ = -\frac{1}{2}\sqrt{3}$, etc.

30. $\sin 225^\circ = -\frac{1}{2}\sqrt{2}$, $\cos 225^\circ = -\frac{1}{2}\sqrt{2}$, etc.

31. $\sin 240^\circ = -\frac{1}{2}\sqrt{3}$, $\cos 240^\circ = -\frac{1}{2}$, etc.

32. $\sin 300^\circ = -\frac{1}{2}\sqrt{3}$, $\cos 300^\circ = +\frac{1}{2}$, etc.

33. $\sin(-30^\circ) = -\frac{1}{2}$, $\cos(-30^\circ) = +\frac{1}{2}\sqrt{3}$, etc

34. $\sin(-225^\circ) = +\frac{1}{2}\sqrt{2}$, $\cos(-225^\circ) = -\frac{1}{2}\sqrt{2}$, etc.

35. $\cos x = -\frac{1}{2}\sqrt{2}$ or $-\sqrt{\frac{1}{2}}$, etc., $x = 225^\circ$.

36. $\tan x = -\sqrt{\frac{1}{3}}$, $\sin x = \frac{1}{2}$, $\cos x = -\frac{1}{2}\sqrt{3}$, $x = 150^\circ$.

37. $\sin 3540^\circ = \sin 300^\circ = -\sin 60^\circ = -\frac{1}{2}\sqrt{3}$, $\cos 3540^\circ = +\frac{1}{2}$, etc.

38. 210° and 330°; 120° and 300°.

39. 135°, 225°, and −225°; 150° and −30°.

40. 30°, 150°, 390°, and 510°.

41. $\sin 168^\circ$, $\cos 334^\circ$, $\tan 225^\circ$, $\cot 252^\circ$,
$\sin 349^\circ$, $\cos 240^\circ$, $\tan 64^\circ$, $\cot 177^\circ$.

42. 0.848. (Hint: $\tan 238^\circ = \tan 58^\circ$, $\sin 122^\circ = \sin 58^\circ$).

43. -1.952.

44. $(a - b)\sin x$.

45. $m \sin x \cos x$.

46. $(a - b)\cot x - (a + b)\tan x$.

47. $a^2 + b^2 + 2ab\cos x$.

48. 0.

49. $\cos x \sin y - \sin x \cos y$.

50. $\tan x$.

51. Positive between $x = 0^\circ$ and $x = 135^\circ$, and between $x = 315^\circ$ and $x = 360^\circ$; negative between $x = 135^\circ$ and $x = 315^\circ$.

52. Positive between $x = 45^\circ$ and $x = 225^\circ$; negative between $x = 0^\circ$ and $x = 45^\circ$, and between $x = 225^\circ$ and $x = 360^\circ$.

53. $\sin(x - 90^\circ) = -\cos x$, $\cos(x - 90^\circ) = \sin x$, etc.

54. $\sin(x - 180^\circ) = -\sin x$, $\cos(x - 180^\circ) = -\cos x$, etc.

Exercises 53 and 54 should be solved by drawing suitable figures, and employing a mode of proof similar to that used in § 28.

EXERCISE XI.

1. $\sin(x+y) = \frac{56}{65}$, $\cos(x+y) = \frac{33}{65}$.

3. $\sin(90^\circ + y) = \cos y$, $\cos(90 + y) = -\sin y$, etc.

4. $\sin(180 - y) = \sin y$, $\cos(180 - y) = -\cos y$, etc.

5. $\sin(180 + y) = -\sin y$, $\cos(180 + y) = -\cos y$, etc.

6. $\sin(270 - y) = -\cos y$, $\cos(270 - y) = -\sin y$, etc.

7. $\sin(270 + y) = -\cos y$, $\cos(270^\circ + y) = \sin y$, etc.

8. $\sin(360^\circ - y) = -\sin y$, $\cos(360 - y) = \cos y$, etc.

9. $\sin(360 + y) = \sin y$, $\cos(360^\circ + y) = \cos y$, etc.

10. $\sin(x - 90^\circ) = -\cos x$, $\cos(x - 90^\circ) = \sin x$, etc.

11. $\sin(x - 180^\circ) = -\sin x$, $\cos(x - 180^\circ) = -\cos x$, etc.

12. $\sin(x - 270^\circ) = \cos x$, $\cos(x - 270^\circ) = -\sin x$, etc.

13. $\sin(-y) = -\sin y$, $\cos(-y) = \cos y$, etc.

14. $\sin(45^\circ - y) = \frac{1}{2}\sqrt{2}(\cos y - \sin y)$, $\cos(45^\circ - y) = \frac{1}{2}\sqrt{2}(\cos y + \sin y)$, etc.

15. $\sin(45^\circ + y) = \frac{1}{2}\sqrt{2}(\cos y + \sin y)$, $\cos(45^\circ + y) = \frac{1}{2}\sqrt{2}(\cos y - \sin y)$, etc.

16. $\sin(30^\circ + y) = \frac{1}{2}(\cos y + \sqrt{3}\sin y)$, $\cos(30^\circ + y) = \frac{1}{2}(\sqrt{3}\cos y - \sin y)$, etc.

17. $\sin(60^\circ - y) = \frac{1}{2}(\sqrt{3}\cos y - \sin y)$, $\cos(60^\circ - y) = \frac{1}{2}(\cos y + \sqrt{3}\sin y)$, etc.

18. $3\sin x - 4\sin^3 x$. 19. $4\cos^3 x - 3\cos x$. 20. 0. 21. $\frac{1}{2}\sqrt{3}$.

22. $\sin\frac{1}{2}x = \sqrt{\frac{1 - 0.4\sqrt{6}}{2}} = 0.10051$; $\cos\frac{1}{2}x = \sqrt{\frac{1 + 0.4\sqrt{6}}{2}} = 0.99494$.

23. $\cos 2x = -\frac{1}{2}$, $\tan 2x = -\sqrt{3}$.

24. $\sin 22\frac{1}{2}^\circ = \frac{1}{2}\sqrt{2 - \sqrt{2}} = 0.3827$, $\cos 22\frac{1}{2}^\circ = \frac{1}{2}\sqrt{2 + \sqrt{2}} = 0.9239$.
$\tan 22\frac{1}{2}^\circ = \sqrt{2} - 1 = 0.4142$, $\cot 22\frac{1}{2}^\circ = \sqrt{2} + 1 = 2.4142$.

25. $\sin 15^\circ = \frac{1}{2}\sqrt{2 - \sqrt{3}} = 0.2588$, $\cos 15^\circ = \frac{1}{2}\sqrt{2 + \sqrt{3}} = 0.9659$.
$\tan 15^\circ = 2 - \sqrt{3} = 0.2679$, $\cot 15^\circ = 2 + \sqrt{3} = 3.7321$.

27–33. The truth of these equations is to be established by expressing the given functions in terms of the *same* function of the *same* angle. Thus, in Example 27,

$$\sin 2x = 2\sin x\cos x,$$

and $$2\tan x = 2\frac{\sin x}{\cos x},\quad 1 + \tan^2 x = \sec^2 x = \frac{1}{\cos^2 x}.$$

By making these substitutions in the given equation its truth will be evident.

34. $\sin A + \sin B + \sin C = \sin A + \sin B + \sin[180 - (A + B)]$

$$\begin{aligned}
&= \sin A + \sin B + \sin(A + B) \\
&= 2\sin\tfrac{1}{2}(A + B)\cos\tfrac{1}{2}(A - B) + 2\sin\tfrac{1}{2}(A + B)\cos\tfrac{1}{2}(A + B) \\
&= 2\sin\tfrac{1}{2}(A + B)[\cos\tfrac{1}{2}(A - B) + \cos\tfrac{1}{2}(A + B)] \\
&= 4\sin\tfrac{1}{2}(A + B)\cos\tfrac{1}{2}A\cos\tfrac{1}{2}B, \qquad \text{(see §§ 34 and 35)}
\end{aligned}$$

But $\cos\frac{1}{2}C = \cos[90^\circ - \frac{1}{2}(A + B)] = \sin\frac{1}{2}(A + B)$.

Therefore, $\sin A + \sin B + \sin C = 4\cos\frac{1}{2}A\cos\frac{1}{2}B\cos\frac{1}{2}C$.

35. Proof similar to that for 34.

36. $$\begin{aligned}\tan A + \tan B + \tan C &= \frac{\sin A \cos B}{\cos A \cos B} + \frac{\cos A \sin B}{\cos A \cos B} + \frac{\sin C}{\cos C}\\ = \frac{\sin C}{\cos A \cos B} + \frac{\sin C}{\cos C} &= \frac{\sin C \cos C + \cos A \cos B \sin C}{\cos A \cos B \cos C}\\ = \frac{(\cos A \cos B + \cos C)\sin C}{\cos A \cos B \cos C} &= \frac{[\cos A \cos B - \cos(A + B)]\sin C}{\cos A \cos B \cos C}\\ = \frac{\sin A \sin B \sin C}{\cos A \cos B \cos C} &= \tan A \tan B \tan C.\end{aligned}$$

37. Proof similar to that for 36.

38. $\dfrac{2}{\sin 2x}$.

39. $2 \cot 2x$.

40. $\dfrac{\cos(x-y)}{\sin x \cos y}$

41. $\dfrac{\cos(x+y)}{\sin x \cos y}$

42. $\tan^2 x$.

43. $\dfrac{\cos(x-y)}{\cos x \cos y}$.

44. $\dfrac{\cos(x+y)}{\cos x \cos y}$

45. $\dfrac{\cos(x-y)}{\sin x \sin y}$.

46. $\dfrac{\cos(x+y)}{\sin x \sin y}$.

47. $\tan x \tan y$.

EXERCISE XII.

1. If, for instance, $B = 90°$, [25] becomes $\dfrac{a}{b} = \sin A$.

3. $a^2 = b^2 + c^2$, $a^2 = b^2 + c^2 - 2bc$, $a^2 = b^2 + c^2 + 2bc$.

6. 90° in each case.

7. (i.) $\dfrac{a-b}{a+b} = \tan(A - 45°)$, and a right triangle.
   (ii.) $a + b = (a - b)(2 + \sqrt{3})$, an isosceles triangle with the angles 30°, 30°, 120°.

EXERCISE XIII.

9. 300.

10. $AB = 59.564$ miles; $AC = 54.285$ miles.

11. 4.6064 miles, 4.4494 miles, 3.7733 miles.

12. 4.1501 and 8.67.

13. 6.1433 miles and 8.7918 miles.

14. 8 and 5.4723.

15. $a = 5$, $c = 9.6592$.

16. $a = 7$, $b = 8.573$.

17. Sides, 600 feet and 1039.2 feet; altitude, 519.6 feet.

18. 855 : 1607.

19. 5.438 and 6.857.

20. 15.588.

EXERCISE XIV.

11. 420. 12. The other diagonal = 124.617.

EXERCISE XV.

11. 6.
12. 10.392.
14. 8.9212.
15. 25.
16. 3800 yards.
17. 729.7 yards.
18. 10.266.
19. $a = 5.0032$, $b = 2.3385$.
20. 26° 0′ 10″ and 14° 5′ 50″.

EXERCISE XVI.

11. $A = 36° 52' 12''$, $B = 53° 7' 48''$, $C = 90°$.
12. $A = B = 33° 33' 27''$, $C = 112° 53' 6''$.
13. $A = B = C = 60°$.
14. Impossible.
15. 15°, 45°, 120°.
16. 45°, 60°, 75°.
17. 4° 23′ W. of N., or W. of S.
18. 60°.
20. 0.88873.
21. 54.516 miles.

EXERCISE XVII.

1. 4333600.
2. 365.68.
3. 13260.
4. 8160.
5. 240.
6. 26208.
7. 15540.
8. 29450 or 6983.
9. $10\sqrt{3} = 17.3205$.
10. $6\sqrt{3} = 10.3923$.
11. 0.19952.
12. $ab \sin A$.
13. $\frac{1}{4}(a^2 - b^2) \tan A$.
14. 2421000.
15. 30°, 30°, 120°.

EXERCISE XVIII.

1. 21.166 miles; 24.966 miles.
2. 6.3399 miles.
3. 119.29 feet.
4. 30°.
5. 20 feet.
6. 2.6268 or 21.4704.
7. 276.14 yards.
8. 383.35 yards.

34′ ?

MISCELLANEOUS PROBLEMS.

2. 107 feet; 143 feet.
3. 1024 feet.
4. 37° [illegible]′ 5″.
5. 238,400 miles.
6. 861,800 miles.
7. 2922.4 miles.
8. 60°.
9. 3.2.
10. 6.6.
11. 199.56 feet.
12. 43 feet.
13. 45 feet.
14. 26° 34′.
15. 78.37 feet.
16. 75 feet.
17. 1.44 miles.
19. 56.65 feet.
20. 69.28 feet.
21. 260 feet; 3690 feet.
22. 1.344 miles.
23. 235.8 yards.
27. 8 inches.
30. 460.45 feet.
31. 88.94 feet.
32. 13.657 miles.
34. 56.5 feet.
35. 51.6 feet.
36. 101.89 feet.
38. N. 76° 56′ E.; 13.94 miles an hour.
39. 422 yards.
40. 256 feet.
41. 3121 feet; 3633.5 feet.
42. 529.5 feet.
43. 41.41 feet.
44. 234.5 feet.
45. 25.43 miles.
46. 294.7 feet.
47. 12,492 feet.
48. 6.34 miles.
49. 210.44 feet.
51. 757.5 feet.
52. 520 yards.
53. 1366.4 feet.
54. 658 pounds; 22° 24′ with first force.
55. 88.33 pounds; 45° 37′ with known force.
58. 500.2; 536.3.
59. 345.47 feet.
60. 345.47 yards.
61. 61.23 feet.
63. 307.79.
64. 19.8; 35.7; 44.5.
65. 45°.
68. 60°.
69. 60°.
70. 30°.
73. $\frac{1}{2}bc\sin A$.
74. $\frac{1}{2}c^2\sin A\sin B\csc(A+B)$.
75. $\sqrt{[s(s-a)(s-b)(s-c)]}$.

77. 199 A. 3 R. 10 P.
78. 210 A. 3 R. 26 P.
79. 12 A. 3 R. 37 P.
80. 3 A. 0 R. 6 P.
81. 12 A. 1 R. 14 P.
82. 4 A. 2 R. 26 P.
83. 14 A. 2 R. 9 P.
84. 61 A. 2 R.
85. 4 A. 2 R. 26 P.
86. 13.93, 23.21, 32.5 ch.
87. 9 A.
89. 876.31.
90. 1229.5.
92. 1075.3.
93. 2660.45.
94. 16,281.
95. 435.8 feet.
96. 49,089 feet.
97. 750 feet.
98. 422.4 feet.
99. 1835 feet.
100. 26.88.
103. 6.
108. 6.
110. 6087 feet.
111. 5° 25′ S.; 457.5 miles.
112. 460.8; 383.1 miles.
113. 229 miles; lat. 11° 39′ S.
114. S. 56° 7′ 30″ E.; 202.6 miles.
115. N. 17° 25′ W.; 37° 46′ N.
116. 56° 11′ E.; 244.3.
121. Long. 68° 55′ W.
122. 103.6 miles.
124. 33° 18′ N.; 36° 24′ W.
125. N. 28° 47′ E.; 1293 miles.
126. S. 50° 40′ W.; 250.8; 20° 9′ W.
127. 38° 21′ N.; 55° 12′ W.

128. 171 miles; 32° 44′ W. 129. N. 36° 52′ W.; 36° 8′ W.

130. 173 miles; 51° 16′ S.; 34° 13′ E.

131. S. 50° 58′ E.; 47° 15′ N.; 20° 49′ W.

132. N. 53° 20′ E., 16° 7′ W.; *or* N. 53° 20′ W., 25° 53′ W.

133. N. 47° 42.5′ E., 19° 27′ N., 121° 51′ E.; *or* N. 47° 42.5′ W., 19° 27′ N., 116° 9′ E.; *or* S. 47° 42.5′ E., 14° 33′ N., 121° 48′ E.; *or* S. 47° 42.5′ W., 14° 33′ N., 116° 12′ E.

137. N. 73′ E., 45 miles; 42° 15′ N., 69° 5′ W.

138. N. 72° W., 287 miles; 33° S., 13° 2′ E.

SPHERICAL TRIGONOMETRY.

EXERCISE XIX.

1. $110°, 100°, 80°$.
2. $140°, 90°, 55°$.
7. $\frac{8}{9}\pi, 2\pi, \frac{26}{9}\pi$.

EXERCISE XX.

3. (i.) Either a or b must be equal to $90°$. (ii.) If $a = 90°$, then $A = 90°$, and $B = b$; if $b = 90°$, then $B = 90°$, and $A = a$. (iii.) $c = 90°$, $A = 90°$, $B = b$. (iv.) $c = 90°$, $A = 90°$, $B = 90°$, $C = 90°$.

EXERCISE XXI.

2. I. The cosine of the middle part = the product of the cotangents of the adjacent parts.

   II. The cosine of the middle part = the product of the sines of the opposite parts.

EXERCISE XXII.

24. $A = 175° 57' 10''$, $B = 135° 42' 50''$, $C = 135° 34' 7''$.
25. $C = 104° 41' 39''$, $a = 104° 53' 2''$, $b = 133° 39' 48''$.
26. ~~$\sin a = \sin A \sec C$, $\cos b = -\tan A \cot C$, $\cos B = -\sec A \cos C$.~~
27. $a = 60°$, $b = 90°$, $B = 90°$.
28. The triangle is impossible; why?
29. $b = 130° 41' 42''$, $c = 71° 27' 43''$, $A = 112° 57' 2''$.
30. $a = 26° 3' 51''$, $A = 35°$, $B = 65° 46' 7''$.
31. Impossible; why?

EXERCISE XXIII.

1. $\cos A = \cot a \tan \frac{1}{2} b$, $\sin \frac{1}{2} B = \csc a \sin \frac{1}{2} b$, $\cos h = \cos a \sec \frac{1}{2} b$.
2. $\sin \frac{1}{2} A = \frac{1}{2} \sec \frac{1}{2} a$, or $\cos A = \frac{1}{2} \cos a \sec^2 \frac{1}{2} a$, or $\tan \frac{1}{2} A = \sec a \cos \frac{1}{2} a$.
3. $\sin \frac{1}{2} A = \sec \frac{1}{2} a \cos \frac{180°}{n}$, $\sin R = \sin \frac{1}{2} a \csc \frac{180°}{n}$,

   $\sin r = \tan \frac{1}{2} a \cot \frac{180°}{n}$.
4. Tetrahedron, $70° 31' 43''$; octahedron, $109° 28' 18''$; icosahedron, $138° 11' 36''$; cube, $90°$; dodecahedron, $116° 33' 44''$.
5. $\cot \frac{1}{2} A = \sqrt{\cos a}$.

$a = 90°$,

m

Exercise XXV.

1. (i.) $\tan m = \tan b \cos A$, $\cos a = \cos b \sec m \cos(c-m)$; (ii.) $\tan n = \tan a \cos B$, $\cos b = \cos a \sec n \cos(c-n)$.

Exercise XXVI.

1. (i.) $\tan x = \tan B \cos c$, $\cos A = \cos B \csc x \sin(C-x)$; (ii.) $\tan x = \tan A \cos b$, $\cos B = \cos A \csc x \sin(C-x)$.

Exercise XXXI.

4. 27.25″.

Exercise XXXII.

1. If x denote the angle required, $\sin \frac{1}{2}x = \cos 18° \sec 9°$, $x = 148° 42'$.
2. $\cos x = \cos A \cos B$.
3. Let $w =$ the inclination of the edge c to the plane of a and b. Then it is easily shown that $V = abc \sin l \sin w$. Now, conceive a sphere constructed having for centre the vertex of the trihedral angle whose edges are a, b, c. The spherical triangle, whose vertices are the points where a, b, c meet the surface of this sphere, has for its sides l, m, n; and w is equal to the perpendicular arc from the side l to the opposite vertex. Let L, M, N, denote the angles of this triangle. Then, by means of [38] and [47], we find that
$$\sin w = \sin m \sin N = 2 \sin m \sin \tfrac{1}{2}N \cos \tfrac{1}{2}N$$
$$= \frac{2}{\sin l}\sqrt{\sin s \sin(s-l) \sin(s-m) \sin(s-n)},$$
where $s = \frac{1}{2}(l+m+n)$;
hence, $V = 2abc\sqrt{\sin s \sin(s-l) \sin(s-m) \sin(s-n)}$.
4. (i.) 9,976,500 square miles; (ii.) 13,316,600 square miles.
5. Let $m =$ longitude of point where the ship crosses the equator, $b =$ her course at the equator, $d =$ distance sailed. Then
$$\tan m = \sin l \tan a,\ \cos b = \cos l \sin a,\ \cot d = \cot l \cos a.$$
6. Let $k =$ arc of the parallel between the places, $x =$ difference required; then $\sin \frac{1}{2} k = \sin \frac{1}{2} d \sec l$. $x = 90° (\sqrt{2} - 1)$.
7. $\cos(m - m') = (\cos d - \sin l \sin l') \sec l \sec l'$; where m and m' are the longitudes of the places.
9. 12 hrs. 42 min. 41 sec., very nearly. 10. 60°.

11. $\cos t = -\tan d \tan l$; time of sunrise $= 12 - \frac{t}{15}$ o'clock A.M.; time of sunset $= \frac{t}{15}$ o'clock P.M.; $\cos a = \sin d \sec l$. For longest day at Boston: time of sunrise, 4 hrs. 26 min. 50 sec. A.M.; time of sunset, 7 hrs. 33 min. 10 sec. P.M. Azimuth of s[illegible]t these times, 57° 25′ 15″; length of day, 15 hrs. 6 min. 20 sec[illegible]or shortest day, times of sunrise and sunset are 7 hrs. 33 min. 10 sec. A.M. and 4 hrs. 26 min. 50 sec. P.M.; azimuth of sun, 122° 34′ 45″; length of day, 8 hrs. 53 min. 40 sec.

12. The problem is impossible when $\cot d < \tan l$; that is, for places in the frigid zone.

13. For the northern hemisphere and positive declination,
$\sin h = \sin l \sin d$, $\cot a = \cos l \tan d$.
Example: $h = 17° 14' 35''$, $a = 73° 51' 34''$ E.

14. The farther the place from the equator, the greater the sun's altitude at 6 A.M. in summer. At the equator it is 0°. At the north pole it is equal to the sun's declination. At a given place, the sun's altitude at 6 A.M. is a maximum on the longest day of the year, and then $\sin h = \sin l \sin e$ (where $e = 23° 27'$).

15. $\cos t = \cot l \tan d$. Times of bearing due east and due west are $12 - \frac{t}{15}$ o'clock A.M., and $\frac{t}{15}$ o'clock P.M., respectively.
Example: 6 hrs. 58 min. A.M. and 5 hrs. 2 min. P.M.

16. When the days and nights are equal, $d = 0°$, $\cos t = 0$, $t = 90°$; that is, sun is everywhere due east at 6 A.M., and due west at 6 P.M. Since l and d must both be less than 90°, $\cos t$ cannot be negative, therefore, t cannot be greater than 90°. As d increases, t decreases; that is, the times in question both approach noon. If $l < d$, then $\cos t > 1$; therefore this case is impossible. If $l = d$, then $\cos t = 1$, and $t = 0°$; that is, the times both coincide with noon. The explanation of this result is, that the sun at noon is in the zenith; hence on the prime vertical. At the pole $l = 90°$, $\cos t = 0$, $t = 90°$; therefore the sun in summer always bears due east at 6 A.M., and due west at 6 P.M.

17. $\sin l = \operatorname{sid} d \csc h$. 18. 11° 50′ 35″.

19. The bearing of the wall, reckoned from the north point of the horizon, is given by the equation $\cot x = \cos l \tan d$; whence, for the given case, $x = 75° 12' 38''$.

20. 55° 45′ 6″ N. 21. 63° 23′ 41″ N. or S.

22. (i.) $\cos t = -\tan l \tan d$; (ii.) $t = z$; (iii.) the result is indeterminate.

23. $\cot a = \cos l \tan d$. 28. $\sin d = \sin e \sin v$, $\tan r = \cos e \tan v$.

25. $h = 65° 37' 20''$. 29. $d = 32° 24' 12''$, $r = 301° 48' 17''$.

26. $h = 58° 25' 15''$, $a = 152° 28'$. 30. $d = 20° 48' 12''$.

27. $t = 45° 42'$, $l = 67° 58' 54''$. 31. 3 hrs. 59 min. $27\frac{1}{2}$ sec. P.M.

32. $\cos \frac{1}{2} a = \sqrt{\cos \frac{1}{2}(l + h + p) \cos \frac{1}{2}(l + h - p) \sec l \sec h}$.

SURVEYING.

CHAPTER I.

DEFINITIONS. INSTRUMENTS AND THEIR USES.

§ 1. DEFINITIONS.

Surveying is the art of determining and representing distances, areas, and the relative position of points upon the surface of the earth.

In plane surveying, the portion surveyed is considered as a plane.

In geodetic surveying, the curvature of the earth is regarded.

A **Plumb-Line** is a cord with a weight attached and freely suspended.

A **Vertical Line** is a line having the direction of the plumb-line.

A **Vertical Plane** is a plane embracing a vertical line.

A **Horizontal Plane** is a plane perpendicular to a vertical line.

A **Horizontal Line** is a line in a horizontal plane.

A **Horizontal Angle** is an angle the sides of which are in a horizontal plane.

A **Vertical Angle** is an angle the sides of which are in a vertical plane. If one side of a vertical angle is horizontal, and the other ascends, it is an *angle of elevation;* if one side is horizontal, and the other descends, it is an *angle of depression.*

The **Magnetic Meridian** is the direction which a bar-magnet assumes when freely supported in a horizontal position.

The **Magnetic Bearing** of a line is the angle it makes with the magnetic meridian.

Surveying commonly comprises three distinct operations; viz.:

1. The **Field Measurements**, or the process of determining by direct measurement certain lines and angles.
2. The **Computation** of the required parts from the measured lines and angles.
3. The **Plotting**, or representing on paper the measured and computed parts in relative extent and position.

THE MEASUREMENT OF LINES.

§ 2. INSTRUMENTS FOR MEASURING LINES.

The **Gunter's Chain** is generally employed in measuring land. It is 4 rods, or 66 feet, in length, and is divided into 100 links. Hence, links may be written as hundredths of a chain.

The **Engineer's Chain** is employed in surveying railroads, canals, etc. It is 100 feet long, and is divided into 100 links.

A **Tape Measure**, divided into feet and inches, is employed in measuring town-lots, cross-section work in railroad surveying, etc.

In the United States Coast and Geodetic Survey, the meter is the unit; and, when great accuracy is required, **rods** placed end to end, and brought to a horizontal position by means of a spirit-level, are employed in measuring lines.

§ 3. CHAINING.

Eleven tally-pins of iron or steel are used in chaining; also, one or more slender poles shod with iron, and bearing a flag.

A forward chainman, or leader, and a hind chainman, or follower, are required. A flag-staff having been placed at the farther end of the line, or at some point in the line visible from the beginning, the follower takes one end of the chain, and a pin which he thrusts into the ground at the beginning of the line. The leader moves forward in the direction of the flag-staff, with the other end of the chain and the remaining ten pins, until the word "halt" from the follower warns him that he has advanced nearly the length of the chain.

At this signal he stops, and the follower, meanwhile having placed his end of the chain at the beginning of the line, directs the leader by the words "right" or "left" until the chain is exactly in line with the flag-staff. This being accomplished, and the chain stretched tightly in a horizontal position, the follower says, "down." The leader then puts in a tally-pin exactly at the end of the chain, and answers, "down"; after which the follower withdraws the pin at the beginning of the line, and the chainmen move forward until the follower nears the pin set by the leader. The follower again says, "halt," and the operation just described is repeated. This process is continued until the end of the line is reached.

If the tally-pins in the hands of the leader are exhausted before the end of the line is reached, when he has placed the last pin in the ground, he waits until the follower comes up to him. The follower gives the leader the ten pins in his hand, and records the fact that ten chains have been measured. The measuring then proceeds as before. If the distance from the last pin to the end of the line is less than a chain, the leader places his end of the chain at the end of the line, and the follower stretches tightly such a part of the chain as is necessary to reach to the last pin, and the number of links is counted. The number of whole chains is indicated by the number of pins in the hands of the follower, *the last pin remaining in the ground.*

In measuring, the chain must be held in a horizontal position. If the ground slopes, one end of the chain must be raised until the horizontal position is attained. By means of a plumb-line, or a slender staff, or, less accurately, by dropping a pin (heavy end downwards), the point vertically under the raised end of the chain may be determined. If the slope is considerable, half a chain or less may be used.

To construct a perpendicular with a chain:

1. When the point through which the perpendicular is to pass is in the line:

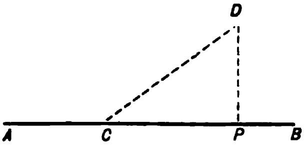


Fig. 1.

Let *AB* (Fig. 1) represent the line, and *P* the point. Measure from *P* to the right or left, *PC* = 40 links, and place a stake at *C*. Let one end of the chain be held at *P*, and the end of the eightieth link at *C*; then, taking the chain at the end of the thirtieth link from *P*, draw it so that the portions *DC* and *DP* are tightly stretched, and place a stake at *D*. *DP* will be the perpendicular required. (Why?)

2. When the point is without the line:

Let *AB* (Fig. 1) be the line, and *D* the point. Take *C* any point in the line, and stretch the chain between *D* and *C*; then, let the middle of the part of the chain between *C* and *D* be held in place, and swing the end at *D* around until it meets the line in *P*. *DP* will be the perpendicular required. (Why?)

§ 4. OBSTACLES TO CHAINING.

1. When a tree, building, or other obstacle is encountered in measuring or extending a line, it may be passed by an offset in the following manner:

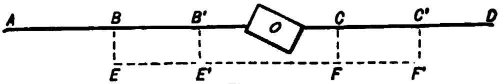


Fig. 2.

Let *O* (Fig. 2) represent a building on the line *AD*. At *B* erect *BE* perpendicular to *AB*; at *E* erect *EF* perpendicular to *BE*; at *F* erect *FC* = *BE* perpendicular to *EF*; then, *CD* perpendicular to *FC* will be in the required line, and $AB + EF + CD = AD$. By constructing two other perpendiculars, *B'E'* and *F'C'*, the accuracy of the work will be increased.

2. To measure across a body of water:

Let it be required to measure the line $ABCD$ (Fig. 3) crossing a river between B and C. Measure $BE = 400$ links; at E erect the perpendicular $EF = 600$ links; at B erect the perpendicular $BG = 300$ links. Place a stake at C, the intersection of AD and FG beyond the river.

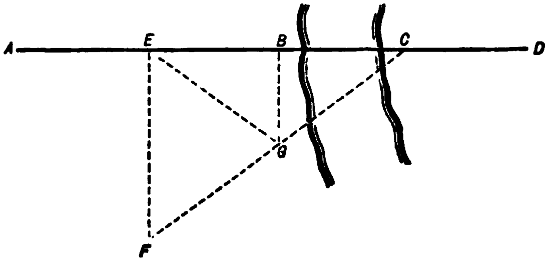


Fig. 3.

Then $BC = 400$ links. For, by similar triangles, $EF : BG :: CE : CB$. But $EF = 2\,BG$; hence, $CE = 2\,CB$, and $CB = BE = 400$ links. EG and FG should be measured, in order to test the accuracy of the work. $EG = FG = 500$ links.

Instead of the above distances, any convenient distances may be taken. For, if $EF = 2\,BG$, then $CB = BE$, and $EG = FG = \sqrt{\overline{EB}^2 + \overline{BG}^2}$.

3. To measure a line the end of which is invisible from the beginning, and intermediate points unknown:

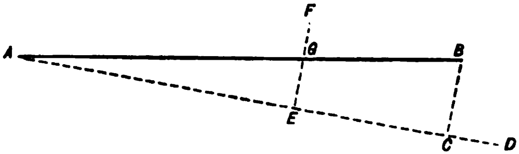


Fig. 4.

Let AB (Fig. 4) represent the line. Set up a flag-staff at D, beyond B and visible from A. From B let fall BC perpendicular to AD. Measure AC and BC. Then

$$AB = \sqrt{\overline{AC}^2 + \overline{BC}^2}.$$

To find intermediate points on AB:

At any point E on AC erect EF perpendicular to AC, and determine EG by the proportion $AC : CB :: AE : EG$. G will be a point on AB.

The line AD is called a **Random Line.**

THE MEASUREMENT OF ANGLES.

§ 5. THE VERNIER COMPASS.*

The **Vernier Compass** is shown on the following page.

The *compass circle* is divided into half-degrees, and is figured from 0° to 90° each way from the north and south points. In the centre of the compass circle is the *pivot* which supports the *magnetic needle*. The needle may be lifted from the pivot by a spring and pressed against the glass covering of the compass circle, when the instrument is not in use. The *main plate* moves around the compass circle through a small arc, read by the *vernier*, for the purpose of allowing for the variation of the needle (§ 23). The *sight standards* at the extremities of the main plate have fine slits nearly their whole length, with circular openings at intervals; on the edges of the north standard *tangent scales* are placed; and on the outside of the south standard two *eye-pieces* at the same distance from the main plate as the zeros of the tangent scales, respectively. The *telescopic sight* (a recent improvement by the Messrs. Gurley), consists of a small telescope attached to the south standard. The main plate is furnished with two *spirit levels* at right angles, and turns horizontally upon the upper end of the *ball spindle*, the lower end of which rests in a spherical socket in the top of the *tripod* or *Jacob's staff* which supports the instrument. From the centre of the plate at the top of the tripod a plumb-bob is suspended by which the centre of the compass can be placed directly over a definite point on the ground.

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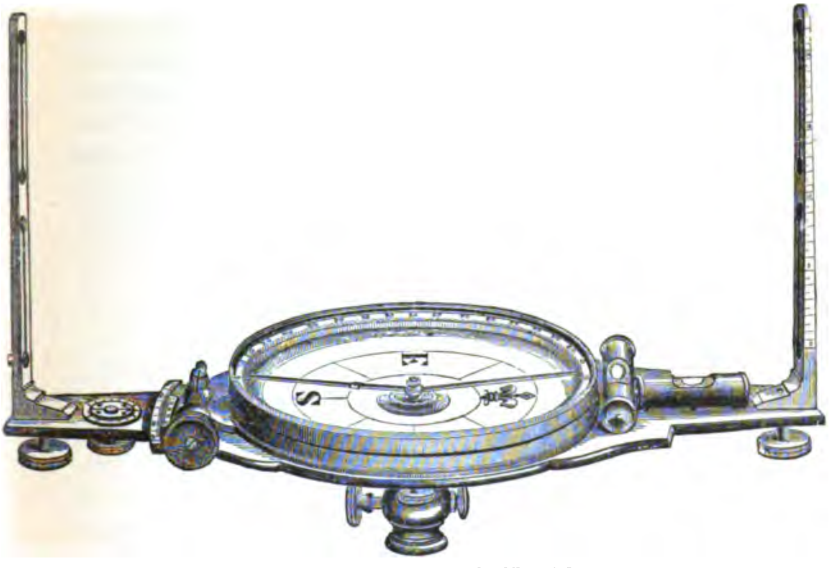
* The instruments described on this and the following pages are adjusted by the maker. If they should require readjustment, full directions will be found in the manual furnished with the instruments.

The manual published by Messrs. W. & L. E. GURLEY, Troy, N.Y., has been freely used, by permission, in describing these instruments.



THE VERNIER COMPASS.

§ 6. USES OF THE COMPASS.

To take the bearing* of a line. Place the instrument so that the bob will be directly over one end of the line, and level by pressing with the hands on the main plate until the bubbles are brought to the middle of the spirit levels. Turn the south end of the instrument toward you, and sight at the flag-staff at the other end of the line. Read the bearing from the north end of the needle. First, write N. or S. according as the north end of the needle is nearer N. or S. of the compass circle; secondly, write the number of degrees between the north end of the needle and the nearest zero mark; and thirdly, write E. or W. according as the north end of the needle is nearer E. or W. of the compass circle.

In Fig. 5 the bearing would be N. 45° W.
In Fig. 6 the bearing would be S. 45° W.
In Fig. 7 the bearing would be S. 30° E.
In Fig. 8 the bearing would be N. 60° E.

If the needle coincides with the N.S. or E.W. line, the bearing would be N., S., E., or W., according as the north end of the needle is over N., S., E., or W.

As the compass circle is divided into half-degrees, the bearing may be determined pretty accurately to quarter-degrees.

When a fence or other obstruction interferes with placing the instrument over the line, it may be placed at one side, the flag-staff being placed at an equal distance from the line.

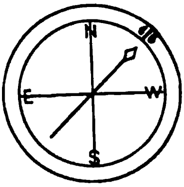


Fig. 5.

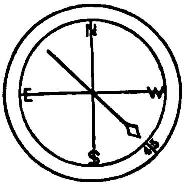


Fig. 6.

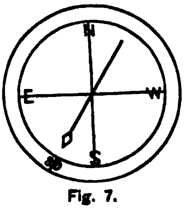


Fig. 7.

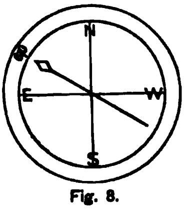


Fig. 8.

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* The magnetic bearing is meant unless otherwise specified.

Local Disturbances. Before a bearing is recorded, care should be exercised that the chain, pins, and other instruments that would affect the direction of the needle, are removed from the vicinity of the compass. Even after the greatest care in this respect is exercised, the direction of the needle is often affected by iron ore, ferruginous rocks, etc.

Reverse Bearings. When the bearing of a line has been taken, the instrument should be removed to the other end of the line and the reverse bearing taken. The number of degrees should be the same as before, but the letters should be reversed.

To take the bearing of a line one end of which cannot be seen from the other. Run a random line (§ 4, 3); then (Fig. 4),

$$\tan CAB = \frac{BC}{AC};$$

whence, the angle *CAB* may be found. This angle combined with the bearing of the random line will give the bearing required.

Another method will be given in § 19.

To measure a horizontal angle by means of the needle. Place the compass over the vertex of the angle, take the bearing of each side separately, and combine these bearings.

To measure angles of elevation. Bring the south end of the compass towards you, place the eye at the lower eye-piece, and with the hand hold a card on the front side of the north sight, so that its top edge will be at right angles to the divided edge and coincide with the zero mark; then, sighting over the top of the card, note upon a flag-staff the height cut by the line of sight; move the staff up the elevation, and carry the card along the edge of the sight until the line of sight again cuts the same height on the staff; read off the degrees of the tangent scale passed over by the card.

To measure angles of depression. Proceed in the same manner as above, using the eye-piece and tangent scale on the opposite sides of the sights, and reading from the top of the sight.

§ 7. VERNIERS.

First form. Let *AB* (Fig. 9) represent a portion of a rod for measuring heights (§ 32). The graduation to feet and hundredths of a foot begins at the lower end, which rests on the ground when the rod is in use. The line extending nearly across the rod at the bottom of the portion shown marks the beginning of the fourth foot. The face of the rod is divided into four columns: in the first is written the number of feet; in the second, the number of tenths; and in the third, the number of hundredths.

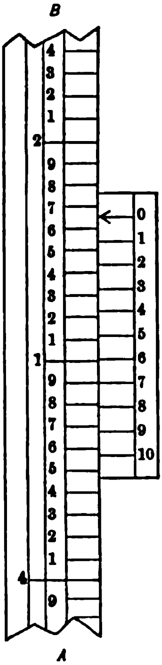


Fig. 9.

It is evident that, with the arrangement just described, heights could be measured only to hundredths of a foot. To enable us to find the height more precisely, a contrivance called a **Vernier** is used. This is shown at the right of the rod. It consists of a piece of metal or wood, the graduated part of which is $\frac{11}{100}$ of a foot in length; and this is divided into ten equal parts. Hence, one division of the vernier $= \frac{1}{10}$ of $\frac{11}{100} = \frac{11}{1000}$ of a foot; and one division of the vernier exceeds one division of the rod by $\frac{11}{1000} - \frac{1}{100} = \frac{1}{1000}$ of a foot.

The vernier slides along the face or side of the rod.

To use the vernier, place the lower end of the rod upon the ground, and move the vernier until its index or zero mark is opposite the point whose distance from the ground is desired. In the figure, the height of the index of the vernier is evidently 4.16 feet, increased by the distance of the index above the next lower line (4.16) of the rod. We shall now determine this distance.

Observe which line of the vernier is exactly opposite a line of the rod. In this case, the line of the vernier numbered 7 is opposite a line of the rod. Then, since each division of the vernier exceeds each division of the rod by $\frac{1}{1000}$ of a foot,

6 of the vernier is $\frac{1}{1000}$ of a foot above the next lower line of the rod.
5 of the vernier is $\frac{2}{1000}$ of a foot above the next lower line of the rod.
4 of the vernier is $\frac{3}{1000}$ of a foot above the next lower line of the rod.
3 of the vernier is $\frac{4}{1000}$ of a foot above the next lower line of the rod.
2 of the vernien is $\frac{5}{1000}$ of a foot above the next lower line of the rod.
1 of the vernier is $\frac{6}{1000}$ of a foot above the next lower line of the rod.
0 of the vernier is $\frac{7}{1000}$ of a foot above the next lower line of the rod.

Hence, the required reading is $4.16 + .007 = 4.167$ feet.

In general, the following rule is evident:

Move the vernier until its zero line is at the required height; read the height to the nearest hundredth below the index, and write in the thousandths' place the number of the division line of the vernier which stands opposite any line of the rod.

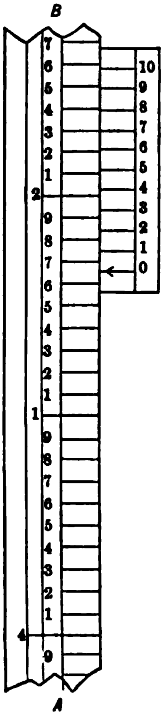


Fig. 10.

Second form. In this form (Fig. 10) the graduated part of the vernier is $\frac{9}{100}$ of a foot in length, and is divided into ten equal parts. Hence, one division of the vernier $= \frac{1}{10}$ of $\frac{9}{100} = \frac{9}{1000}$ of a foot; and one division of the vernier is less than one division of the rod by $\frac{1}{100} - \frac{9}{1000} = \frac{1}{1000}$ of a foot.

The height of the index of the vernier in Fig. 10 is 4.16 feet, increased by the distance of the index from the next lower line (4.16) of the rod. We shall now determine this distance.

We observe that the line of the vernier numbered 7 stands exactly opposite a line (3) of the rod. Hence,

6 of the vernier is $\frac{1}{1000}$ of a foot above the next lower line of the rod.
5 of the vernier is $\frac{2}{1000}$ of a foot above the next lower line of the rod.
4 of the vernier is $\frac{3}{1000}$ of a foot above the next lower line of the rod.
3 of the vernier is $\frac{4}{1000}$ of a foot above the next lower line of the rod.
2 of the vernier is $\frac{5}{1000}$ of a foot above the next lower line of the rod.
1 of the vernier is $\frac{6}{1000}$ of a foot above the next lower line of the rod.
0 of the vernier is $\frac{7}{1000}$ of a foot above the next lower line of the rod.

Hence, the required reading is $4.16 + .007 = 4.167$ feet; and the rule is evidently the same as for the first form.

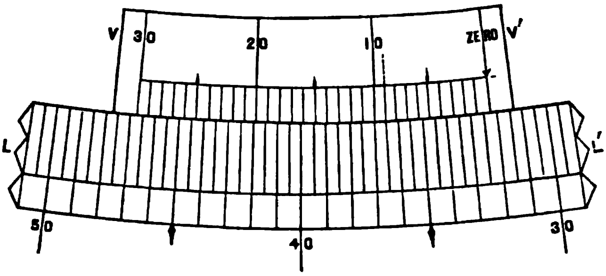


Fig. 11.

Compass Verniers. Let *LL'* (Fig. 11) represent the limb of the compass graduated to half-degrees, and *VV'* the vernier divided into thirty equal spaces, equal to twenty-nine spaces of the limb. Then one space of the vernier is less than one space of the limb by 1', and the reading may be obtained to single minutes.

In Fig. 11 the index or zero of the vernier stands between 32° and 32° 30', and the line of the vernier marked 9 coincides with a line of the limb. Hence, the reading is 32° 9'.

When the index moves from the zero line of the limb in a direction contrary to that in which the numbers of the limb run, the number of minutes obtained as above must be subtracted from 30' to obtain the minutes required.

If, however, the vernier be made double, that is, if it have thirty spaces on each side of the zero line, it is always read directly. The usual form of the double vernier, shown in

Fig. 12, has only fifteen spaces on each side of the zero line. When the vernier is turned to the *right* less than 15′ past a division line of the limb, read the lower figures on the *left* of the zero line at any coincidence; if moved more than 15′ past a division line of the limb, read the upper figures on the *right* of the zero line at any coincidence; and *vice versa*.

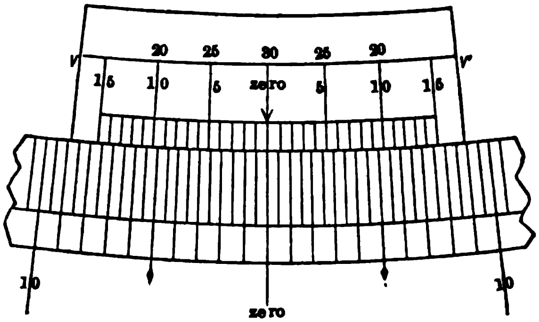


Fig. 12.

Uses of the Compass Vernier. The most important use of the vernier of the vernier compass is in setting off the variation of the needle (§ 23). If the variation of the needle at any place is known, by means of the vernier screw the compass circle may be turned through an arc equal to the variation. If the observer stands at the south end of the instrument, the vernier is turned to the right or left according as the variation is west or east. The compass will now give the bearings of the lines with the *true meridian*.

In order to retrace the lines of an old survey, turn the sights in the direction of a known line, and move the vernier until the needle indicates the old bearing. The arc moved over by the vernier will indicate the change of variation since the time of the old survey. If no line is definitely known, the *change of variation* from the time of the old survey will give the arc to be set off.

§ 8. THE SURVEYOR'S TRANSIT.

This instrument is shown on page 17.

The *compass circle* is similar to that of the compass. The *vernier plate* which carries the *telescope* has two *verniers* and moves entirely around the *graduated limb* of the main plate. The axis of the telescope carries a *vertical circle* which measures vertical angles to single minutes by means of a vernier. Under the telescope, and attached to it, is a *spirit level* by means of which horizontal lines may be run, or the difference of level between two stations found. The *cross wires* are two fine fibres of spider's web, or fine platinum wires, which extend across the tube of the telescope at right angles to each other; their intersection determines the *optical axis* or *line of collimation* of the telescope. The transit is levelled by four *levelling screws* which pass through a plate firmly fastened to the ball spindle, and the lower ends of which rest in depressions on the upper side of the tripod plate.

Two recent improvements (introduced by the Messrs. Gurley) enable the surveyor to bring the transit quickly to an approximately level position by the pressure of the hands, after which the levelling screws are used; also, to change the position of the transit without changing the position of the tripod legs, so as to bring the bob exactly over any point.

To level the transit by the levelling screws. Turn the instrument until the spirit levels on the vernier plate are parallel to the vertical planes passing through opposite pairs of levelling screws. Take hold of opposite screw heads with the thumb and fore-finger of each hand, and turn both thumbs in or out as may be necessary to raise the lower side of the parallel plate and lower the other until the desired correction is made.

To use the telescope. Both the eye-piece and the object glass may be moved in and out by a rack-and-pinion movement. The eye-piece must be moved until the cross wires are perfectly distinct; in which case, a slight movement of the eye of the observer, from side to side, will produce no apparent change in the position of the threads upon the object. The object glass must be moved until the object is distinctly visible; and this operation must be repeated whenever the distance of the object is changed.

§ 9. USES OF THE TRANSIT.

The transit may be used for all the purposes indicated in § 6, but with much greater precision than the compass. *The principal use, however, of the transit is in measuring horizontal angles by means of the graduated limb and verniers.*

To measure a horizontal angle with the transit. Place the transit over the vertex of the angle; level, and set the limb at zero. Turn the telescope in the direction of one of the sides of the angle, clamp to the spindle; unclamp the main plate, and turn the telescope until it is in the direction of the other side of the angle, and read the angle by the verniers. The object of the two verniers on the vernier plate is to correct any mistake that might arise from the want of exact coincidence in the centres of the verniers and the limb. The correct reading may be obtained by adding to the reading of one vernier the supplement of the reading of the other, and dividing by 2.

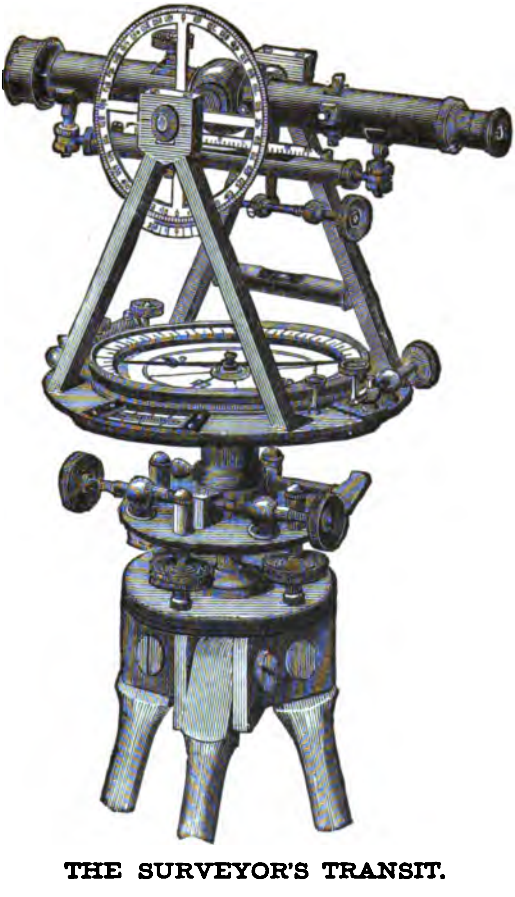
By turning off a right angle by this method, perpendiculars may be constructed with much greater facility than by the chain.

§ 10. THE THEODOLITE.

The telescope of the transit can perform a complete revolution on its axis; whence the name *transit*. The theodolite differs from the transit chiefly in that its telescope cannot be so revolved. It is not much used in this country.

§ 11. THE RAILROAD COMPASS.

This instrument has all the features of the ordinary compass, and has also a vernier plate and graduated limb for measuring horizontal angles.



THE SURVEYOR'S TRANSIT.

§ 12. PLOTTING.

The principal plotting instruments are a ruler, pencil, straight-line pen, hair-spring dividers, diagonal scale, a right triangle of wood, and a circular protractor. A T-square will also be found convenient.

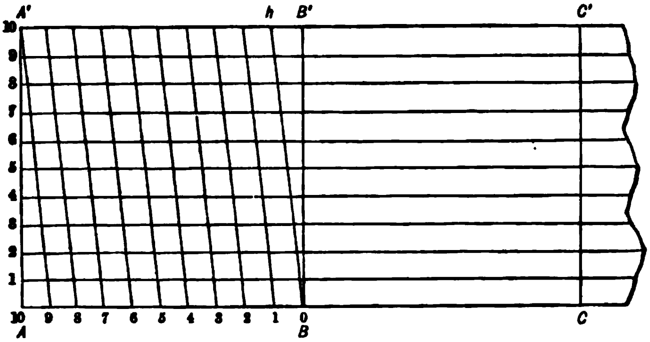


Fig. 13.

The Diagonal Scale. A portion of this scale is shown in Fig. 13. AB is the unit. AB and $A'B'$ are divided into ten equal parts, and B is joined with h, the first division point to the left of B'; the first division point to the left of B is joined with the second to the left of B', etc.

The part of the horizontal line numbered 1 intercepted between BB' and Bh is evidently $\frac{1}{10}$ of $\frac{1}{10} = \frac{1}{100}$ of the unit; the part of the horizontal line numbered 2 intercepted between BB' and Bh is $\frac{2}{100}$ of the unit, etc.

The method of using this scale, in laying off distances, will be made plain by the following example:

Let it be required to lay off the distance 1.43.

Place one foot of the dividers at the intersection of the horizontal line numbered 3 and the diagonal numbered 4, and place the other foot at the intersection of the vertical line numbered 1 (CC') and the horizontal line numbered 3; the distance between the feet of the dividers will be the distance required. For, measuring along the horizontal line numbered 3, from CC' to BB' is 1; from BB' to Bh is .03; and from Bh to the diagonal numbered 4 is .4; and $1 + .03 + .4 = 1.43$.

The Circular Protractor. This instrument (Fig. 14) usually consists of a semi-circular piece of brass or german silver, having its arc divided into degrees and its centre marked.

To lay off an angle with the protractor, place the centre over the vertex of the angle, and make the diameter coincide with the given side of the angle. Mark off the number of degrees in the given angle, and draw a line through this point and the vertex.

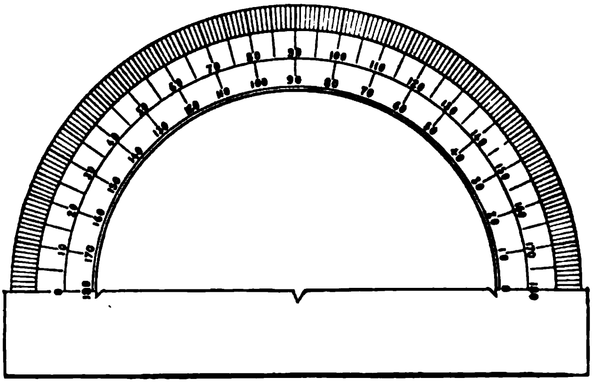


Fig. 14.

Some protractors have an arm which carries a vernier, by which angles may be constructed to single minutes.

To draw through a given point a line parallel to a given line, make one of the sides of a triangle coincide with the given line, and, placing a ruler against one of the other sides, move the triangle along the ruler until the first side passes through the given point; then draw a line along this side.

To draw through a given point a line perpendicular to a given line, make the hypotenuse of a right triangle coincide with the given line, and, placing a ruler against one of the other sides of the triangle, revolve the triangle about the vertex of the right angle as a centre until its other perpendicular side is against the ruler; then move the triangle along the ruler until the hypotenuse passes through the given point, and draw a line along the hypotenuse.

CHAPTER II.

LAND SURVEYING.

§ 13. DEFINITION.

Land Surveying is the art of measuring, laying out, and dividing land, and preparing a plot.

§ 14. DETERMINATION OF AREAS.

The unit of land measure is the

$$\begin{aligned} \text{acre} &= 10 \text{ square chains} \\ &= 4 \text{ roods} \\ &= 160 \text{ square rods, perches, or poles.} \end{aligned}$$

Areas are referred to the horizontal plane, no allowance being made for inequalities of surface.

For convenience of reference, the following rules for areas are given:

Let A, B, and C be the angles of a triangle, and a, b, and c the opposite sides, respectively; and let $s = \frac{1}{2}(a+b+c)$.

$$\begin{aligned} \text{Area of triangle } ABC &= \sqrt{s(s-a)(s-b)(s-c)} && [\text{A}] \\ &= \tfrac{1}{2} bc \sin A && [\text{B}] \\ &= \tfrac{1}{2} \frac{a^2 \sin B \sin C}{\sin(B+C)} && [\text{C}] \\ &= \tfrac{1}{2} \text{ base} \times \text{altitude.} && [\text{D}] \end{aligned}$$

Area of rectangle = base × altitude.

Area of trapezoid = ½ sum of parallel sides × altitude.

PROBLEM 1. To determine the area of a triangular field.

Measure the necessary parts with a Gunter's chain, or with a chain and transit, and compute by formula [A], [B], [C], or [D].

Problem 2. To find the area of a field having any number of straight sides.

(*a*) Divide the field into triangles by diagonals; find the area of each triangle and take the sum.

(*b*) Run a diagonal, and perpendiculars from the opposite vertices to this diagonal. The field is thus divided into right triangles, rectangles, and trapezoids, the areas of which may be found and the sum taken.

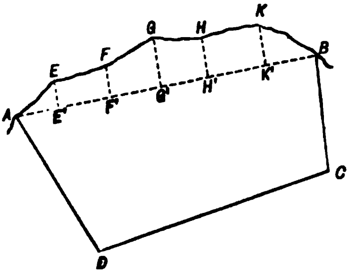


Fig. 15.

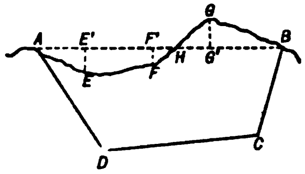


Fig. 16.

Problem 3. To find the area of a field having an irregular boundary line.

(*a*) Let *AGBCD* (Fig. 15) represent a field having a stream *AEFGHKB* as a boundary line. Run the line *AB*. From *E*, *F*, *G*, *H*, and *K*, prominent points on the bank of the stream, let fall perpendiculars *EE'*, *FF'*, etc., upon *AB*. Regarding *AE*, *EF*, etc., as straight lines, the portion of the field cut off by *AB* is divided into right triangles, rectangles, and trapezoids, the necessary elements of which can be measured and the areas computed. The sum of these areas added to the area of *ABCD* will give the area required.

(*b*) When the irregular boundary line crosses the straight line joining its extremities, as in Fig. 16, the areas of *AEFH* and *HGB* may be found separately, as in the preceding case. Then the area required = *ABCD* + *HGB* – *AEFH*.

Problem 4. To determine the area of a field from two interior stations.

Let *ABCD* (Fig. 17) represent a field, and *P* and *P'* two stations within it. Measure *PP'* with great exactness. Measure the angles between *PP'* and the lines from *P* and *P'* to the corners of the field.

In the triangle $PP'D$, PP' and the angles $P'PD$ and $PP'D$ are known; hence, PD may be found. In like manner, PC may be found. Then, in the triangle PDC, PD, PC, and the angle DPC are known; hence, the area of PDC may be computed.

In like manner, the areas of all the triangles about P and P' may be determined.

Area $ABCD = PAD + PDC + PCB + PBA$. Also,

Area $ABCD = P'AD + P'DC + P'CB + P'BA$.

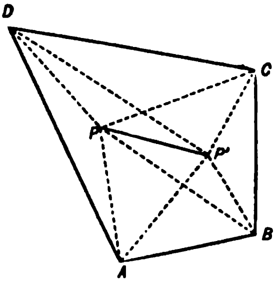


Fig. 17.

PROBLEM 5. **To determine the area of a field from two exterior stations.**

Let $ABCD$ (Fig. 18) represent the field, and P and P' the stations. Determine the areas of the triangles PAD, PDC, PCB, and PBA, as in the preceding problem.

Area $ABCD = PAD + PDC + PBC - PBA$. Also,

Area $ABCD = P'AD + P'DC + P'BA - P'BC$.

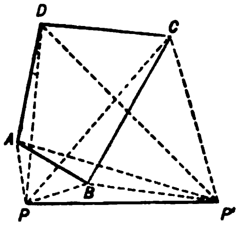


Fig. 18.

EXERCISE I.

1. Required the area of a triangular field whose sides are respectively 13, 14, and 15 chains.

2. Required the area of a triangular field whose sides are respectively 20, 30, and 40 chains.

3. Required the area of a triangular field whose base is 12.60 chains, and altitude 6.40 chains.

4. Required the area of a triangular field which has two sides 4.50 and 3.70 chains, respectively, and the included angle 60°.

5. Required the area of a field in the form of a trapezium, one of whose diagonals is 9 chains, and the two perpendiculars upon this diagonal from the opposite vertices 4.50 and 3.25 chains.

6. Required the area of the field $ABCDEF$ (Fig. 19), if $AE = 9.25$ chains, $FF' = 6.40$ chains, $BE = 13.75$ chains, $DD' = 7$ chains, $DB = 10$ chains, $CC' = 4$ chains, and $AA' = 4.75$ chains.

7. Required the area of the field $ABCDEF$ (Fig. 20), if $AF' = 4$ chains, $FF' = 6$ chains, $EE' = 6.50$ chains, $AE' = 9$ chains, $AD = 14$ chains, $AC' = 10$ chains, $AB' = 6.50$ chains, $BB' = 7$ chains, $CC' = 6.75$ chains.

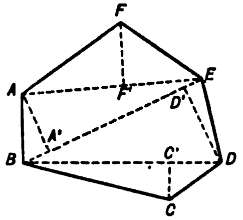


Fig. 19.

8. Required the area of the field $AGBCD$ (Fig. 15), if the diagonal $AC = 5$, BB' (the perpendicular from B to AC) $= 1$, DD' (the perpendicular from D to AC) $= 1.60$, $EE' = 0.25$, $FF' = 0.25$, $GG' = 0.60$, $HH' = 0.52$, $KK' = 0.54$, $AE' = 0.2$, $E'F' = 0.50$, $F'G' = 0.45$, $G'H' = 0.45$, $H'K' = 0.60$, and $K'B = 0.40$.

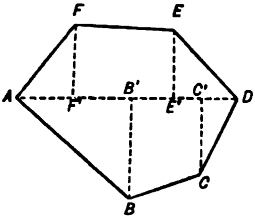


Fig. 20.

9. Required the area of the field $AGBCD$ (Fig. 16), if $AD = 3$, $AC = 5$, $AB = 6$, angle $DAC = 45°$, angle $BAC = 30°$, $AE' = 0.75$, $AF' = 2.25$, $AH = 2.53$, $AG' = 3.15$, $EE' = 0.60$, $FF' = 0.40$, and $GG' = 0.75$.

10. Determine the area of the field $ABCD$ from two interior stations, P and P', if $PP' = 1.50$ chains,

angle $PP'C = 89° 35'$,	angle $P'PB = 3° 35'$,
$PP'B = 185° 30'$,	$P'PA = 113° 45'$,
$PP'A = 309° 15'$,	$P'PD = 165° 40'$,
$PP'D = 349° 45'$,	$P'PC = 303° 15'$.

11. Determine the area of the field $ABCD$ from two exterior stations P and P', if $PP' = 1.50$ chains,

angle $P'PB = 41° 10'$,	angle $PP'D = 66° 45'$,
$P'PA = 55° 45'$,	$PP'C = 95° 40'$,
$P'PC = 77° 20'$,	$PP'B = 132° 15'$,
$P'PD = 104° 45'$,	$PP'A = 103° 0'$.

RECTANGULAR SURVEYING.

§ 15. DEFINITIONS.

An **East and West Line** is a line perpendicular to the magnetic meridian.

The **Latitude** of a line is the distance between the east and west lines through its extremities.

The **Departure** of a line is the distance between the meridians through its extremities.

NOTE. When a line extends north of the initial point the latitude is called a northing; when it extends south, a southing; when it extends east the departure is called an easting; when it extends west, a westing.

The **Meridian Distance** of a point is its distance from a meridian.

Let AB (Fig. 21) represent a line, and NAS the magnetic meridian. Let BB' be perpendicular to NS.

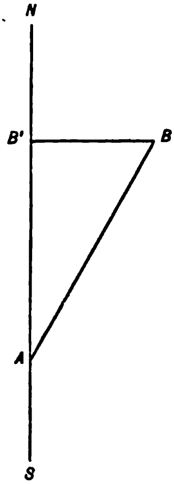


Fig. 21.

The bearing of the line AB is the angle BAB'.

The latitude of the line AB is AB'.

The departure of the line AB is BB'.

The meridian distance of the point B is BB'.

In the right triangle ABB',

$$AB' = AB \times \cos BAB',$$

and

$$BB' = AB \times \sin BAB'.$$

Hence, *latitude = distance × cos of bearing*,
and *departure = distance × sin of bearing*.

The latitudes and departures corresponding to any distance and bearing may be found from the above formulas by means of a table of natural sines and cosines, or from "The Traverse Table." *

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* See Table VII. of Wentworth & Hill's Five-Place Logarithmic and Trigonometric Tables.

§ 16. Field Notes, Computation, and Plotting.

The field notes are kept in a book provided for the purpose. The page is ruled in three columns, in the first of which is written the number of the station; in the second, the bearing of the side; and in the third, the length of the side.

Example 1. To survey the field *ABCD* (Fig. 22).

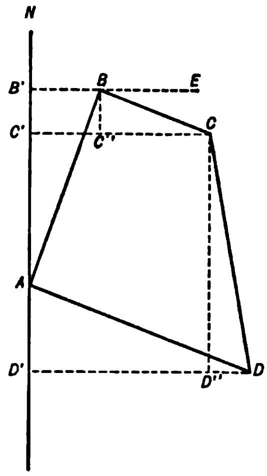


Fig. 22.

Field Notes.

1	N. 20° E.	8.66
2	S. 70° E.	5.00
3	S. 10° E.	10.00
4	N. 70° W.	10.00

(*a*) To obtain the field notes.

Place the compass at *A*, the first station, and take the bearing of *AB* (§ 6); suppose it to be N. 20° E. Write the result in the second column of the field notes opposite the number of the station. Measure $AB = 8.66$ chains, and write the result in the third column of the field notes.

Place the compass at *B*, and, after testing the bearing of *AB* (§ 6), take the bearing of *BC*, measure *BC*, and write the results in the field notes; and so continue until the bearing and length of each side have been recorded.

(*b*) To compute the area.

I.	II.	III.	IV.	V.	VI.	VII.	VIII.	IX.	X.	XI.
Side.	*Bearing.*	*Dist.*	*N.*	*S.*	*E.*	*W.*	*M.D.*	*D.M.D.*	*N.A.*	*S.A.*
AB	N. 20° E.	8.66	AB' 8.14	....	BB' 2.96	...	BB' 2.96	BB' 2.96	$2ABB'$ 24.0944	
BC	S. 70° E.	5.00	....	$B'C'$ 1.71	CC'' 4.70	...	CC' 7.66	$BB'+CC'$ 10.62	....	$2C'CBB'$ 18.1602
CD	S. 10° E.	10.00	....	$C'D'$ 9.85	DD'' 1.74	...	DD' 9.40	$CC'+DD'$ 17.06	....	$2D'DCC'$ 168.0410
DA	N. 70° W.	10.00	$D'A$ 3.42	....	....	DD' 9.40	0	DD' 9.40	$2ADD'$ 32.1480	
									56.2424	186.2012

The survey may begin at any corner of the field; but in computing the area, the field notes should be arranged so that the most eastern or most western station will stand first. For the sake of uniformity, we shall always begin with the most *western* station, and keep the field on the *right* in passing around it.

$$\begin{array}{r|l}
 & 186.2012 \\
 & \underline{56.2424} \\
2 & 129.9588 \\
10 & 64.98 \text{ sq. chains.} \\
 & 6.498 \text{ acres.}
\end{array}$$

The field notes occupy the first three of the eleven columns in the above tablet. Columns IV., V., VI., and VII. contain the latitudes and departures corresponding to the sides, and taken from the Traverse Table. The lines represented by these numbers are indicated immediately above each number. Column VIII. contains the meridian distances of the points B, C, D, and A, taken in order. Column IX. contains the double meridian distances. Their composition is indicated by the letters immediately above the numbers. Column X. contains the products of the double meridian distances by the northings in the same line. The first number,

$$24.0944 = 2.96 \times 8.14 = BB' \times AB' = 2 \text{ area of the triangle } ABB';$$
$$32.1480 = 9.40 \times 3.42 = DD' \times AD' = 2 \text{ area of the triangle } ADD'.$$

Column XI. contains the products of the double meridian distances by the southings in the same line. The first number,

$$\begin{aligned}18.1602 = 10.62 \times 1.71 &= (BB' + CC') \times B'C' \\ &= 2 \text{ area of the trapezoid } C'CBB'; \\ 168.0410 = 17.06 \times 9.85 &= (CC' + DD') \times D'C' \\ &= 2 \text{ area of the trapezoid } D'DCC'.\end{aligned}$$

The sum of the north areas in column X.

$$= 56.2424 = 2(ABB' + ADD').$$

The sum of the south areas in column XI.

$$= 186.2012 = 2(C'CBB' + D'DCC').$$

But $(C'CBB' + D'DCC') - (ABB' + ADD') = ABCD.$

Hence, $2(C'CBB' + D'DCC') - 2(ABB' + ADD') = 2ABCD;$

that is, $186.2012 - 56.2424 = 129.9588 = 2ABCD.$

Hence, area $ABCD = \frac{1}{2}$ of $129.9588 = 64.9794$ sq. ch. $= 6.498$ acres.

(*c*) To make the plot.

The plot or map may be drawn to any desired scale. If a line one inch in length in the plot represents a line one chain in length, the plot is said to be drawn to a scale of one chain to an inch. In this case the plot (Fig. 22) is drawn to a scale of eight chains to an inch.

Draw the line NAS to represent the magnetic meridian, and lay off the first northing $AB' = 8.14$ (§ 12). Draw the indefinite line $B'E$ perpendicular to NS and lay off $B'B$, the first easting = 2.96. Join A and B; then the line AB will represent the first side of the field. Through B draw BC'' perpendicular to BB', and make BC'' = 1.71, the first southing. Through C'' draw $C''C$ perpendicular to BC'', and equal to 4.70, the second easting. Join B and C. The line BC will represent the second side of the field.

Proceed in like manner until the field is completely represented. The extremity of the last line $D'A$, measured from D', should fall at A. This will be a test of the accuracy of the plot.

By drawing the diagonal AC, and letting fall upon it perpendiculars from B and D, the quadrilateral $ABCD$ is divided into two triangles, the bases and altitudes of which may be measured and the area computed approximately.

Other methods of plotting will suggest themselves, but the method just explained is one of the best.

Balancing the Work.

In the survey, we pass entirely around the field; hence, we move just as far north as south. Therefore, the sum of the northings should equal the sum of the southings. In like manner, the sum of the eastings should equal the sum of the westings. In this way the accuracy of the field work may be tested.

In Example 1, the sum of the northings is equal to the sum of the southings, being 11.56 in each case; and the sum of the eastings is equal to the sum of the westings, being 9.40 in each case. Hence, the work balances.

In actual practice the work seldom balances. When it does not balance, corrections are generally applied to the latitudes and departures, by the following rules:

The perimeter of the field : any one side
:: total error in latitude : correction;
:: total error in departure : correction.

If special difficulty has been experienced in taking a particular bearing, or in measuring a particular line, the corrections should be applied to the corresponding latitudes and departures.

The amount of error allowable varies in the practice of different surveyors, and according to the nature of the ground. An error of 1 link in 8 chains would not be considered too great on smooth, level ground; while, on rough ground, an error of 1 link in 2 or 3 chains might be allowed. If the error is considerable, the field measurements should be repeated.

Side.	Bearing.	Dist.	N.	S.	E.	W.	N'.	S'.	E'.	W'.	M. D.	D. M. D.	N. A.	S. A.
AB	N. 20° 00' E.	11.18	10.51	. . .	3.82	. . .	*AB'* 10.51	. . .	*B'B* 3.82	. . . .	*B'B* 3.82	*B'B* 3.82	2 *ABB'* 40.1482	. . . .
BC	S. 43° 30' E.	5.00	. . .	3.63	3.44	. . .	. . . .	*B'C'* 3.63	*C'C* 3.44	. . . .	*C'C* 7.26	*B'B* + *C'C* 11.08	. . . .	2 *C'CBB'* 40.2204
CD	S. 13° 30' E.	10.00	. . .	9.72	2.33	. . .	. . . .	*C'D'* 9.72	*D''D* 2.33	. . . .	*D'D* 9.59	*C'C* + *D'D* 16.85	. . . .	2 *D'DCC'* 163.7820
DE	N. 73° 30' W.	5.00	1.42	. . .	. . .	4.79	*D'E'* 1.42	. . .	. . . .	*DD'''* 4.80	*E'E* 4.79	*D'D* + *E'E* 14.38	2 *D'DEE'* 20.4196	. . . .
EF	S. 16° 30' W.	5.00	. . .	4.79	. . .	1.42	. . . .	*E'F'* 4.79	. . . .	*F''F* 1.42	*F'F* 3.37	*E'E* + *F'F* 8.16	. . . .	2 *F'FEE'* 39.0864
FA	N. 28° 30' W.	7.07	6.21	. . .	. . .	3.37	*F'A* 6.21	. . .	. . . .	*F'F* 3.37	0	*F'F* 3.37	2 *AFF'* 20.9277	. . . .
			18.14	18.14	9.59	9.58							81.4955	243.0888

EXAMPLE 2. Let it be required to survey the field *ABCDEF* (Fig. 23).

FIELD NOTES.

1	N. 73° 30′ W.	5.00
2	S. 16° 30′ W.	5.00
3	N. 28° 30′ W.	7.07
4	N. 20° 00′ E.	11.18
5	S. 43° 30′ E.	5.00
6	S. 13° 30′ E.	10.00

243.0888
81.4955
2 | 161.5933
10 | 80.7967
8.0797 acres.

EXPLANATION. The first station in the field notes is *D*, but we rearrange the numbers in the tablet so that *A* stands first. The northings and southings balance, but the eastings exceed the westings by 1 link. We apply the correction to the westing 4.79 (the distance *DE* being in doubt), making it 4.80, and rewrite all the latitudes and departures in the next four columns, incorporating the correction. In practice, the corrected numbers are written in red ink.

The remainder of the computation does not require explanation.

It will be seen that this method of computing areas is perfectly general.

§ 17. Supplying Omissions.

If, for any reason, the bearing and length of any side do not appear in the field notes, the latitude and departure of this side may be found in the following manner:

Find the latitudes and departures of the other sides as usual. The difference between the northings and southings will give the northing or southing of the unknown side, and the difference between the eastings and westings will give the easting or westing of the unknown side.

If the length and bearing of the unknown side are desired, they may be found by solving the right triangle, whose sides are the latitude and departure found by the method just explained, and whose hypotenuse is the length required.

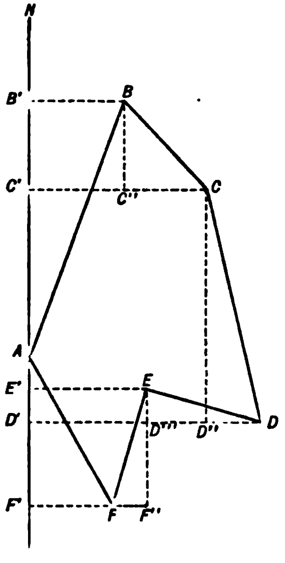


Fig. 23.

§ 18. Irregular Boundaries.

If a field have irregular boundaries, its area may be found by offsets, as explained in § 14, Prob. 3.

§ 19. Obstructions.

If the end of a line be not visible from its beginning, or if the line be inaccessible, its length and bearing may be found as follows:

1. By means of a random line (§ 4, 3).
2. When it is impossible to run a random line, which is frequently the case on account of the extent of the obstruction, the following method may be used:

Let AB (Fig. 24) represent an inaccessible line whose extremities A and B only are known, and B invisible from A.

Set flag-staffs at convenient points, C and D. Find the bearings and lengths of AC, CD, and DB, and then proceed to find the latitude and departure of AB, as in § 17.

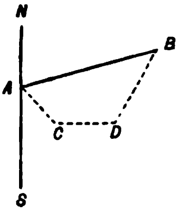


Fig. 24.

Example. Suppose that we have the following notes (see Fig. 24):

Side.	Bearing.	Dist.	N.	S.	E.	W.
AC	S. 45° E.	3.00		2.12	2.12	
CD	E.	3.50			3.50	
DB	N. 30° E.	4.83	4.18		2.42	
			4.18	2.12	8.04	0

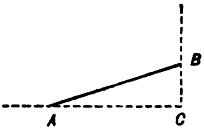


Fig. 25.

4.18
2.12
2.06

The northing of AB is 2.06, and the easting, 8.04; which numbers may be entered in the tablet in the columns N. and E., opposite the side AB.

If the bearing and length of AB are required, construct the right triangle ABC (Fig. 25), making $AC = 8.04$ and $BC = 2.06$.

$$\tan BAC = \frac{BC}{AC} = \frac{2.06}{8.04} = 0.256.$$

Hence, the angle $BAC = 14° 22'$.

Also, $$AB = \sqrt{\overline{AC}^2 + \overline{BC}^2} = \sqrt{8.04^2 + 2.06^2} = 8.29.$$

Therefore, the bearing and length of AB are N. 75° 38′ E. 8.29.

EXERCISE II.

NOTE. In examples 5 and 6 detours were made on account of inaccessible sides (§ 19, 2). The notes of the detours are written in braces.

1.

Sta.	*Bearings.*	*Dist.*
1	S. 75° E.	6.00
2	S. 15° E.	4.00
3	S. 75° W.	6.93
4	N. 45° E.	5.00
5	N. 45° W.	5.19½

2.

Sta.	*Bearings.*	*Dist.*
1	N. 45° E.	10.00
2	S. 75° E.	11.55
3	S. 15° W.	18.21
4	N. 45° W.	19.11

3.

Sta.	*Bearings.*	*Dist.*
1	N. 15° E.	3.00
2	N. 75° E.	6.00
3	S. 15° W.	6.00
4	N. 75° W.	5.20

4.

Sta.	*Bearings.*	*Dist.*
1	N. 89°45′ E.	4.94
2	S. 7°00′ W.	2.30
3	S. 28°00′ E.	1.52
4	S. 0°45′ E.	2.57
5	N. 84°45′ W.	5.11
6	N. 2°30′ W.	5.79

5.

Sta.	*Bearings.*	*Dist.*
1	S. 2°15′ E.	9.68
2	N. 51°45′ W.	2.39
	S. 85°00′ W.	6.47
	S. 55°10′ W.	1.62
3	N. 3°45′ E.	6.39
4	S. 66°45′ E.	1.70
5	N. 15°00′ E.	4.98
6	S. 82°45′ E.	6.03

6.

Sta.	*Bearings.*	*Dist.*
1	S. 81°20′ W.	4.28
	N. 76°30′ W.	2.67
2	N. 5°00′ E.	8.68
3	S. 87°30′ E.	5.54
4	S. 7°00′ E.	1.79
	S. 27°00′ E.	1.94
	S. 10°30′ E.	5.35
	N. 76°45′ W.	1.70

7.

Sta.	*Bearings.*	*Dist.*
1	N. 6°15′ W.	6.31
2	S. 81°50′ W.	4.06
3	S. 5°00′ E.	5.86
4	N. 88°30′ E.	4.12

8.

Sta.	*Bearings.*	*Dist.*
1	N. 5°30′ W.	6.08
2	S. 82°30′ W.	6.51
3	S. 3°00′ E.	5.33
4	E.	6.72

9.

Sta.	*Bearings.*	*Dist.*
1	N. 20°00′ E.	4.62¼
2	N. 73°00′ E.	4.16½
3	S. 45°15′ E.	6.18½
4	S. 38°30′ W.	8.00
5	Wanting.	Wanting.

10.

Sta.	*Bearings.*	*Dist.*
1	S. 3°00′ E.	4.23
2	S. 86°45′ W.	4.78
3	S. 37°00′ W.	2.00
4	N. 81°00′ W.	7.45
5	N. 61°00′ W.	2.17
6	N. 32°00′ E.	8.68
7	S. 75°50′ E.	6.38
8	S. 14°45′ W.	0.98
9	S. 79°15′ E.	4.52

§ 20. Modification of the Rectangular Method.

The area of a field may be found by a modification of the rectangular method, if its sides and interior angles are known.

Let A, B, C, D, represent the interior angles of the field $ABCD$ (Fig. 26). Let the side AB determine the direction of reference.

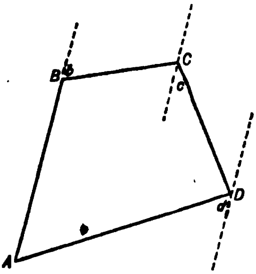


Fig. 26.

The bearing of AB, with reference to AB, is 0°.

The bearing of BC, with reference to AB, is the angle $b = 180° - B$.

The bearing of CD, with reference to AB, is the angle $c = C - b$.

The bearing of DA, with reference to AB, is the angle $d = A$.

The area may now be computed by the rectangular method, regarding AB as the magnetic meridian.

As the interior angles may be measured with considerable accuracy by the transit, the latitudes and departures should be obtained by using a table of natural sines and cosines.

Exercise III.

1. Find the area of the field $ABCD$, in which the angle $A = 120°$, $B = 60°$, $C = 150°$, and $D = 30°$; and the side $AB = 4$ chains, $BC = 4$ chains, $CD = 6.928$ chains, and $DA = 8$ chains.

2. Find the area of the farm $ABCDE$, in which the angle $A = 106° 19'$, $B = 99° 40'$, $C = 120° 20'$, $D = 86° 8'$, and $E = 127° 33'$; and the side $AB = 79.86$ rods, $BC = 121.13$ rods, $CD = 90$ rods, $DE = 100.65$ rods, and $EA = 100$ rods.

§ 21. General Remarks on Determining Areas.

Operations depending upon the reading of the magnetic needle must lack accuracy. Hence, when great accuracy is required (which is seldom the case in land surveying), the rectangular method (§§ 16–19) cannot be employed.

The best results are obtained by the methods explained in §§ 14 and 20, the horizontal angles being measured with the transit, and great care exercised in measuring the lines.

§ 22. THE VARIATION OF THE NEEDLE.

The **Magnetic Declination**, or variation of the needle, at any place, is the angle which the magnetic meridian makes with the true meridian, or north and south line. The variation is said to be east or west, according as the north end of the needle lies east or west of the true meridian. Western variation is indicated by the sign +, and eastern variation by the sign —.

Irregular Variations are sudden deflections of the needle, which occur without apparent cause. They are sometimes accompanied by auroral displays and thunder storms, and are most frequent in years of greatest sun-spot activity.

Solar-Diurnal Variation. North of the equator, the north end of the needle moves to the west, from 8 A.M. to 1.30 P.M., about 6′ in winter and 11′ in summer, and then returns gradually to its normal position.

Secular Variation is a change in the same direction for about a century and a half; then in the opposite direction for about the same time.

The line of no variation, or the **Agonic Line**, is a line joining those places at which the magnetic meridian coincides with the true meridian. In the United States, this line at present (1882) passes through Michigan, Ohio, the Virginias, and the Carolinas. It is moving gradually westward, so that the variation is increasing at places east of this line, and decreasing at places west of this line. East of this line the variation is westerly, and west of this line the variation is easterly.

The table on page 35, which has been prepared by permission from the report for 1879 of the United States Coast and Geodetic Survey, shows the magnetic variation at different places in the United States and Canada for several years; also, the annual change for 1880.

Place.	Latitude.	Longitude.	Variation.							Annual Change.
			1800	1820	1840	1860	1870	1880	1885	1880
	Deg. Min.	Deg. Min.	Degrees.	Degrees.	Degrees.	Degrees.	Degrees.	Degrees.	Degrees.	Minutes.
Portland, Me.	43 38.8	70 16.6	8.90	10.00	11.23	12.35	12.80	13.13	13.25	1.6
Portsmouth, N.H.	43 04.2	70 42.5	7.60	8.30	9.59	11.16	11.92	12.60	12.90	3.7
Boston, Mass.	42 21.5	71 03.8	6.98	7.88	9.11	10.43	11.03	11.56	11.78	2.9
Cambridge, Mass.	42 22.9	71 07.7	7.10	8.00	9.33	10.67	11.21	11.63	11.78	2.1
Quebec, Canada	46 48.4	71 14.5	12.15	12.23	13.70	15.95	16.82	17.31	17.40	1.6
Providence, R.I.	41 49.5	71 24.1	6.37	6.73	8.31	9.65	10.21	10.90	. . . .	. . . .
Hartford, Conn.	41 45.9	72 40.4	5.16	5.46	6.24	7.36	7.99	8.62	8.92	3.7
New Haven, Conn.	41 18.5	72 55.7	4.67	4.98	5.95	7.35	8.10	8.84	9.19	4.3
Burlington, Vt.	44 28.2	73 12.3	7.30	7.49	8.95	10.26	10.98	11.91	12.41	6.0
Albany, N.Y.	42 39.2	73 45.8	. . . .	5.81	7.00	8.49	9.23	9.90	10.19	3.7
New York, N.Y.	40 42.7	74 00.4	4.25	4.44	5.56	6.93	7.40	7.81	8.03	2.5
Philadelphia, Pa.	39 56.9	75 09.0	1.90	2.54	3.63	4.76	5.45	6.26	6.70	4.9
Baltimore, Md.	39 17.8	76 37.0	0.64	0.88	1.70	2.90	3.55	4.17	4.47	3.6
Harrisburg, Pa.	40 15.9	76 52.9	0.04	0.83	2.17	3.71	4.43	5.05	5.30	3.3
Washington, D.C.	38 53.3	77 00.6	0.00	0.40	1.29	2.45	3.04	3.61	3.87	3.2
Buffalo, N.Y.	42 52.8	78 53.5	0.03	0.22	1.16	2.64	3.48	4.32	4.73	5.0
Toronto, Can.	43 39.4	79 23.4	. . . .	. . . .	1.32	2.17	2.66	3.62	3.88	4.5
Charleston, S.C.	32 46.6	79 55.8	–4.70	–3.97	–2.84	–1.56	–0.95	–0.41	–0.17	3.0
Erie, Pa.	42 07.8	80 05.4	–0.33	–0.37	0.34	1.60	2.32	3.04	3.39	4.2
Savannah, Ga.	32 04.9	81 05.5	. . . .	–4.80	–4.14	–3.08	–2.48	–1.89	–1.60	3.5
Cleveland, O.	41 30.3	81 42.0	–1.90	–1.40	–0.61	0.38	0.87	1.31	1.51	2.5
Key West, Fla.	24 33.5	81 48.5	. . . .	–6.70	–6.06	–4.88	–4.18	–3.47	–3.12	4.2
Detroit, Mich.	42 20.0	83 03.0	–3.18	–2.90	–2.09	–0.99	–0.41	0.13	0.37	3.0
Mobile, Ala.	30 41.4	88 02.5	–5.80	–6.73	–7.09	–6.77	–6.38	–5.86	–5.56	3.4
New Orleans, La.	29 57.2	90 03.9	–7.52	–8.11	–8.10	–7.52	–7.05	–6.49	–6.18	3.5
St. Louis, Mo.	38 38.0	90 12.2	. . . .	–9.20	–8.40	–7.39	–6.83	–6.28	–6.00	3.2
Omaha, Neb.	41 15.7	95 56.5	. . . .	. . . .	. . . .	. . . .	. . . .	10.10	. . . .	2.6
San Diego, Cal.	32 42.1	117 14.3	–11.10	–11.60	–12.20	–12.88	–13.20	–13.50	–13.64	–1.7
San Francisco, Cal.	37 47.5	122 27.2	–13.30	–14.42	–15.40	–16.13	–16.37	–16.52	–16.56	–0.5

§ 23. To Establish a True Meridian.

This may be done as follows:

1. *By means of Burt's Solar Compass* (§ 25).
2. *By observations of Polaris.*

The North Star or Polaris revolves about the pole at present at the distance of about 1¼°; hence, it is on the meridian twice in 23 h. 56 m. (a siderial day), once above the pole called the upper culmination, and 11 h. 58 m. later below the pole called the lower culmination. It attains its greatest eastern or western elongation, or greatest distance from the meridian, 5 h. 59 m. after the culmination.

The following table gives the time of the upper culmination of Polaris for 1882. The time is growing later at the rate of about one minute in three years.

Month.	First Day.	Eleventh Day.	Twenty-first Day.
	H. M.	H. M.	H. M.
January . .	6 32 P.M.	5 53 P.M.	5 13 P.M.
February .	4 30 P.M.	3 50 P.M.	3 11 P.M.
March . . .	2 35 P.M.	1 56 P.M.	1 17 P.M.
April. . . .	12 29 P.M.	11 50 A.M.	11 11 A.M.
May	10 31 A.M.	9 52 A.M.	9 13 A.M.
June	8 30 A.M.	7 51 A.M.	7 12 A.M.
July	6 32 A.M.	5 53 A.M.	5 14 A.M.
August. . .	4 31 A.M.	3 52 A.M.	3 13 A.M.
September .	2 29 A.M.	1 50 A.M.	1 11 A.M.
October . .	12 32 A.M.	11 52 P.M.	11 13 P.M.
November .	10 30 P.M.	9 50 P.M.	9 11 P.M.
December .	8 32 P.M.	7 52 P.M.	7 13 P.M.

The time of the upper culmination of Polaris may be found by means of the star Alioth, which is the star in the handle of the Dipper (in the constellation of the Great Bear) next to the four which form the bowl. It crosses the meridian about the same time as Polaris. Suspend from a height of about 20 feet a plumb-line, placing the bob in a pail of water to lessen its vibrations. About 15 feet south of the plumb-line, upon a horizontal board firmly supported at a convenient height, place a compass sight fastened to a board a few inches square. At night, when Alioth by estimation approaches the meridian, place the compass sight in line with Polaris and the plumb-line, and move it so as to keep it in this line until the plumb-line also falls on Alioth (Fig 27). Note the time; then twenty-two minutes later Polaris will be on the meridian.

If the lower culmination takes place at night, the time may be found in a similar manner.

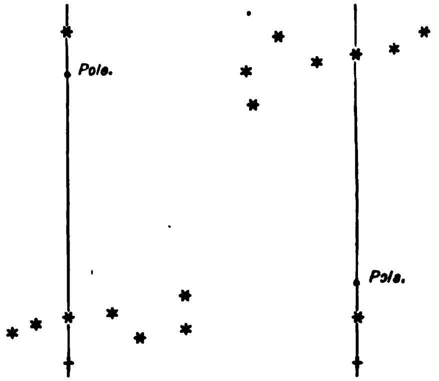


Fig. 27.

Instead of the compass sight, any upright with a small opening or slit may be used.

The plumb-line may be made visible by a light held near it.

(*a*) **To locate the true meridian by the position of Polaris at its culmination.**

1. *By using the apparatus described in finding the time of culmination.* At the time of culmination bring Polaris, the plumb-line, and the compass sight into line. The compass sight and the plumb-bob will give two points in the true meridian.

2. *By means of the transit.* Bring the telescope to bear on Polaris at the time of culmination, holding a light near to make the wires visible, if the observation is made at night. The telescope will then lie in the plane of the meridian, which may be marked by bringing the telescope to a horizontal position.

(*b*) **To locate the meridian by the position of Polaris at greatest elongation.**

The **Azimuth** of a star is the angle which the meridian plane makes with a vertical plane passing through the star and the zenith of observer.

Let Z (Fig. 28) represent the zenith of the place, P the pole, and N Polaris at its greatest elongation. Let ZP, ZN, and PN be arcs of great circles, and let N be a right angle.

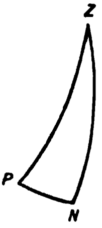


Fig. 28.

$$\sin PN = \cos(90° - ZP)\cos(90° - Z).$$

[Spher. Trig. § 47.]

But $ZP =$ the complement of the latitude.

Hence, $90° - ZP =$ the latitude of the place.

Hence, $\sin PN = \cos \text{latitude} \times \sin Z$.

Hence, $$\sin Z = \frac{\sin PN}{\cos \text{latitude}}.$$

Hence, Z (the azimuth of Polaris) can be found if the latitude of the place and the greatest elongation of Polaris (PN) are known.

The following table gives the latter element Jan. 1, 1882–93.

GREATEST ELONGATION OF POLARIS.

1882	1° 19′ 12.5″	1886	1° 17′ 56.6″	1890	1° 16′ 40.7″
1883	1° 18′ 53.5″	1887	1° 17′ 37.6″	1891	1° 16′ 21.8″
1884	1° 18′ 34.5″	1888	1° 17′ 18.6″	1892	1° 16′ 3″
1885	1° 18′ 15.5″	1889	1° 16′ 59.7″	1893	1° 15′ 44.1″

The greatest elongation of Polaris, or the polar distance, is given in the Nautical Almanac. The table gives this element for Jan. 1. It may be found for other dates by interpolation.

To obtain a line in the direction of Polaris at greatest elongation.

1. *By using the apparatus for finding the time of culmination.* A few minutes before the time of greatest elongation (5 h. 59 m. after culmination), place the compass sight in line with the plumb-line and Polaris, and keep it in line with these until the star begins to recede. At this moment the sight and plumb-line are in the required line.

2. *By means of the transit.* A few minutes before the time of greatest elongation, bring the telescope to bear on the star, and follow it, keeping the vertical wire over the star until it begins to recede. The telescope will then be in the required line.

To establish the meridian. Having the transit sighted in the direction of the line just found, turn it through an angle equal to the azimuth in the proper direction.

§ 24. Dividing Land.

A few problems in the Division of Land are solved in this section, for the purpose of acquainting the student with some of the methods employed. The surveyor must, for the most part, depend on his general knowledge of Geometry and Trigonometry, and his own ingenuity, for solutions of the problems that arise in practice.

Problem 1. **To divide a triangular field into two parts having a given ratio, by a line through a given vertex.**

Let ABC (Fig. 29) be the triangle, and A the given vertex.

Divide BC at D, so that $\frac{BD}{DC}$ equals the given ratio, and join A and D. ABD and ADC will be the parts required; for

$$ABD : ADC :: BD : DC.$$

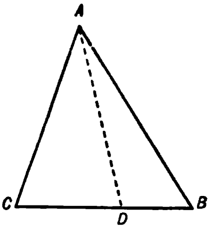


Fig. 29.

Problem 2. **To cut off from a triangular field a given area, by a line parallel to the base.**

Let ABC (Fig. 30) be the triangle, and let DE be the division line required.

$$\sqrt{ABC} : \sqrt{ADE} :: AB : AD.$$

$$\therefore AD = AB\sqrt{\frac{ADE}{ABC}}$$

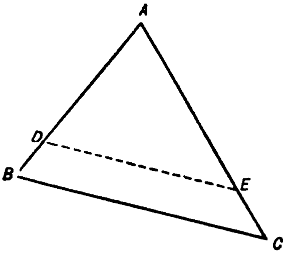


Fig. 30.

Problem 3. To divide any field into two parts having a given ratio, by a line through a given point in the perimeter.

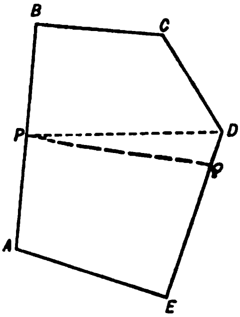


Fig. 31.

Let *ABCDE* (Fig. 31) represent the field, *P* the given point, and *PQ* the required division line.

The areas of the whole field and of the required parts having been determined, run the line *PD* from *P* to a corner *D*, dividing the field, as near as possible, as required. Determine the area *PBCD*.

The triangle *PDQ* represents the part which must be added to *PBCD* to make the required division.

$$\text{Area } PDQ = \tfrac{1}{2} \times PD \times DQ \times \sin PDQ.$$

$$\text{Hence, } DQ = \frac{2 \text{ area } PDQ}{PD \times \sin PDQ}.$$

Note. $DQ = \dfrac{2 \text{ area } PDQ}{\text{perpendicular from } P \text{ on } DE}$. This perpendicular from *P* on *DE* may be run and measured directly.

Problem 4. To divide a field into a given number of parts, so that access to a pond of water is given to each.

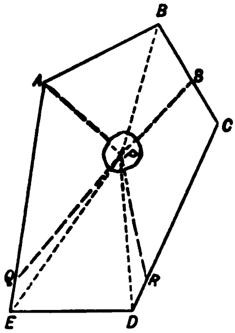


Fig. 32.

Let *ABCDE* (Fig. 32) represent the field, and *P* the pond. Let it be required to divide the field into four parts. Find the area of the field and of each part.

Let *AP* be one division line. Run *PE*, and find the area *APE*. Take the difference between *APE* and the area of one of the required parts; this will give the area of the triangle *PQE*, from which *QE* may be found, as in Problem 3. Join *P* and *Q*; *PAQ* will be one of the required parts. In like manner, *PQR* and *PAS* are determined; whence, *PSR* must be the fourth part required.

EXERCISE IV.

1. From the square *ABCD*, containing 6 A. 1 R. 24 P., part off 3 A. by a line *EF* parallel to *AB*.

2. From the rectangle *ABCD*, containing 8 A. 1 R. 24 P., part off 2 A. 1 R. 32 P. by a line *EF* parallel to $AD = 7$ ch. Then, from the remainder of the rectangle, part off 2 A. 3 R. 25 P., by a line *GH* parallel to *EB*.

3. Part off 6 A. 3 R. 12 P. from a rectangle *ABCD*, containing 15 A., by a line *EF* parallel to *AB*; *AD* being 10 ch.

4. From a square *ABCD*, whose side is 9 ch., part off a triangle which shall contain 2 A. 1 R. 36 P., by a line *BE* drawn from *B* to the side *AD*.

5. From *ABCD*, representing a rectangle, whose length is 12.65 ch., and breadth 7.58 ch., part off a trapezoid which shall contain 7 A. 3 R. 24 P., by a line *BE* drawn from *B* to the side *DC*.

6. In the triangle *ABC*, $AB = 12$ ch., $AC = 10$ ch., and $BC = 8$ ch.; part off 1 A. 2 R. 16 P., by the line *DE* parallel to *AB*.

7. In the triangle *ABC*, $AB = 26$ ch., $AC = 20$ ch., and $BC = 16$ ch.; part off 6 A. 1 R. 24 P., by the line *DE* parallel to *AB*.

8. It is required to divide the triangular field *ABC* among three persons whose claims are as the numbers 2, 3, and 5, so that they may all have the use of a watering-place at *C*; $AB = 10$ ch., $AC = 6.85$ ch., and $CB = 6.10$ ch.

9. Divide the five-sided field *ABCHE* among three persons, X, Y, and Z, in proportion to their claims, X paying $500, Y paying $750, and Z paying $1000, so that each may have the use of an interior pond at *P*, the quality of the land being equal throughout. Given $AB = 8.64$ ch., $BC = 8.27$ ch., $CH = 8.06$ ch., $HE = 6.82$ ch., and $EA = 9.90$ ch. The perpendicular *PD* upon $AB = 5.60$ ch., PD' upon $BC = 6.08$ ch., PD'' upon $CH = 4.80$ ch., PD''' upon $HE = 5.44$ ch., and PD'''' upon $EA = 5.40$ ch. Assume *PH* as the divisional

fence between X 's and Z 's shares; it is required to determine the position of the fences *PM* and *PN* between X 's and Y 's shares and Y 's and Z 's shares, respectively.

10. Divide the triangular field *ABC*, whose sides *AB*, *AC*, and *BC* are 15, 12, and 10 ch., respectively, into three equal parts, by fences *EG* and *DF* parallel to *BC*.

11. Divide the triangular field *ABC*, whose sides *AB*, *BC*, and *AC* are 22, 17, and 15 ch., respectively, among three persons, A, B, and C, by fences parallel to the base *AB*, so that A may have 3 A., B, 4 A., and C, the remainder.

25. UNITED STATES PUBLIC LANDS.

Burt's Solar Compass.

This instrument, which is exhibited on the following page, may be used for most of the purposes of a compass or transit. Its most important use, however, is to run north and south lines in laying out the public lands.

A full description of the solar compass, with its principles, adjustments, and uses, forms the subject of a considerable volume, which should be in the hands of the surveyor who uses this instrument. The limits of our space will allow only a brief reference to its principal features.

The main plate and standards resemble these parts of the compass.

a is the *latitude arc.*

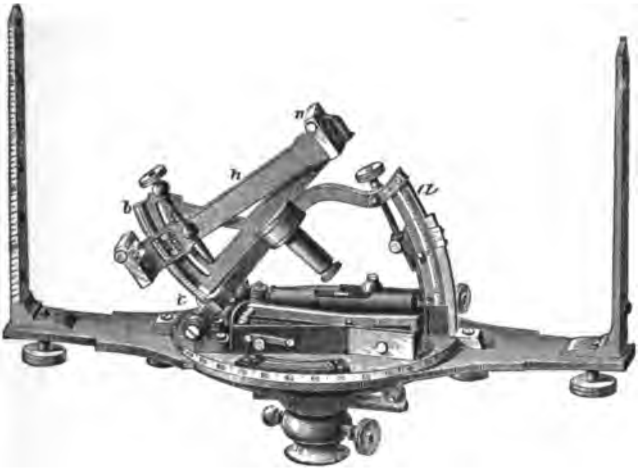
b is the *declination arc.*

h is an arm, on each end of which is a *solar lens* having its focus on a silvered plate on the other end.

c is the *hour arc.*

n is the *needle-box*, which has an arc of about 36°.

To run a north and south line with the solar compass. Set off the declination of the sun on the declination arc. Set off the latitude of the place (which may be determined by this instrument) on the latitude arc. Set the instrument over the station,



BURT'S SOLAR COMPASS.

level, and turn the sights in a north and south direction, approximately, by the needle. Turn the solar lens toward the sun, and bring the sun's image between the equatorial lines on the silvered plate. Allowance being made for refraction, the sights will then indicate a true north and south line.

The Solar Attachment for Transits.

This consists, essentially, of the solar apparatus of the solar compass attached to the telescope of the ordinary transit.

Laying Out the Public Lands.

The public lands north of the Ohio River and west of the Mississippi are generally laid out in townships approximately six miles square.

A **Principal Meridian**, or true north and south line, is first run by means of Burt's Solar Compass, and then an east and west line, called a **Base Line**.

Parallels to the base line are run at intervals of six miles, and north and south lines at the same intervals. Thus, the tract would be divided into townships exactly six miles square, if it were not for the convergence of the meridians on account of the curvature of the earth.

The north and south lines, or meridians, are called **Range Lines**. The east and west lines, or parallels, are called **Township Lines**.

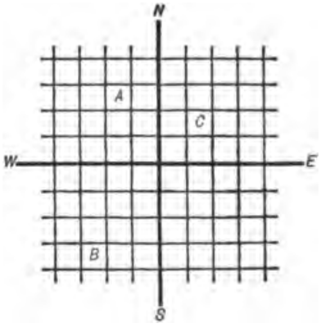


Fig. 33.

Let *NS* (Fig. 33) represent a principal meridian, and *WE* a base line; and let the other lines represent meridians and parallels at intervals of six miles.

The small squares, *A*, *B*, *C*, etc., will represent townships.

A would be designated thus: T. 3 N., R. 2 W.; that is, township three north, range two west; which means that the township is in the third tier north of the base line, and in the second tier west of the principal meridian. *B* and *C*, respectively, would be designated thus: T. 4 S., R. 3 W.; and T. 2 N., R. 2 E.

The townships are divided into sections approximately one mile square, and the sections are divided into quarter-sections. The township, section, and quarter-section corners are permanently marked.

6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

Fig. 34.

The sections are numbered, beginning at the north-east corner, as in Fig. 34, which represents a township divided into sections. The quarter-sections are designated, according to their position, as N.E., N.W., S.E., and S.W.

Every fifth parallel is called a **Standard Parallel** or **Correction Line.**

Let *NS* (Fig. 35) represent a principal meridian; *WE* a base line; *rp*, etc., meridians; and *ms* the fifth parallel. If *Op* equals six miles, *mr* will be less than six miles on account of the convergence of the meridians. Surveyors are instructed to make *Op* such a distance that *mr* shall be six miles; then *mh*, *hk*, etc., are taken similarly. At the correction lines north of *ms* the same operation is repeated.

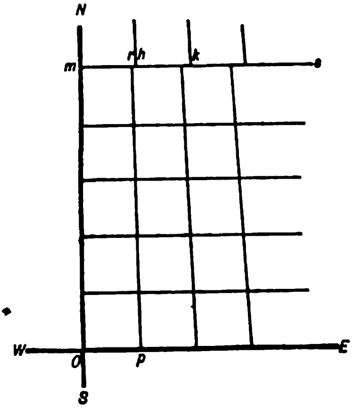


Fig. 35.

The township and section lines are surveyed in such an order as to throw the errors on the north and outer townships and sections.

If, in running a line, a navigable stream or a lake more than one mile in length is encountered, it is *meandered* by marking the intersection of the line with the bank and running lines from this point along the bank to prominent points which are marked, and the lengths and bearings of the connecting lines recorded.

Six principal meridians have been established and connected. In addition to these there are several independent meridians in the Western States and Territories which will in time be connected with each other and with the eastern system.

§ 26. PLANE-TABLE SURVEYING.*

After the principal lines of a survey have been determined and plotted, the details of the plot may be filled in by means of the plane-table; or, when a plot only of a tract of land is desired, this instrument affords the most expeditious means of obtaining it.

An approved form of the plane-table, as used in the United States Coast and Geodetic Survey, is shown in the plate on page 49.

The **Table-top** is a board of well-seasoned wood, panelled with the grain at right angles to prevent warping, and supported at a convenient height by a **Tripod** and **Levelling Head.**

The **Alidade** is a ruler of brass or steel supporting a telescope or sight standards, whose line of sight is parallel to a plane perpendicular to the lower side of the ruler, and embracing its fiducial edge.

The **Declinatoire** consists of a detached rectangular box containing a magnetic needle which moves over an arc of about 10° on each side of the 0.

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* In preparing this section the writer has consulted, by permission, the treatise on the plane-table by Mr. E. Hergesheimer, contained in the report for 1880 of the U.S. Coast and Geodetic Survey.

Two spirit levels at right angles are attached to the ruler or to the declinatoire. In some instruments these are replaced by a circular level, or by a detached spirit level.

The paper upon which the plot is to be made or completed is fastened evenly to the board by clamps, the surplus paper being loosely rolled under the sides of the board.

To place the table in position. This operation, which is sometimes called orienting the table, consists in placing the table so that the lines of the plot shall be parallel to the corresponding lines on the ground.

This may be accomplished by turning the table until the needle of the declinatoire indicates the same bearing as at a previous station, the edge of the declinatoire coinciding with the same line on the paper at both stations.

If, however, the line connecting the station at which the instrument is placed with another determined station is already plotted, the table may be placed in position by placing it over the station so that the plotted line is by estimation over and in the direction of the line on the ground; then making the edge of the ruler coincide with the plotted line, and turning the board until the line of sight bisects the signal at the other end of the line on the ground.

To plot any point. Let ab on the paper represent the line AB on the ground; it is required to plot c, representing C on the ground.

1. *By intersection.*

Place the table in position at A (Fig. 36), plumbing a over A, and making the fiducial edge of the ruler pass through a; turn the alidade about a until the line of sight bisects the signal at C, and draw a line along the fiducial edge of the ruler. Place the table in position at B, plumbing b over B, and repeat the operation just described. c will be the intersection of the two lines thus drawn.

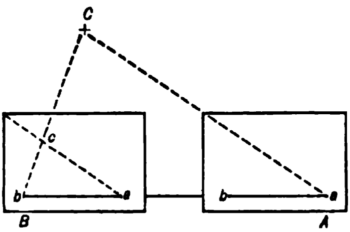
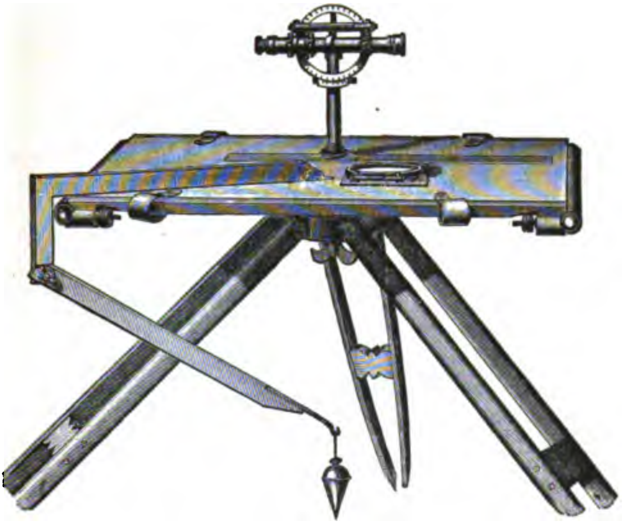


Fig. 36.



THE PLANE-TABLE.

2. *By resection.*

Place the table in position at *A* (Fig. 37), and draw a line in the direction of *C*, as in the former case; then remove the instrument to *C*, place it in position by the line drawn from *a*, make the edge of the ruler pass through *b*, and turn the alidade about *b* until *B* is in the line of sight. A line drawn along the edge of the ruler will intersect the line from *a* in *c*.

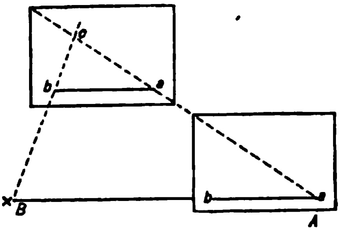


Fig. 37.

3. *By radiation.*

Place the table in position at *A* (Fig. 38), and draw a line from *a* toward *C*, as in the former cases. Measure *AC*, and lay off *ac* to the same scale as *ab*.

To plot a field *ABCD*.....

1. *By radiation.*

Set up the table at any point *P*, and mark *p* on the paper over *P*. Draw indefinite lines from *p* toward *A*, *B*, *C*, ... Measure *PA*, *PB*, ..., and lay off *pa*, *pb*, ..., to a suitable scale, and join *a* and *b*, *b* and *c*, *c* and *d*, etc.

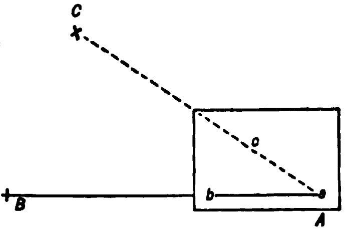


Fig. 38.

2. *By progression.*

Set up the table at *A*, and draw a line from *a* toward *B*. Measure *AB*, and plot *ab* to a suitable scale. Set up the table in position at *B*, and in like manner determine and plot *bc*, etc.

3. *By intersection.*

Plot one side as a base line. Plot the other corners by the method of intersection, and join.

4. *By resection.*

Plot one side as a base line. Plot the other corners by the method of resection, and join.

The Three Point Problem.

Let *A*, *B*, *C* represent three points determined and plotted as *a*, *b*, *c* (Fig. 39); it is required to plot by the plane-table, *d* representing a fourth undetermined point *D*.

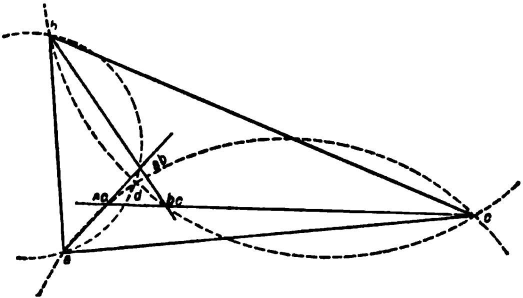


Fig. 39.

Determine the point *d* by the method of resection; first, from *A* and *B*, then from *A* and *C*. If the three lines from *a*, *b*, and *c* meet in a point, this will determine *d*. Ordinarily, they will not meet in a point, but will form a *triangle of error*, *ac bc ab*. Through *a*, *b*, and *ab*; *a*, *c*, and *ac*; and *b*, *c*, and *bc*, respectively, pass circumferences of circles; these three circles will intersect in the required point *d*.

CHAPTER III.

TRIANGULATION.*

§ 27. INTRODUCTORY REMARKS.

Geographical positions upon the surface of the earth are commonly determined by systems of triangles which connect a carefully determined base line with the points to be located.

Let *F* (Fig. 40) represent a point whose position with reference to the base line *AB* is required. Connect *AB* with *F* by the series of triangles *ABC*, *ACD*, *ADE*, and *DEF*, so that a signal at *C* is visible from *A* and *B*, a signal at *D* visible from *A* and *C*, a signal at *E* visible from *A* and *D*, and a signal at *F* visible from *D* and *E*. In the triangle *ABC*, the side *AB* is known, and the angles at *A* and *B* may be measured; hence, *AC* may be computed. In the triangle *ACD*, *AC* is known, and the angles at *A* and *C* may be measured; hence, *AD* may be computed. In like manner *DE* and *EF* or *DF* may be determined. *DF*, or some suitable line connected with *DF*, may be measured, and this result compared with the computed value to test the accuracy of the field measurements.

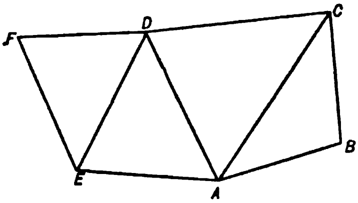


Fig. 40.

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* In preparing this chapter the writer has consulted, by permission, recent reports of the United States Coast and Geodetic Survey.

Three orders of triangulation are recognized; viz.:

Primary, in which the sides are from 20 to 150 miles in length.

Secondary, in which the sides are from 5 to 40 miles in length, and which connect the primary with the tertiary.

Tertiary, in which the sides are seldom over 5 miles in length, and which bring the survey down to such dimensions as to admit of the minor details being filled in by the compass and plane-table.

§ 28. THE MEASUREMENT OF BASE LINES.

Base lines should be measured with a degree of accuracy corresponding to their importance.

Suitable ground must be selected and cleared of all obstructions. Each extremity of the line may be marked by cross lines on the head of a copper tack driven into a stub which is sunk to the surface of the ground. Poles are set up in line about half a mile apart, the alignment being controlled by a transit placed over one end of the line.

The *preliminary measurement* may be made with an iron wire about one-eighth of an inch in diameter and 60^m in length. In measuring, the wire is brought into line by means of a transit set up in line not more than one-fourth of a mile in the rear. The end of each 60^m is marked with pencil lines on a wooden bench whose legs are thrust into the ground after its position has been approximately determined. If the last measurement exceeds or falls short of the extremity of the line, the difference may be measured with the 20^m chain.

The *final measurement* is made with the *base apparatus*, which consists of bars 6^m long, which are supported upon trestles when in use. These bars are placed end to end, and brought to a horizontal position, if this can be quickly accomplished; if not, the angle of inclination is taken by a sector, or a vertical offset is measured with the aid of a transit, so that the exact horizontal distance can be computed.

A thermometer is attached to each bar, so that the temperature of the bar may be noted and a correction for temperature applied.

The method of measuring lines varies according to the required degree of accuracy in any particular case, but the brief description given above will give the student a general idea of the methods employed.

§ 29. THE MEASUREMENT OF ANGLES.

Angles are measured by large theodolites, and the reading taken by microscopes to single seconds.

In order to eliminate errors of observation, and errors arising from imperfect graduation of the circles, a large number of readings is made and their mean taken. Two methods are in use; viz., repetition and series.

The method of *repetition* consists, essentially, in measuring the angles about a point singly, then taking two adjacent angles as a single angle, then three, etc.; thus "closing the horizon," or measuring the whole angular magnitude about a point in several different ways.

The method of *series* consists, essentially, in taking the readings of an angle with the circle or limb of the theodolite in one position, then turning the circle through an arc and taking the readings of the same angle again, etc.; thus reading the angle from successive portions of the graduated circle.

On account of the curvature of the earth, the sum of the three angles of a triangle upon its surface exceeds 180°. This *spherical excess*, as it is called, becomes appreciable only when the sides of the triangle are about 5 miles in length. To determine the angles of the rectilinear triangle having the same vertices, one-third of the spherical excess is deducted from each spherical angle.

CHAPTER IV.

LEVELLING.

§ 30. DEFINITIONS, CURVATURE, AND REFRACTION.

A **Level Surface** is a surface parallel with the surface of still water.

A **Level Line** is a line in a level surface.

Levelling is the process of finding the difference of level of two places, or the distance of one place above or below a level line through another place.

The **Line of Apparent Level** of a place is a tangent to the level line at that place. Hence, the line of apparent level is perpendicular to the plumb-line.

The **Correction for Curvature** is the deviation of the line of apparent level from the level line for any distance.

Let t (Fig. 41) represent the line of apparent level of the place P, a the level line, d the diameter of the earth; then c represents the correction for curvature. To compute the correction for curvature:

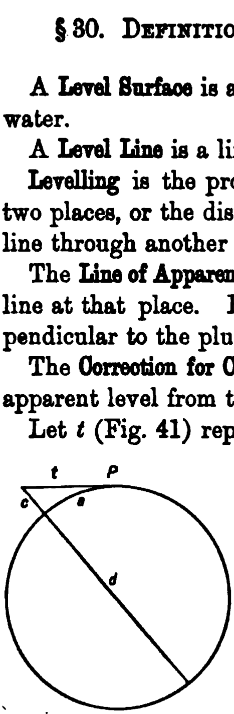


Fig. 41.

$$t^2 = c(c+d).$$

Therefore, $c = \dfrac{t^2}{c+d} = \dfrac{a^2}{d}$

approximately, since c is very small compared with d, and $t = a$ without appreciable error.

Since d is constant (= 7920 miles, nearly), the correction for curvature varies as the square of the distance.

Example. What is the correction for curvature for 1 mile?

By substituting in the formula deduced above, $c = \frac{a^2}{d} = \frac{1^2}{7920}$ mi. = 8 in., nearly.

Hence, the correction for curvature for any distance may be found in inches, approximately, by multiplying 8 by the square of the distance expressed in miles.

A correction for the refraction of the rays of light is sometimes made by decreasing the correction for curvature by one-sixth of itself.

§ 31. The Y Level.

This instrument is shown on page 59.

The *telescope* is about 20 inches in length, and rests on supports called *Y's*, from their shape. The *spirit level* is underneath the telescope, and attached to it. The *levelling-head* and *tripod* are similar to the same parts of the transit.

§ 32. The Levelling Rod.

The rod shown in Fig. 42 is known as the New York levelling rod. It is made of two pieces of wood, sliding upon each other, and held together in any position by a clamp. The front surface of the rod is graduated to hundredths of a foot up to 6½ feet.

The target slides along the front of the rod, and is held in place by two springs which press upon the sides of the rod. It has a square opening at the centre, through which the division line of the rod opposite to the horizontal line of the target may be seen. It carries a vernier by which heights may be read to thousandths of a foot (§ 7).

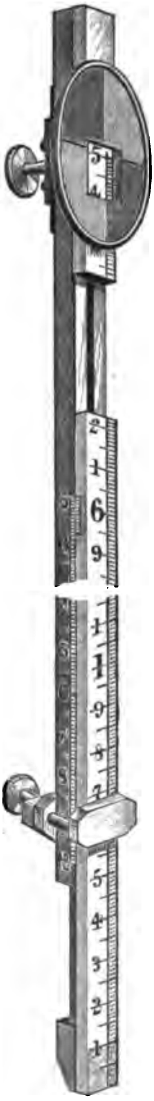


Fig. 42.

If a greater height than 6½ feet is desired, the target is made fast with its horizontal line at 6½ feet from the lower end. The back part of the rod is then moved up until the target is at the required height, and the reading is taken at the side of the rod. When fully extended the rod is 12 feet long.

§ 33. DIFFERENCE OF LEVEL.

To find the difference of level between two places visible from an intermediate place.

Let A and B (Fig. 43) represent the two places. Set the Y level at a station equally distant, or nearly so, from A and B, but not necessarily on the line AB. Place the legs of the tripod firmly in the ground, and level over each opposite pair of levelling screws, successively. Let the rodman hold the levelling rod vertically at A. Bring the telescope to bear upon the rod (§ 8), and by signal direct the rodman to move the target until its horizontal line is in the line of apparent level of the telescope. Let the rodman now record the height AA' of the target. In like manner find BB'. The difference between AA' and BB' will be the difference of level required. If the instrument be equally distant from A and B, or nearly so, no correction for curvature will be necessary.

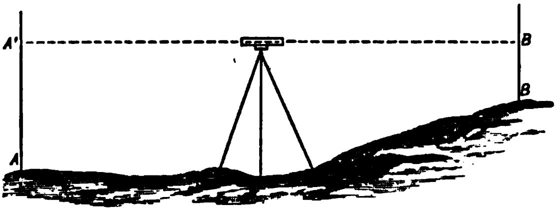
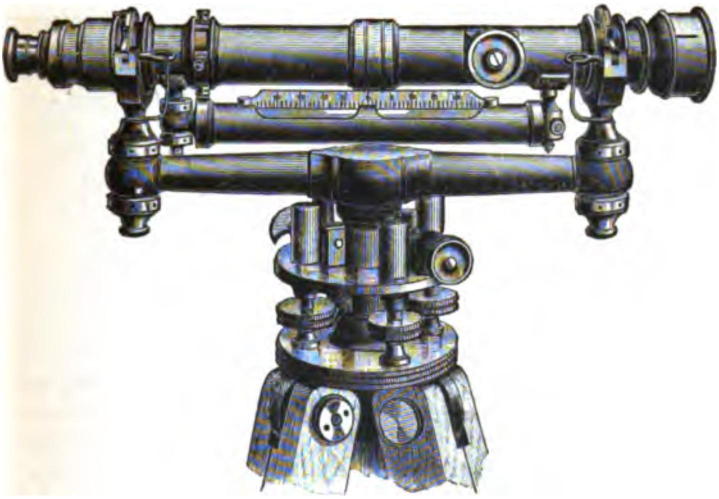


Fig. 43.

If the instrument be set up at one station, and the rod at the other, the difference between the heights of the optical axis of the telescope and the target, corrected for curvature and refraction, will be the difference of level required.



THE Y LEVEL.

To find the difference of level of two places, one of which cannot be seen from the other, and both invisible from the same place; or, when the two places differ considerably in level.

Let *A* and *D* (Fig. 44) represent the two places. Place the level midway between *A* and some intermediate station *B*.

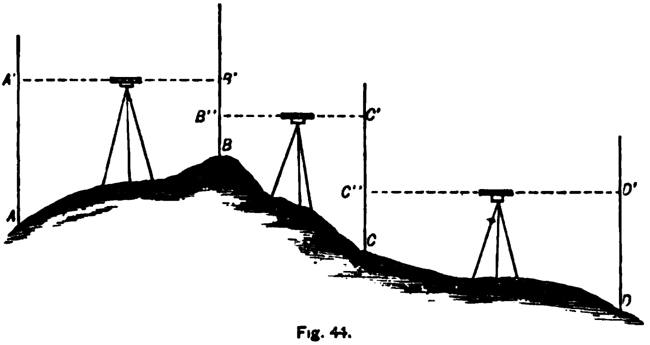


Fig. 44.

Find *AA'* and *BB'*, as in the preceding case, and record the former as a *back-sight* and the latter as a *fore-sight*. Select another intermediate station *C*, and in like manner find the back-sight *BB''* and the fore-sight *CC'*; and so continue until the place *D* is reached. The difference between the sum of the fore-sights and the sum of the back-sights will be the difference of level required.

§ 34. Levelling for Section.

The intersection of a vertical plane with the surface of the earth is called a **Section** or **Profile**. The term profile, however, usually designates the **Plot** or representation of the section on paper.

Levelling for Section is levelling to obtain the data necessary for making a profile or plot of any required section.

A profile is made for the purpose of exhibiting in a single view the inequalities of the surface of the ground for great distances along the line of some proposed improvement, such as a railroad, canal or ditch, and thus facilitating the establishment of the proper grades.

The data necessary for making a profile of any required section are, the heights of its different points above some assumed horizontal plane, called the **Datum Plane,** together with their horizontal distances apart or from the beginning of the section.

The position of the datum plane is fixed with reference to some permanent object near the beginning of the section, called a **Bench Mark,** and, in order to avoid negative heights, is assumed at such a distance below this mark that all the points of the section shall be above it.

The heights of the different points of the section above the datum plane are determined by means of the level and levelling-rod; and the horizontal length of the section is measured with an engineer's chain or tape, and divided into equal parts, one hundred feet in length, called **Stations,** marked by stakes numbered 0, 1, 2, 3, etc.

Where the ground is very irregular, it may be necessary, besides taking sights at the regular stakes, to take occasional sights at points between them. If, for instance, at a point sixty feet in advance of stake 8 there is a sudden rise or fall in the surface, the height of this point would be determined and recorded as at stake 8.60.

The readings of the rod are ordinarily taken to the nearest tenth of a foot, except on *bench marks* and points called *turning points*, where they are taken to thousandths of a foot.

A Turning Point is a point on which the last sight is taken just before changing the position of the level, and the first sight from the new position of the instrument. A turning point may be coincident with one of the stakes, but must always be a hard point, so that the foot of the rod may stand at the same level for both readings.

To explain the method of obtaining the field notes necessary for making a profile, let 0, 1, 2, 3 ..... 11 (Fig. 45) represent a portion of a section to be levelled and plotted. Establish a bench mark at or near the beginning of the line, measure the horizontal length of the section, and set stakes one hundred feet apart, numbering them 0, 1, 2, 3, etc. Place the level at some point, as between 2 and 3, and take the reading of the rod on the bench $= 4.832$. Let PP' represent the datum plane, say 15 feet below the bench mark, then

$$15 + 4.832 = 19.832$$

will be the height of the line of sight AB, called the **Height of the Instrument**, above the datum plane. Now take the reading at $0 = 5.2 = 0A$, and subtract the same from 19.832, which leaves $14.6 = 0P$, the height of the point 0 above the datum plane. Next take sights at 1, 2, 3, 3.40, and 4 equal respectively to 3.7, 3.0, 5.1, 4.8, and 8.3, and subtract the same from 19.832; the remainders 16.1, 16.8, 14.7, 15.0, and 11.5 will be the respective heights of the points 1, 2, 3, 3.40, and 4. Then, as it will be necessary to change the position of the instrument, select a point in the neighborhood of 4 suitable as a turning point (*t.p.* in the figure), and take a careful reading on $it = 8.480$; subtract this from 19.832, and the remainder, 11.352, will be the height of the turning point. Now carry the instrument forward to a new position, as between 5 and 6, shown in the figure, while the rodman remains at *t.p.*; take a second reading

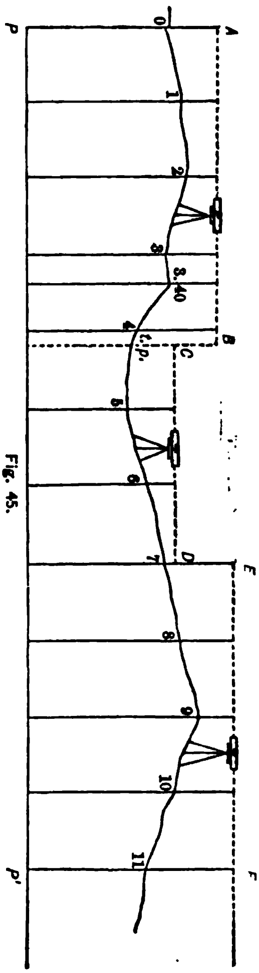


Fig. 45.

on *t.p.* = 4.102, and add it to 11.352, the height of *t.p.* above PP'; the sum 15.454 will be the height of the instrument CD in its new position. Now take sight upon 5, 6, and 7, equal respectively to 4.9, 2.8, and 0.904; subtract these sights from 15.454, and the results 10.6, 12.7, and 14.550 will be the heights of the points 5, 6, and 7 respectively. The point 7, being suitable, is made a turning point, and the instrument is moved forward to a point between 9 and 10. The sight at 7 = 6.870 added to the height of 7 gives 21.420 as the height of the instrument EF in its new position. The readings at 8, 9, 10, and 11, which are respectively 5.4, 3.6, 5.8, and 9.0, subtracted from 21.420, will give the heights of these points, namely, 16.0, 17.8, 15.6, and 12.4.

Proceed in like manner until the entire section is levelled, establishing bench marks at intervals along the line to serve as reference points for future operations. A record of the work described above is kept in a field book as follows:

Station.	+ *S.*	*H.I.*	− *S.*	*H.S.*	*Remarks.*
B	4.832			15.	Bench on rock 20 ft. south of 0.
0		19.832	5.2	14.6	
1			3.7	16.1	
2			3.0	16.8	
3			5.1	14.7	3 to 3.40 turnpike road.
3.40			4.8	15.0	
4			8.3	11.5	
t.p.	4.102		8.480	11.352	
5		15.454	4.9	10.6	
6			28.	12.7	
7	6.870		0.904	14.550	
8		21.420	5.4	16.0	
9			3.6	17.8	
10			5.8	15.6	
11			9.0	12.4	
B					Bench on oak stump 27 ft. N.E. of 12,
12					
etc.					etc.

The first column contains the numbers or names of all the points on which sights are taken. The second column contains the sight taken on the first bench mark, and the sight on each turning point taken immediately after the instrument has been moved to a new position. These are called **Plus Sights** (+*S.*) because they are **added** to the heights of the points on which they are taken to obtain the height of the instrument given in the third column (*H.I.*). The fourth column contains all the readings except those recorded in the second column. These are called **Minus Sights** (– *S.*) because they are **subtracted** from the numbers in the third column to obtain all the numbers in the fifth column except the first, which is the assumed depth of the datum plane below the bench. The fifth column contains the required heights of all the points of the section named in the first column together with the heights of all benches and turning points.

To find the difference of level between any two points of the section, we have only to take the difference between the numbers in the fifth column opposite these points.

The real field notes are contained in the first, second, fourth, and last columns; the other columns may be filled after the field operations are completed. The field book may contain other columns; one for **height of grade** (*H.G.*), another for **depth of cut** (*C.*), and another for **height of embankment** or **fill** (*F.*).

To plot the section. Draw a line *PP'* (Fig. 45), to represent the datum plane, and beginning at some point as *P*, lay off the distances 100, 200, 300, 340, 400 feet, etc., to the right, using some convenient scale, say 250 feet to the inch, as in the figure. At these points of division erect perpendiculars equal in length to the height of the points 0, 1, 2, 3.40, 4, etc., given in the fifth column of the above field notes, using in this case a larger scale, say 20 feet to the inch. Through the extremities of these perpendiculars draw the irregular line 0, 1, 2, 3 ..... 11, and the result, with some explanatory figures, will be the required plot or profile.

The making of a profile is much simplified by the use of *profile paper*, which may be had by the yard or roll.

If a *horizontal plot* is required, the bearings of the different portions of the section must be taken.

§ 35. Substitutes for the Y Level.

For many purposes not requiring accuracy, the following simple instruments in connection with a graduated rod will be found sufficient.

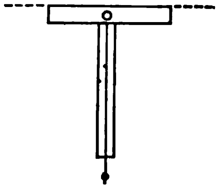


Fig. 46.

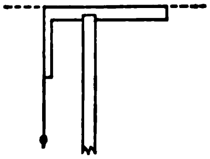


Fig. 47.

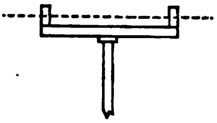


Fig. 48.

The **Plumb Level** (Fig. 46) consists of two pieces of wood joined at right angles. A straight line is drawn on the upright perpendicular to the upper edge of the cross-head.

The instrument is fastened to a support by a screw through the centre of the cross-head. The upper edge of the cross-head is brought to a level by making the line on the upright coincide with a plumb-line.

A modified form is shown in Fig. 47. A carpenter's square is supported by a post, the top of which is split or sawed so as to receive the longer arm. The shorter arm is made vertical by a plumb-line which brings the longer arm to a level.

The **Water Level** is shown in Fig. 48. The upright tubes are of glass, cemented into a connecting tube of any suitable material. The whole is nearly filled with water, and supported at a convenient height. The surface of the water in the uprights determines the level.

By sighting along the upper surface of the block in which the **Spirit Level** is mounted for the use of mechanics, a level line may be obtained.

EXERCISE V.

1. Find the difference of level of two places from the following field notes: back-sights, 5.2, 6.8, and 4.0; fore-sights, 8.1, 9.5, and 7.9.

2. Write the proper numbers in the third and fifth columns of the following table of field notes, and make a profile of the section.

Station.	+ *S.*	*H.I.*	− *S.*	*H.S.*	*Remarks.*
B	6.944			20.	Bench on post 22 ft. north of 0.
0			7.4		
1			5.6		
2			3.9		
3			4.6		
t.p.	3.855		5.513		
4			4.9		
5			3.5		
6			1.2		

3. Stake 0 of the following notes stands at the lowest point of a pond to be drained into a creek; stake 10 stands at the edge of the bank, and 10.25 at the bottom of the creek. Make a profile, draw the grade line through 0 and 10.25, and fill out the columns *H.G.* and *C.*, the former to show the height of grade line above the datum, and the latter, the depths of cut at the several stakes necessary to construct the drain.

Station.	+ *S.*	*H.I.*	− *S.*	*H.S.*	*H.G.*	*C.*	*Remarks.*
B	6.000			25.			Bench on rock 30 feet west of stake 1.
0			10.2		20.8	0.0	
1			5.3			5.3	
2			4.6				
3			4.0				
4			6.8				
5	4.572		7.090				
6			3.9				
7			2.0				
8			4.9				
9			4.3				
10.			4.5				
10.25			11.8				

§ 36. Topographical Levelling.

The principal object of topographical surveying is to show the contour of the ground. This operation, called topographical levelling, is performed by representing on paper the curved lines in which parallel horizontal planes at uniform distances apart would meet the surface.

It is evident that all points in the intersection of a horizontal plane with the surface of the ground are at the same level. Hence, it is only necessary to find points at the same level, and join these to determine a line of intersection.

The method commonly employed will be understood by a reference to Fig. 49. The ground *ABCD* is divided into equal squares, and a numbered stake driven at each intersection. By means of a level and levelling rod the heights of the other stations above *m* and *D*, the lowest stations, are determined. A plot of the ground with the intersecting lines is then drawn, and the height of each station written as in the figure.

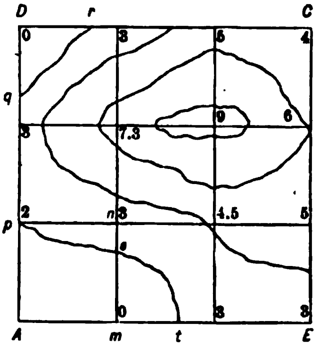


Fig 49.

Suppose that the horizontal planes are 2 feet apart; if the first passes through *m* and *D*, the second will pass through *p*, which is 2 feet above *m*; and since *n* is 3 feet above *m*, the second plane will cut the line *mn* in a point *s* determined by the proportion $mn : ms :: 3 : 2$. In like manner the points *t*, *q*, and *r* are determined.

The irregular line *tsp* ..... *qr* represents the intersection of the second horizontal plane with the surface of the ground. In like manner the intersections of the planes, respectively, 4, 6, and 8 feet above *m*, are traced.

It is evident that the more rapid the change in level the nearer these lines will approach each other.

CHAPTER V.

RAILROAD SURVEYING.

§ 37. General Remarks.

When the general route of a railroad has been determined, a middle surface line is run with the transit. A profile of this line is determined, as in § 34. The levelling stations are commonly 1 chain (100 feet) apart. Places of different level are connected by a gradient line, which intersects the perpendiculars to the datum line at the levelling stations in points determined by simple proportion. Hence, the distance of each levelling station, above or below the level or gradient line which represents the position of the road bed, is known.

§ 38. Cross Section Work.

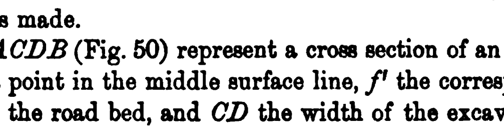


Fig. 50.

Excavations. If the road bed lies below the surface, an excavation is made.

Let $ACDB$ (Fig. 50) represent a cross section of an excavation, f a point in the middle surface line, f' the corresponding point in the road bed, and CD the width of the excavation at the bottom. The slopes at the sides are commonly made so that $AA' = \frac{2}{3}A'C$, and $BB' = \frac{2}{3}DB'$. ff' and CD being known, the points A, B, C', and D' are readily determined by a level and tape measure.

If from the area of the trapezoid $ABB'A'$ the areas of the triangles $AA'C$ and $BB'D$ be deducted, the remainder will be the area of the cross section.

In like manner the cross section at the next station may be determined. These two cross sections will be the bases of a frustum of a quadrangular pyramid whose volume will be the amount of the excavation, approximately.

Embankments. If the road bed lies above the surface, an embankment is made, the cross section of which is like that of the excavation, but inverted.

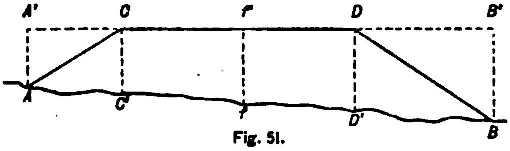


Fig. 51.

Fig. 51 represents the cross section of an embankment which is lettered so as to show its relation to Fig. 50.

§ 39. Railroad Curves.

When it is necessary to change the direction of a railroad, it is done gradually by a curve, usually the arc of a circle.

Let AB and AO (Fig. 52) represent two lines to be thus connected. Take $AD = AE = t$. The intersection of the perpendiculars DC and EC determines the centre C, and the radius of curvature $DC = r$. The length of the radius

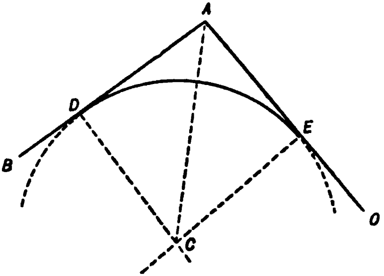


Fig. 52.

of curvature will depend on the angle A and the tangent AD. For, in the right triangle ADC,

$$\tan DAC = \frac{DC}{AD}, \text{ or } \tan \tfrac{1}{2} A = \frac{r}{t}.$$

$$\text{Hence, } r = t \tan \tfrac{1}{2} A.$$

To Lay out the Curve.

First Method. Let Dm (Fig. 53) represent a portion of the tangent. It is required to find mP, the perpendicular to the tangent meeting the curve at P.

$$mP = Dn = CD - Cn.$$

$$\text{But} \quad CD = r,$$

$$\text{and} \quad Cn = \sqrt{\overline{CP}^2 - \overline{Pn}^2}$$

$$= \sqrt{r^2 - t^2}.$$

$$\text{Hence,} \quad mP = r - \sqrt{r^2 - t^2}.$$

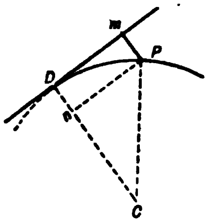


Fig. 53.

Second Method. It is required to find mP (Fig. 54) in the direction of the centre.

$$mP = mC - PC.$$

$$\text{But} \quad mC = \sqrt{\overline{DC}^2 + \overline{Dm}^2} = \sqrt{r^2 + t^2}.$$

Hence,

$$mP = \sqrt{r^2 + t^2} - r.$$

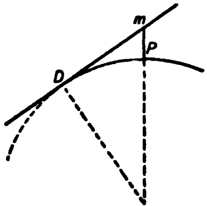


Fig. 54.

Third Method. Place transits at D and E (Fig. 55). Direct the telescope of the former to E, and of the latter to A. Turn each toward the curve the same number of degrees, and mark P, the point of intersection of the lines of sight. P will be a point in the circle to which AD and AE are tangents at D and E, respectively.

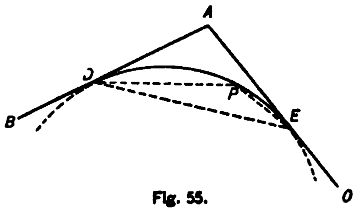


Fig. 55.

Fourth Method. Measure the angle A and the tangents $AD = AE$ (Fig. 56). Compute r. Select any distance l (the length of the chain will be found convenient). Place the transit at D and direct toward A. Turn off an angle ADP determined by the equation $\sin ADP = \frac{l}{2r}$, and measure $DP = l$; make the angle $ADP' = 2\,ADP$ and $PP' = l$; make the angle $ADP'' = 3\,ADP$ and $P'P'' = l$; etc. P, P', P'', etc., will be in the circumference of the required arc.

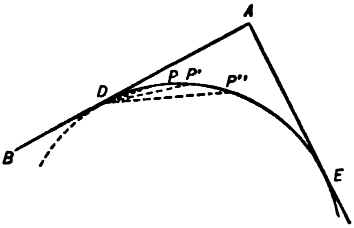


Fig. 56.

ANSWERS.

SURVEYING.

EXERCISE I.

1. 8 A. 64 P.
2. 29 A. $7\frac{3}{5}$ P.
3. 4 A. $5\frac{8}{25}$ P.
4. $115\frac{7}{20}$ P.
5. 3 A. 78 P.
6. 13 A. $6\frac{1}{10}$ P.
7. 11 A. 157 P.
8. 7.51925.
9. 13.0735.
10. 2 A. $58\frac{1}{2}$ P.
11. 4 A. 35 P.

EXERCISE II.

1. 2 A. 26 P.
2. 20 A. 12 P.
3. 2 A. 54 P.
4. 2 A. 151 P.
5. 8 A. 54 P.
6. 5 A. 42 P.
7. 2 A. 78 P.
8. 3 A. 122 P.
9. 6 A. 2 P.
10. 9 A. 40 P.

EXERCISE III.

1. 2 A. $12\frac{1}{2}$ P.
2. 98 A. 92 P.

EXERCISE IV.

1. $AE = 3.75$ ch.
2. $AE = 3.50$ ch.;
   $EG = 3.42$ ch.
3. $AE = 4.55$ ch.
4. $AE = 5.50$ ch.
5. $CE = 4.455$ ch.
6. $AD = 2.275$ ch.;
   $BE = 1.82$ ch.
7. $AD = 4.51$ ch.;
   $BE = 3.608$ ch.
8. The distances on AB are 2, 3, and 5 ch.
9. EM(on EA) $= 2.5087$ ch.
   AN(on AB) $= 6.439$ ch.
10. Let $EG > DF$,

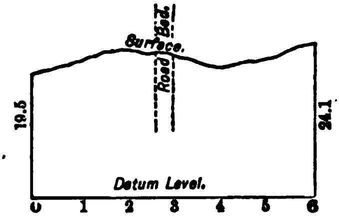
$$\text{then}\begin{cases}AE = 12.247 \text{ ch.}\\ AG = 9.798 \text{ ch.}\\ AD = 8.659 \text{ ch.}\\ AF = 6.928 \text{ ch.}\end{cases}$$

11. Let $DG > EF$,

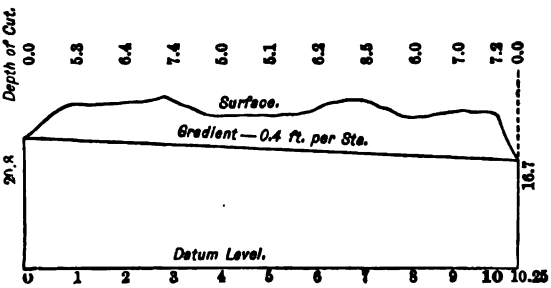
$$\text{then}\begin{cases}CG = 14.862 \text{ ch.}\\ CD = 13.113 \text{ ch.}\\ CF = 11.404 \text{ ch.}\\ CE = 10.062 \text{ ch.}\end{cases}$$

Exercise V.

1. 9.5 ft.
2. Third column: 26.944 opposite 0; 25.286 opposite 4.
   Fifth column: 20, 19.5, 23, 22.3, 21.431, 20.4, 21.8, and 24.1.



3. Column *H.G.* 20.8, 20.4, 20.0, 19.6, etc.
   Column *C.* 0.0, 5.3, 6.4, 7.4, 5.0, 5.1, etc.



FIVE-PLACE

LOGARITHMIC AND TRIGONOMETRIC TABLES.

ARRANGED BY

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AND

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BOSTON:
PUBLISHED BY GINN & COMPANY.
1887.

Entered according to Act of Congress, in the year 1882, by
G. A. WENTWORTH AND G. A. HILL,
in the office of the Librarian of Congress at Washington.

J. S. CUSHING & CO., PRINTERS, BOSTON.

Required the logarithm of 0.0015764.

The required mantissa is the same as the mantissa for 1576.4; therefore it will be found by adding to the mantissa for 1576 four-tenths of the difference between the mantissas for 1576 and 1577.

The mantissa for 1576 is 19756.

The difference between the mantissas for 1576 and 1577 is 27.

Hence, the mantissa for 1576.4 is $19756 + (0.4 \times 27) = 19767$.

Therefore, the required logarithm of 0.0015764 is $7.19767 - 10$.

Required the logarithm of 32.6708.

The required mantissa is the same as the mantissa for 3267.08; therefore it will be found by adding to the mantissa for 3267 eight-hundredths of the

11. The logarithms of numbers that can be derived from one another by multiplication or division by an integral power of 10 have the same mantissa.

For, multiplying or dividing a number by an integral power of 10 will increase or diminish its logarithm by the exponent of that power of 10; and since this exponent is an integer, the mantissa of the logarithm will be unaffected.

Thus,

$$\begin{aligned}
\log 4.6021 &= 0.66296. \quad \text{(Page 9.)}\\
\log 460.21 &= \log (4.6021 \times 10^2) = \log 4.6021 + \log 10^2\\
&= 0.66296 + 2 = 2.66296.\\
\log 460210 &= \log (4.6021 \times 10^5) = \log 4.6021 + \log 10^5\\
&= 0.66296 + 5 = 5.66296.\\
\log 0.046021 &= \log (4.6021 \div 10^2) = \log 4.6021 - \log 10^2\\
&= 0.66296 - 2 = 8.66296 - 10.
\end{aligned}$$

TABLE I.

12. In this table (pp. 1–19) the vertical columns headed N contain the numbers, and the other columns the logarithms. On page 1 both the characteristic and the mantissa are printed. On pages 2–19 the mantissa only is printed.

The fractional part of a logarithm can be expressed only approximately, and in a five-place table all figures that follow the fifth are rejected. Whenever the sixth figure is 5, or more, the fifth figure is increased by 1. The figure $\underline{5}$ is written when the value of the figure in the place in which it stands, together with the succeeding figures, is more than 4½, but less than 5.

Thus, if the mantissa of a logarithm written to seven places is 5328732, it is written in this table (a five-place table) 53287. If it is 5328751, it is written 53288. If it is 5328461 or 5328499, it is written in this table 5328$\underline{5}$.

Again, if the mantissa is 5324981, it is written 532$\underline{5}$0; and if it is 4999967, it is written $\underline{5}$0000.

the logarithm is given on page 1. If zeros follow [illegible] figures, or if the number is a proper decimal fraction, the characteristic must be determined by § 10.

14. If the given number has three significant figures, it will be found in the column headed N (pp. 2–19), and the mantissa of its logarithm in the next column to the right, and on the same line. Thus,

Page 2. log 145 = 2.16137, log 14500 = 4.16137.
Page 14. log 716 = 2.85491, log 0.716 = 9.85491 − 10.

15. If the given number has four significant figures, the first three will be found in the column headed N, and the fourth at the top of the page in the line containing the figures 1, 2, 3, etc. The mantissa will be found in the column headed by the fourth figure, and on the same line with the first three figures. Thus,

Page 15. log 7682 = 3.88547, log 76.85 = 1.88564.
Page 18. log 93280 = 4.96979, log 0.9468 = 9.97626 − 10.

16. If the given number has five or more significant figures, a process called **interpolation** is required.

Interpolation is based on the *assumption* that between two consecutive mantissas of the table the change in the mantissa is directly proportional to the change in the number.

Required the logarithm of 34237.

The required mantissa is (§ 11) the same as the mantissa for 3423.7; therefore it will be found by adding to the mantissa of 3423 seven-tenths of the difference between the mantissas for 3423 and 3424.

The mantissa for 3423 is 53441.

The difference between the mantissas for 3423 and 3424 is 12.

Hence, the mantissa for 3423.7 is 53441 + (0.7 × 12) = 53449.

Therefore, the required logarithm of 34237 is 4.53449.

Required the logarithm of 0.0015764.

The required mantissa is the same as the mantissa for 1576.4; therefore it will be found by adding to the mantissa for 1576 four-tenths of the difference between the mantissas for 1576 and 1577.

The mantissa for 1576 is 19756.

The difference between the mantissas for 1576 and 1577 is 27.

Hence, the mantissa for 1576.4 is 19756 + (0.4 × 27) = 19767.

Therefore, the required logarithm of 0.0015764 is 7.19767 − 10.

Required the logarithm of 32.6708.

The required mantissa is the same as the mantissa for 3267.08; therefore it will be found by adding to the mantissa for 3267 eight-hundredths of the difference between the mantissas for 3267 and 3268.

The mantissa for 3267 is 51415.

The difference between the mantissas for 3267 and 3268 is 13.

Hence, the mantissa for 3267.08 is 51415 + (0.08 × 13) = 51416.

Therefore, the required logarithm of 32.6708 is 1.51416.

17. When the fraction of a unit in the part to be added to the mantissa for four figures is less than 0.5 it is to be neglected; when it is 0.5 or more than 0.5 it is to be taken as one unit.

Thus, in the first example, the part to be added to the mantissa for 3423 is 8.4, and the .4 is rejected. In the second example, the part to be added to the mantissa for 1576 is 10.8, and 11 is added.

To Find the Number Corresponding to a Given Logarithm.

18. If the given mantissa can be found in the table, the first three figures of the required number will be found in the same line with the mantissa in the column headed N, and the fourth figure at the top of

Find the angle

$$\log 0.54936 = 9.73986 - 10$$

$$\operatorname{colog}\frac{1}{a''} = \log a'' = 5.31443$$

$$\log \text{angle} = 5.05429 = \log 113316$$

$$\therefore \text{angle} = 113316'' = 31^\circ\, 28'\, 36''$$

23. The relations between arcs and angles given in Table II. are readily deduced from the circular measure of an angle.

In **Circular Measure** an angle is defined by the equation

Therefore, the requi[illegible] number [illegible] 300.

Find the number corresponding to the logarithm 7.50325 − 10.

Page 6. The number for the mantissa 50325 is 3186.

Therefore, the required number is 0.003186.

19. If the given mantissa cannot be found in the table, find in the table the two adjacent mantissas between which the given mantissa lies, and the four figures corresponding to the smaller of these two mantissas will be the first four significant figures of the required number. If more than four figures are desired, they may be found by interpolation, as in the following examples:

Find the number corresponding to the logarithm 1.48762.

Here the two adjacent mantissas of the table, between which the given mantissa 48762 lies, are found to be (page 6) 48756 and 48770. The corresponding numbers are 3073 and 3074. The smaller of these, 3073, contains the first four significant figures of the required number.

The difference between the two adjacent mantissas is 14, and the difference between the corresponding numbers is 1.

The difference between the smaller of the two adjacent mantissas, 48756, and the given mantissa, 48762, is 6. Therefore, the number to be annexed to 3073 is $\frac{6}{14}$ of $1 = 0.428$, and the fifth significant figure of the required number is 4.

Hence, the required number is 30.734.

Find the number corresponding to the logarithm 7.82326 − 10.

The two adjacent mantissas between which 82326 lies are (page 13) 82321 and 82328. The number corresponding to the mantissa 82321 is 6656.

The difference between the two adjacent mantissas is 7, and the difference between the corresponding numbers is 1.

The difference between the smaller mantissa, 82321, and the given mantissa, 82326, is 5. Therefore, the number to be annexed to 6656 is $\frac{5}{7}$ of $1 = 0.7$, and the fifth significant figure of the required number is 7.

Hence, the required number is 0.0066567.

In using a five-place table the numbers corresponding to mantissas may be carried to five significant figures, and in the first part of the table to six figures.*

16. If the given number has five or more significant figures, a process called **interpolation** is required.

Interpolation is based on the *assumption* that between two consecutive mantissas of the table the change in the mantissa is directly proportional to the change in the number.

Required the logarithm of 34237.

The required mantissa is (§ 11) the same as the mantissa for 3423.7; there[illegible] will be found by adding to the mantissa of 3423 seven-tenths of the ber preceding the mantissa should be increased by such a number as will make the subtrahend, when divided by the index of the root, 10 or a multiple of 10.

---

* In most tables of logarithms proportional parts are given as an aid to interpolation; but, after a little practice, the operation can be performed nearly as rapidly without them. Their omission allows a page with larger-faced type and more open spacing, and consequently less trying to the eyes.

(7) Find the square root of 0.000043641.

$$\begin{array}{lll}
\text{Page 8.} & \log 0.000043641 & = 5.63989 - 10 \\
 & & \ 10 \qquad\ \ - 10 \\
\text{Divide by 2 (§ 5),} & & 2\overline{)15.63989 - 20} \\
\text{Page 13.} & \log \sqrt{0.000043641} & = 7.81995 - 10 = \log 0.0066062 \\
 & \therefore\ \sqrt{0.000043641} & = 0.0066062
\end{array}$$

(8) Find the sixth root of 0.076553.

$$\begin{array}{lll}
\text{Page 15.} & \log 0.076553 & = 8.88397 - 10 \\
 & & \ 50 \qquad\ \ - 50 \\
\text{Divide by 6 (§ 5),} & & 6\overline{)58.88397 - 60} \\
\text{Page 13} & \log \sqrt[6]{0.076553} & = 9.81400 - 10 = \log 0.65163 \\
 & \therefore\ \sqrt[6]{0.076553} & = 0.65163
\end{array}$$

TABLE II.

22. This table (page 20) contains the value of the number π, its most useful combinations, and their logarithms.

Find the length of an arc of 47° 32′ 57″ in a unit circle.

$$\begin{array}{ll}
\quad 47^\circ\, 32'\, 57'' & = 171177'' \\
\log 171177 & = 5.23344 \\
\log \dfrac{1}{a''} & = 4.68557 - 10 \\
\hline
\log \text{arc } 47^\circ\, 32'\, 57'' & = 9.91901 - 10 = \log 0.82994 \\
\therefore \text{ length of arc} & = 0.82994
\end{array}$$

Find the angle if the length of its arc in a unit circle = 0.54936.

$$\begin{array}{ll}
\log 0.54936 & = 9.73986 - 10 \\
\operatorname{colog} \dfrac{1}{a''} = \log a'' & = 5.31443 \\
\hline
\log \text{angle} & = 5.05429 = \log 113316 \\
\therefore \text{ angle} & = 113316'' = 31^\circ\, 28'\, 36''
\end{array}$$

23. The relations between arcs and angles given in Table II. are readily deduced from the circular measure of an angle.

In **Circular Measure** an angle is defined by the equation

$$\text{angle} = \frac{\text{arc}}{\text{radius}},$$

in which the word arc denotes the length of the arc corresponding to the angle, when both arc and radius are expressed in terms of the *same linear unit.*

Since the arc and radius for a given angle in different circles vary in the same ratio, the value of the angle given by this equation is independent of the value of the radius. If the radius is unity, the equation defining the angle becomes

$$\text{angle} = \text{arc}.$$

That is, in circular measure an angle is measured by the length of its arc in a unit circle. Therefore,

If the arc = circumference, the angle $= 2\pi$.
If the arc = semicircumference, the angle $= \pi$.
If the arc = quadrant, the angle $= \frac{1}{2}\pi$.
If the arc = radius (= 1), the angle = 1;

that is, in circular measure the angular unit is the angle whose arc is equal in length to the radius of the circle.

Since 180° in common measure equals π units in circular measure, therefore

$$1^\circ \text{ in common measure } = \frac{\pi}{180} \text{ units in circular measure;}$$

$$1 \text{ unit in circular measure} = \frac{180^\circ}{\pi} \text{ in common measure.}$$

By means of these two equations, the value of an angle expressed in one measure may be changed to its value in the other measure.

Thus, the angle whose arc is equal to the radius is an angle of 1 unit in circular measure, and is equal to $\frac{180^\circ}{\pi}$, or 57° 17′ 45″, very nearly.

TABLE III.

24. This table (pp. 21–49) contains the logarithms of the trigonometric functions of angles. In order to avoid negative characteristics, the characteristic of every logarithm is printed 10 too large. Therefore, − 10 is to be annexed to each logarithm.

On pages 28–49 the characteristic remains the same throughout each column, and is printed at the top and the bottom of the column. But on pp. 30, 49, the characteristic changes one unit in value at the places marked with bars. Above these bars the proper characteristic is printed at the top, and below them at the bottom, of the column.

25. On pages 28–49 the log sin, log tan, log cot, and log cos, of 1° to 89°, are given to every minute. Conversely, this part of the table gives the value of the angle to the nearest minute when log sin, log tan, log cot, or log cos is known, provided log sin or log cos lies between 8.23822 and 9.99992, and log tan or log cot lies between 8.23829 and 11.76171.

If the exact value of the given logarithm of a function is not found in the table, the value nearest to it is to be taken, unless interpolation is employed as explained in § 26.

If the angle is less than 45°, the number of degrees is printed at the top of the page, and the number of minutes in the column to the left of the columns containing the logarithm. If the angle is greater than 45°, the number of degrees is printed at the bottom of the page, and the number of minutes in the column to the right of the columns containing the logarithms.

If the angle is less than 45°, the names of its functions are printed at the top of the page; if greater than 45°, at the bottom of the page. Thus,

Page 38. log sin 21° 37′ = 9.56631 − 10.
Page 45. log cot 36° 53′ = 10.12473 − 10 = 0.12473.
Page 37. log cos 69° 14′ = 9.54969 − 10.
Page 49. log tan 45° 59′ = 10.01491 − 10 = 0.01491.
Page 48. If log cos = 9.87468 − 10, angle = 41° 28′.
Page 34. If log cot = 9.39353 − 10, angle = 76° 6′.

If log sin = 9.47760 − 10, the nearest log sin in the table is 9.47774 − 10 (page 36), and the angle corresponding to this value is 17° 29′.

If log tan = 0.76520 = 10.76520 − 10, the nearest log tan in the table is 10.76490 − 10 (page 32), and the angle corresponding to this value is 80° 15′.

26. If it is desired to obtain the logarithms of the functions of angles that contain seconds, or to obtain the value of the angle in degrees, minutes, and seconds, from the logarithms of its functions, interpolation must be employed. Here it must be remembered that,

The difference between two consecutive angles in the table is 60″.

Log sin and log tan increase as the angle increases; log cos and log cot diminish as the angle increases.

Find log tan 70° 46′ 8″.

Page 37. log tan 70° 46′ = 0.45731.

The difference between the mantissas of log tan 70° 46′ and log tan 70° 47′ is 41, and $\frac{8}{60}$ of 41 = 5.

As the function is increasing, the 5 must be added to the figure in the fifth place of the mantissa 45731; and

Therefore log tan 70° 46′ 8″ = 0.45736.

Find log cos 47° 35′ 4″.

Page 48. log cos 47° 35′ = 9.82899 − 10.

The difference between this mantissa and the mantissas of the next log cos is 14, and $\frac{4}{60}$ of 14 = 1.

As the function is decreasing, the 1 must be subtracted from the figure in the fifth place of the mantissa 82899; and

Therefore log cos 47° 35′ 4″ = 9.82898 − 10.

Find the angle for which log sin = 9.45359 − 10.

Page 35. The mantissa of the nearest smaller log sin in the table is 45334.

The angle corresponding to this value is 16° 30′.

The difference between 45334 and the given mantissa, 45359, is 25.

The difference between 45334 and the next following mantissa, 45377, is 43, and $\frac{25}{43}$ of 60″ = 35″.

As the function is increasing, the 35″ must be added to 16° 30′; and the required angle is 16° 30′ 35″.

Find the angle for which log cot = 0.73478.

Page 32. The mantissa of the nearest smaller log cot in the table is 73415.

The angle corresponding to this value is 10° 27′.

The difference between 73415 and the given mantissa is 63.

The difference between 73415 and next following mantissa is 71, and $\frac{63}{71}$ of 60″ = 53″.

As the function is decreasing, the 53″ must be subtracted from 10° 27′; and the required angle is 10° 26′ 7″.

27. If log sec or log csc of an angle is desired, it may be found from the table by the formulas,

$$\sec A = \frac{1}{\cos A}; \quad \text{hence, } \log \sec A = \text{colog} \cos A.$$

$$\csc A = \frac{1}{\sin A}; \quad \text{hence, } \log \csc A = \text{colog} \sin A.$$

Page 31. log sec 8° 28′ = colog cos 8° 28′ = 0.00476.

Page 42. log csc 59° 36′ 44″ = colog sin 59° 36′ 44″ = 0.06418.

28. If a given angle is between 0° and 1°, or between 89° and 90°; or, conversely, if a given log sin or log cos does *not* lie between the limits 8.23822 and 9.99992 in the table; or, if a given log tan or log cot does *not* lie between the limits 8.23829 and 11.76171 in the table; then pages 21–24 of Table III. must be used.

On page 21, log sin of angles between 0° and 0° 3′, or log cos of the complementary angles between 89° 57′ and 90°, are given to every second; for the angles between 0° and 0° 3′, log tan = log sin, and log cos = 0.00000; for the angles between 89° 57′ and 90°, log cot = log cos, and log sin = 0.00000.

On pages 22–24, log sin, log tan, and log cos of angles between 0° and 1°, or log cos, log cot, and log sin of the complementary angles between 89° and 90°, are given to every 10″.

Whenever log tan or log cot is not given, they may be found by the formulas,

$$\log \tan = \text{colog} \cot. \qquad \log \cot = \text{colog} \tan.$$

Conversely, if a given log tan or log cot is not contained in the table, then the colog must be found; this will be the log cot or log tan, as the case may be, and will be contained in the table.

On pages 25–27 the logarithms of the functions of angles between 1° and 2°, or between 88° and 90°, are given in the manner employed on pages 22–24. These pages should be used if the angle lies between these limits, and if not only degrees and minutes, but degrees, minutes, and multiples of 10″ are given or required.

When the angle is between 0° and 2°, or 88° and 90°, and a greater degree of accuracy is desired than that given by the table, interpolation may be employed; but for these angles interpolation does not always give true results, and it is better to use Table IV.

Find log tan 0° 2′ 47″, and log cos 89° 37′ 20″.

Page 21. log tan 0° 2′ 47″ = log sin 0° 2′ 47″ = 6.90829 − 10.
Page 23. log cos 89° 37′ 20″ = 7.81911 − 10.

Find log cot 0° 2′ 15″.

$$\begin{array}{lll} & & 10 \qquad -10 \\ \text{Page 21.} & \log\tan 0^\circ 2' 15'' = & \underline{6.81591 - 10} \\ \text{Therefore,} & \log\cot 0^\circ 2' 15'' = & 3.18409 \end{array}$$

Find log tan 89° 38′ 30″.

$$\begin{array}{lll} & & 10 \qquad -10 \\ \text{Page 23.} & \log\cot 89^\circ 38' 30'' = & \underline{7.79617 - 10} \\ \text{Therefore,} & \log\tan 89^\circ 38' 30'' = & 2.20383 \end{array}$$

Find the angle for which log tan = 6.92090 − 10.

Page 21. The nearest log tan is 6.92110 − 10.
The corresponding angle for which is 0° 2′ 52″.

Find the angle for which log cos = 7.70240 − 10.

Page 22. The nearest log cos is 7.70261 − 10.
The corresponding angle for which is 89° 42′ 40″.

Find the angle for which log cot = 2.37368.

This log cot is not contained in the table.
The colog cot = 7.62632 − 10 = log tan.
The log tan in the table nearest to this is (page 22) 7.62510 − 10, and the angle corresponding to this value of log tan is 0° 14′ 30″.

29. If an angle x is between 90° and 360°, it follows, from formulas established in Trigonometry, that,

between 90° and 180°,	between 180° and 270°,
$\log\sin x = \log\sin(180^\circ - x)$,	$\log\sin x = \log\sin(x - 180^\circ)_n$,
$\log\cos x = \log\cos(180^\circ - x)_n$,	$\log\cos x = \log\cos(x - 180^\circ)_n$,
$\log\tan x = \log\tan(180^\circ - x)_n$,	$\log\tan x = \log\tan(x - 180^\circ)$,
$\log\cot x = \log\cot(180^\circ - x)_n$;	$\log\cot x = \log\text{oot}(x - 180^\circ)$;

between 270° and 360°,

$$\log\sin x = \log\sin(360° - x)_n,$$
$$\log\cos x = \log\cos(360° - x),$$
$$\log\tan x = \log\tan(360° - x)_n,$$
$$\log\cot x = \log\cot(360° - x)_n.$$

The letter *n* is placed (according to custom) after the logarithms of those functions which are negative in value.

The above formulas show, without further explanation, how to find by means of Table III. the logarithms of the functions of any angle between 90° and 360°.

5 Thus, $\log\sin 137° 45' 22'' = \log\sin\ 42° 14' 38'' = 9.82756 - 10.$
5 $\log\cos 137° 45' 22'' = \log_n\cos 42° 14' 38'' = 9.86940_n - 10.$
$\log\tan 137° 45' 22'' = \log_n\tan 42° 14' 38'' = 9.95815_n - 10.$
5 $\log\cot 137° 45' 22'' = \log_n\cot 42° 14' 38'' = 0.04185_n.$
$\log\sin 209° 32' 50'' = \log_n\sin 29° 32' 50'' = 9.69297_n - 10.$
5 $\log\cos 330° 27' 10'' = \log\cos\ 29° 32' 50'' = 9.93949 - 10.$

Conversely, to a given logarithm of a trigonometric function there correspond between 0° and 360° four angles, one angle in each quadrant, and so related that if x denote the acute angle, the other three angles are $180° - x$, $180° + x$, and $360° - x$.

If besides the given logarithm it is known whether the function is positive or negative, the ambiguity is confined to *two* quadrants, therefore to *two* angles.

Thus, if the log tan = 9.47451 − 10, the angles are 16° 36′ 17″ in Quadrant I. and 196° 36′ 17″ in Quadrant III.; but if the log tan = $9.47451_n - 10$, the angles are 163° 23′ 43″ in Quadrant II. and 343° 23′ 43″ in Quadrant IV.

To remove all ambiguity, further conditions are required, or a knowledge of the special circumstances connected with the problem in question.

TABLE IV.

30. This table (page 50) must be used when great accuracy is desired in working with angles between 0° and 2°, or between 88° and 90°.

The values of S and T are such that when the angle a is expressed in seconds,

$$S = \log\sin a - \log a'',$$
$$T = \log\tan a - \log a''.$$

Hence follow the formulas given on page 50.

The values of S and T are printed with the characteristic 10 too large, and in using them −10 must always be annexed.

Find log sin 0° 58′ 17″.

0° 58′ 17″ = 3497″
log 3497 = 3.54370
S = 4.68555 − 10
log sin 0° 58′ 17″ = 8.22925 − 10

Find log cos 88° 26′ 41.2″.

90° − 88° 26′ 41.2″ = 1° 33′ 18.8″
= 5598.8″
log 5598.8 = 3.74809
S = 4.68552 − 10
log cos 88° 26′ 41.2″ = 8.43361 − 10

Find log tan 0° 52′ 47.5″.

0° 52′ 47.5″ = 3167.5″
log 3167.5 = 3.50072
T = 4.68561 − 10
log tan 0° 52′ 47.5″ = 8.18633 − 10

Find log tan 89° 54′ 37.362″.

90° − 89° 54′ 37.362″ = 0° 5′ 22.638′
= 322.638″
log 322.638 = 2.50871
T = 4.68558 − 10
log cot 89° 54′ 37.362″ = 7.19429 − 10
log tan 89° 54′ 37.362″ = 2.80571

Find the angle, if log sin = 6.72306 − 10.

6.72306 − 10
S = 4.68557 − 10
Subtract, 2.03749 = log 109.015
109.015″ = 0° 1′ 49.015″

Find the angle for which log cot = 1.67604.

colog cot = 8.32396 − 10
T = 4.68564 − 10
Subtract, 3.63832 = log 4348.3
4348.3″ = 1° 12′ 28.3″

Find the angle for which log tan = 1.55407.

colog tan = 8.44593 − 10
T = 4.68569 − 10
Subtract, 3.76024 = log 5757.6
5757.6″ = 1° 35′ 57.6″,
and 90° − 1° 35′ 57.6″ = 88° 24′ 2.4″.
Therefore, the angle required is 88° 24′ 2.4″.

TABLE V.

31. Table V. (pp. 51–53), contains the natural sines, cosines, tangents, and cotangents of angles from 0° to 90°, at intervals of 10′. If greater accuracy is desired it may be obtained by interpolation.

TABLE VI.

32. This table (p. 54), containing the circumferences and areas of circles, does not require explanation.

Note. In preparing the preceding explanations, free use has been made of the Logarithmic Tables by F. G. Gauss, from which, also, Tables II. and VI. have been taken.

TABLE VII.

33. This table (pp. 55–60) gives the latitude and departure to three places of decimals for distances from 1 to 10, corresponding to bearings from 0° to 90° at intervals of 15′.

If the bearing does not exceed 45° it is found in the *left*-hand column, and the designations of the columns under "Distance" are taken from the *top* of the page; but if the bearing exceeds 45°, it is found in the *right*-hand column, and the designations of the columns under "Distance" are taken from the *bottom* of the page.

The method of using the table will be made plain by the following examples: —

(1) Let it be required to find the latitude and departure of the course N. 35° 15′ E. 6 chains.

On p. 60, left-hand column, look for 35° 15′; opposite this bearing, in the vertical column headed "Distance 6," are found 4.900 and 3.463 under the headings "Latitude" and "Departure" respectively. Hence, latitude or northing = 4.900 chains, and departure or easting = 3.463 chains.

(2) Let it be required to find the latitude and departure of the course S. 87° W. 2 chains.

As the bearing exceeds 45°, we look in the right-hand column of p. 55, and opposite 87° in the column marked "Distance 2" we find (taking the designations of the columns from the bottom of the page) latitude = .105 chains, and departure = 1.997 chains. Hence, latitude or southing = .105 chains, and departure or westing = 1.997 chains.

(3) Let it be required to find the latitude and departure of the course N. 15° 45′ W. 27.36 chains.

In this case we find the required numbers for each figure of the distance separately, arranging the work as in the following table. In practice, only the last columns under "Latitude" and "Departure" are written.

Distance.	Latitude.	Departure.
20 = 2 × 10	1.925 × 10 = 19.25	0.543 × 10 = 5.43
7	6.737	1.90
0.3 = 3 ÷ 10	2.887 ÷ 10 = 0.289	0.814 ÷ 10 = 0.081
0.06 = 6 ÷ 100	5.775 ÷ 100 = 0.058	1.628 ÷ 100 = 0.016
27.36	26.334	7.427

Hence, latitude = 26.334 chains, and departure = 7.427 chains.

TABLE I.

THE

COMMON OR BRIGGS LOGARITHMS

OF THE

NATURAL NUMBERS

From 1 to 10000.

1—100

N	log	N	log	N	log	N	log	N	log
1	0.00 000	21	1.32 222	41	1.61 278	61	1.78 533	81	1.90 849
2	0.30 103	22	1.34 242	42	1.62 325	62	1.79 239	82	1.91 381
3	0.47 712	23	1.36 173	43	1.63 347	63	1.79 934	83	1.91 908
4	0.60 206	24	1.38 021	44	1.64 345	64	1.80 618	84	1.92 428
5	0.69 897	25	1.39 794	45	1.65 321	65	1.81 291	85	1.92 942
6	0.77 815	26	1.41 497	46	1.66 276	66	1.81 954	86	1.93 450
7	0.84 510	27	1.43 136	47	1.67 210	67	1.82 607	87	1.93 952
8	0.90 309	28	1.44 716	48	1.68 124	68	1.83 251	88	1.94 448
9	0.95 424	29	1.46 240	49	1.69 020	69	1.83 885	89	1.94 939
10	1.00 000	30	1.47 712	50	1.69 897	70	1.84 510	90	1.95 424
11	1.04 139	31	1.49 136	51	1.70 757	71	1.85 126	91	1.95 904
12	1.07 918	32	1.50 515	52	1.71 600	72	1.85 733	92	1.96 379
13	1.11 394	33	1.51 851	53	1.72 428	73	1.86 332	93	1.96 848
14	1.14 613	34	1.53 148	54	1.73 239	74	1.86 923	94	1.97 313
15	1.17 609	35	1.54 407	55	1.74 036	75	1.87 506	95	1.97 772
16	1.20 412	36	1.55 630	56	1.74 819	76	1.88 081	96	1.98 227
17	1.23 045	37	1.56 820	57	1.75 587	77	1.88 649	97	1.98 677
18	1.25 527	38	1.57 978	58	1.76 343	78	1.89 209	98	1.99 123
19	1.27 875	39	1.59 106	59	1.77 085	79	1.89 763	99	1.99 564
20	1.30 103	40	1.60 206	60	1.77 815	80	1.90 309	100	2.00 000
N	log	N	log	N	log	N	log	N	log

N	0	1	2	3	4	5	6	7	8	9
100	00 000	00 043	00 087	00 130	00 173	00 217	00 260	00 303	00 346	00 389
101	00 432	00 475	00 518	00 561	00 604	00 647	00 689	00 732	00 775	00 817
102	00 860	00 903	00 945	00 988	01 030	01 072	01 115	01 157	01 199	01 242
103	01 284	01 326	01 368	01 410	01 452	01 494	01 536	01 578	01 620	01 662
104	01 703	01 745	01 787	01 828	01 870	01 912	01 953	01 995	02 036	02 078
105	02 119	02 160	02 202	02 243	02 284	02 325	02 366	02 407	02 449	02 490
106	02 531	02 572	02 612	02 653	02 694	02 735	02 776	02 816	02 857	02 898
107	02 938	02 979	03 019	03 060	03 100	03 141	03 181	03 222	03 262	03 302
108	03 342	03 383	03 423	03 463	03 503	03 543	03 583	03 623	03 663	03 703
109	03 743	03 782	03 822	03 862	03 902	03 941	03 981	04 021	04 060	04 100
110	04 139	04 179	04 218	04 258	04 297	04 336	04 376	04 415	04 454	04 493
111	04 532	04 571	04 610	04 650	04 689	04 727	04 766	04 805	04 844	04 883
112	04 922	04 961	04 999	05 038	05 077	05 115	05 154	05 192	05 231	05 269
113	05 308	05 346	05 385	05 423	05 461	05 500	05 538	05 576	05 614	05 652
114	05 690	05 729	05 767	05 805	05 843	05 881	05 918	05 956	05 994	06 032
115	06 070	06 108	06 145	06 183	06 221	06 258	06 296	06 333	06 371	06 408
116	06 446	06 483	06 521	06 558	06 595	06 633	06 670	06 707	06 744	06 781
117	06 819	06 856	06 893	06 930	06 967	07 004	07 041	07 078	07 115	07 151
118	07 188	07 225	07 262	07 298	07 335	07 372	07 408	07 445	07 482	07 518
119	07 555	07 591	07 628	07 664	07 700	07 737	07 773	07 809	07 846	07 882
120	07 918	07 954	07 990	08 027	08 063	08 099	08 135	08 171	08 207	08 243
121	08 279	08 314	08 350	08 386	08 422	08 458	08 493	08 529	08 565	08 600
122	08 636	08 672	08 707	08 743	08 778	08 814	08 849	08 884	08 920	08 955
123	08 991	09 026	09 061	09 096	09 132	09 167	09 202	09 237	09 272	09 307
124	09 342	09 377	09 412	09 447	09 482	09 517	09 552	09 587	09 621	09 656
125	09 691	09 726	09 760	09 795	09 830	09 864	09 899	09 934	09 968	10 003
126	10 037	10 072	10 106	10 140	10 175	10 209	10 243	10 278	10 312	10 346
127	10 380	10 415	10 449	10 483	10 517	10 551	10 585	10 619	10 653	10 687
128	10 721	10 755	10 789	10 823	10 857	10 890	10 924	10 958	10 992	11 025
129	11 059	11 093	11 126	11 160	11 193	11 227	11 261	11 294	11 327	11 361
130	11 394	11 428	11 461	11 494	11 528	11 561	11 594	11 628	11 661	11 694
131	11 727	11 760	11 793	11 826	11 860	11 893	11 926	11 959	11 992	12 024
132	12 057	12 090	12 123	12 156	12 189	12 222	12 254	12 287	12 320	12 352
133	12 385	12 418	12 450	12 483	12 516	12 548	12 581	12 613	12 646	12 678
134	12 710	12 743	12 775	12 808	12 840	12 872	12 905	12 937	12 969	13 001
135	13 033	13 066	13 098	13 130	13 162	13 194	13 226	13 258	13 290	13 322
136	13 354	13 386	13 418	13 450	13 481	13 513	13 545	13 577	13 609	13 640
137	13 672	13 704	13 735	13 767	13 799	13 830	13 862	13 893	13 925	13 956
138	13 988	14 019	14 051	14 082	14 114	14 145	14 176	14 208	14 239	14 270
139	14 301	14 333	14 364	14 395	14 426	14 457	14 489	14 520	14 551	14 582
140	14 613	14 644	14 675	14 706	14 737	14 768	14 799	14 829	14 860	14 891
141	14 922	14 953	14 983	15 014	15 045	15 076	15 106	15 137	15 168	15 198
142	15 229	15 259	15 290	15 320	15 351	15 381	15 412	15 442	15 473	15 503
143	15 534	15 564	15 594	15 625	15 655	15 685	15 715	15 746	15 776	15 806
144	15 836	15 866	15 897	15 927	15 957	15 987	16 017	16 047	16 077	16 107
145	16 137	16 167	16 197	16 227	16 256	16 286	16 316	16 346	16 376	16 406
146	16 435	16 465	16 495	16 524	16 554	16 584	16 613	16 643	16 673	16 702
147	16 732	16 761	16 791	16 820	16 850	16 879	16 909	16 938	16 967	16 997
148	17 026	17 056	17 085	17 114	17 143	17 173	17 202	17 231	17 260	17 289
149	17 319	17 348	17 377	17 406	17 435	17 464	17 493	17 522	17 551	17 580
150	17 609	17 638	17 667	17 696	17 725	17 754	17 782	17 811	17 840	17 869
N	0	1	2	3	4	5	6	7	8	9

N	0	1	2	3	4	5	6	7	8	9
150	17 609	17 638	17 667	17 696	17 725	17 754	17 782	17 811	17 840	17 869
151	17 898	17 926	17 955	17 984	18 013	18 041	18 070	18 099	18 127	18 156
152	18 184	18 213	18 241	18 270	18 298	18 327	18 355	18 384	18 412	18 441
153	18 469	18 498	18 526	18 554	18 583	18 611	18 639	18 667	18 696	18 724
154	18 752	18 780	18 808	18 837	18 865	18 893	18 921	18 949	18 977	19 005
155	19 033	19 061	19 089	19 117	19 145	19 173	19 201	19 229	19 257	19 285
156	19 312	19 340	19 368	19 396	19 424	19 451	19 479	19 507	19 535	19 562
157	19 590	19 618	19 645	19 673	19 700	19 728	19 756	19 783	19 811	19 838
158	19 866	19 893	19 921	19 948	19 976	20 003	20 030	20 058	20 085	20 112
159	20 140	20 167	20 194	20 222	20 249	20 276	20 303	20 330	20 358	20 385
160	20 412	20 439	20 466	20 493	20 520	20 548	20 575	20 602	20 629	20 656
161	20 683	20 710	20 737	20 763	20 790	20 817	20 844	20 871	20 898	20 925
162	20 952	20 978	21 005	21 032	21 059	21 085	21 112	21 139	21 165	21 192
163	21 219	21 245	21 272	21 299	21 325	21 352	21 378	21 405	21 431	21 458
164	21 484	21 511	21 537	21 564	21 590	21 617	21 643	21 669	21 696	21 722
165	21 748	21 775	21 801	21 827	21 854	21 880	21 906	21 932	21 958	21 985
166	22 011	22 037	22 063	22 089	22 115	22 141	22 167	22 194	22 220	22 246
167	22 272	22 298	22 324	22 350	22 376	22 401	22 427	22 453	22 479	22 505
168	22 531	22 557	22 583	22 608	22 634	22 660	22 686	22 712	22 737	22 763
169	22 789	22 814	22 840	22 866	22 891	22 917	22 943	22 968	22 994	23 019
170	23 045	23 070	23 096	23 121	23 147	23 172	23 198	23 223	23 249	23 274
171	23 300	23 325	23 350	23 376	23 401	23 426	23 452	23 477	23 502	23 528
172	23 553	23 578	23 603	23 629	23 654	23 679	23 704	23 729	23 754	23 779
173	23 805	23 830	23 855	23 880	23 905	23 930	23 955	23 980	24 005	24 030
174	24 055	24 080	24 105	24 130	24 155	24 180	24 204	24 229	24 254	24 279
175	24 304	24 329	24 353	24 378	24 403	24 428	24 452	24 477	24 502	24 527
176	24 551	24 576	24 601	24 625	24 650	24 674	24 699	24 724	24 748	24 773
177	24 797	24 822	24 846	24 871	24 895	24 920	24 944	24 969	24 993	25 018
178	25 042	25 066	25 091	25 115	25 139	25 164	25 188	25 212	25 237	25 261
179	25 285	25 310	25 334	25 358	25 382	25 406	25 431	25 455	25 479	25 503
180	25 527	25 551	25 575	25 600	25 624	25 648	25 672	25 696	25 720	25 744
181	25 768	25 792	25 816	25 840	25 864	25 888	25 912	25 935	25 959	25 983
182	26 007	26 031	26 055	26 079	26 102	26 126	26 150	26 174	26 198	26 221
183	26 245	26 269	26 293	26 316	26 340	26 364	26 387	26 411	26 435	26 458
184	26 482	26 505	26 529	26 553	26 576	26 600	26 623	26 647	26 670	26 694
185	26 717	26 741	26 764	26 788	26 811	26 834	26 858	26 881	26 905	26 928
186	26 951	26 975	26 998	27 021	27 045	27 068	27 091	27 114	27 138	27 161
187	27 184	27 207	27 231	27 254	27 277	27 300	27 323	27 346	27 370	27 393
188	27 416	27 439	27 462	27 485	27 508	27 531	27 554	27 577	27 600	27 623
189	27 646	27 669	27 692	27 715	27 738	27 761	27 784	27 807	27 830	27 852
190	27 875	27 898	27 921	27 944	27 967	27 989	28 012	28 035	28 058	28 081
191	28 103	28 126	28 149	28 171	28 194	28 217	28 240	28 262	28 285	28 307
192	28 330	28 353	28 375	28 398	28 421	28 443	28 466	28 488	28 511	28 533
193	28 556	28 578	28 601	28 623	28 646	28 668	28 691	28 713	28 735	28 758
194	28 780	28 803	28 825	28 847	28 870	28 892	28 914	28 937	28 959	28 981
195	29 003	29 026	29 048	29 070	29 092	29 115	29 137	29 159	29 181	29 203
196	29 226	29 248	29 270	29 292	29 314	29 336	29 358	29 380	29 403	29 425
197	29 447	29 469	29 491	29 513	29 535	29 557	29 579	29 601	29 623	29 645
198	29 667	29 688	29 710	29 732	29 754	29 776	29 798	29 820	29 842	29 863
199	29 885	29 907	29 929	29 951	29 973	29 994	30 016	30 038	30 060	30 081
200	30 103	30 125	30 146	30 168	30 190	30 211	30 233	30 255	30 276	30 298
N	0	1	2	3	4	5	6	7	8	9

200—250

N	0	1	2	3	4	5	6	7	8	9
200	30 103	30 125	30 146	30 168	30 190	30 211	30 233	30 255	30 276	30 298
201	30 320	30 341	30 363	30 384	30 406	30 428	30 449	30 471	30 492	30 514
202	30 535	30 557	30 578	30 600	30 621	30 643	30 664	30 685	30 707	30 728
203	30 750	30 771	30 792	30 814	30 835	30 856	30 878	30 899	30 920	30 942
204	30 963	30 984	31 006	31 027	31 048	31 069	31 091	31 112	31 133	31 154
205	31 175	31 197	31 218	31 239	31 260	31 281	31 302	31 323	31 345	31 366
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417	62 014	62 024	62 034	62 045	62 055	62 066	62 076	62 086	62 097	62 107
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422	62 531	62 542	62 552	62 562	62 572	62 583	62 593	62 603	62 613	62 624
423	62 634	62 644	62 655	62 665	62 675	62 685	62 696	62 706	62 716	62 726
424	62 737	62 747	62 757	62 767	62 778	62 788	62 798	62 808	62 818	62 829
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503	70 157	70 165	70 174	70 183	70 191	70 200	70 209	70 217	70 226	70 234
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516	71 265̲	71 273	71 282	71 290	71 299	71 307	71 315	71 324	71 332	71 341
517	71 349	71 357	71 366	71 374	71 383	71 391	71 399	71 408	71 416	71 425̲
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524	71 933	71 941	71 95̲0	71 958	71 966	71 975̲	71 983	71 991	71 999	72 008
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547	73 799	73 807	73 815̲	73 823	73 830	73 838	73 846	73 854	73 862	73 870
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575	75 967	75 974	75 982	75 989	75 997	76 005̲	76 012	76 020	76 027	76 035̲
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593	77 305	77 313	77 320	77 327	77 335̲	77 342	77 349	77 357	77 364	77 371
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612	78 675	78 682	78 689	78 696	78 704	78 711	78 718	78 725̲	78 732	78 739
613	78 746	78 753	78 760	78 767	78 774	78 781	78 789	78 796	78 803	78 810
614	78 817	78 824	78 831	78 838	78 845	78 852	78 859	78 866	78 873	78 880
615	78 888	78 895̲	78 902	78 909	78 916	78 923	78 930	78 937	78 944	78 951
616	78 958	78 965	78 972	78 979	78 986	78 993	79 000	79 007	79 014	79 021
617	79 029	79 036	79 043	79 05̲0	79 057	79 064	79 071	79 078	79 085̲	79 092
618	79 099	79 106	79 113	79 120	79 127	79 134	79 141	79 148	79 155	79 162
619	79 169	79 176	79 183	79 190	79 197	79 204	79 211	79 218	79 225	79 232
620	79 239	79 246	79 253	79 260	79 267	79 274	79 281	79 288	79 295	79 302
621	79 309	79 316	79 323	79 330	79 337	79 344	79 351	79 358	79 365	79 372
622	79 379	79 386	79 393	79 400	79 407	79 414	79 421	79 428	79 435̲	79 442
623	79 449	79 456	79 463	79 470	79 477	79 484	79 491	79 498	79 505̲	79 511
624	79 518	79 525	79 532	79 539	79 546	79 553	79 560	79 567	79 574	79 581
625	79 588	79 595̲	79 602	79 609	79 616	79 623	79 630	79 637	79 644	79 650
626	79 657	79 664	79 671	79 678	79 685	79 692	79 699	79 706	79 713	79 720
627	79 727	79 734	79 741	79 748	79 754	79 761	79 768	79 775	79 782	79 789
628	79 796	79 803	79 810	79 817	79 824	79 831	79 837	79 844	79 851	79 858
629	79 865	79 872	79 879	79 886	79 893	79 900	79 906	79 913	79 920	79 927
630	79 934	79 941	79 948	79 955̲	79 962	79 969	79 975	79 982	79 989	79 996
631	80 003	80 010	80 017	80 024	80 030	80 037	80 044	80 051	80 058	80 065̲
632	80 072	80 079	80 085	80 092	80 099	80 106	80 113	80 120	80 127	80 134
633	80 140	80 147	80 154	80 161	80 168	80 175̲	80 182	80 188	80 195	80 202
634	80 209	80 216	80 223	80 229	80 236	80 243	80 250	80 257	80 264	80 271
635	80 277	80 284	80 291	80 298	80 305̲	80 312	80 318	80 325	80 332	80 339
636	80 346	80 353	80 359	80 366	80 373	80 380	80 387	80 393	80 400	80 407
637	80 414	80 421	80 428	80 434	80 441	80 448	80 455̲	80 462	80 468	80 475
638	80 482	80 489	80 496	80 502	80 509	80 516	80 523	80 530	80 536	80 543
639	80 550	80 557	80 564	80 570	80 577	80 584	80 591	80 598	80 604	80 611
640	80 618	80 625̲	80 632	80 638	80 645	80 652	80 659	80 665	80 672	80 679
641	80 686	80 693	80 699	80 706	80 713	80 720	80 726	80 733	80 740	80 747
642	80 754	80 760	80 767	80 774	80 781	80 787	80 794	80 801	80 808	80 814
643	80 821	80 828	80 835̲	80 841	80 848	80 855̲	80 862	80 868	80 875	80 882
644	80 889	80 895	80 902	80 909	80 916	80 922	80 929	80 936	80 943	80 949
645	80 956	80 963	80 969	80 976	80 983	80 990	80 996	81 003	81 010	81 017
646	81 023	81 030	81 037	81 043	81 050	81 057	81 064	81 070	81 077	81 084
647	81 090	81 097	81 104	81 111	81 117	81 124	81 131	81 137	81 144	81 151
648	81 158	81 164	81 171	81 178	81 184	81 191	81 198	81 204	81 211	81 218
649	81 224	81 231	81 238	81 245̲	81 251	81 258	81 265̲	81 271	81 278	81 285̲
650	81 291	81 298	81 305̲	81 311	81 318	81 325̲	81 331	81 338	81 345̲	81 351
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650	81 291	81 298	81 305	81 311	81 318	81 325	81 331	81 338	81 345	81 351
651	81 358	81 365	81 371	81 378	81 385	81 391	81 398	81 405	81 411	81 418
652	81 425	81 431	81 438	81 445	81 451	81 458	81 465	81 471	81 478	81 485
653	81 491	81 498	81 505	81 511	81 518	81 525	81 531	81 538	81 544	81 551
654	81 558	81 564	81 571	81 578	81 584	81 591	81 598	81 604	81 611	81 617
655	81 624	81 631	81 637	81 644	81 651	81 657	81 664	81 671	81 677	81 684
656	81 690	81 697	81 704	81 710	81 717	81 723	81 730	81 737	81 743	81 750
657	81 757	81 763	81 770	81 776	81 783	81 790	81 796	81 803	81 809	81 816
658	81 823	81 829	81 836	81 842	81 849	81 856	81 862	81 869	81 875	81 882
659	81 889	81 895	81 902	81 908	81 915	81 921	81 928	81 935	81 941	81 948
660	81 954	81 961	81 968	81 974	81 981	81 987	81 994	82 000	82 007	82 014
661	82 020	82 027	82 033	82 040	82 046	82 053	82 060	82 066	82 073	82 079
662	82 086	82 092	82 099	82 105	82 112	82 119	82 125	82 132	82 138	82 145
663	82 151	82 158	82 164	82 171	82 178	82 184	82 191	82 197	82 204	82 210
664	82 217	82 223	82 230	82 236	82 243	82 249	82 256	82 263	82 269	82 276
665	82 282	82 289	82 295	82 302	82 308	82 315	82 321	82 328	82 334	82 341
666	82 347	82 354	82 360	82 367	82 373	82 380	82 387	82 393	82 400	82 406
667	82 413	82 419	82 426	82 432	82 439	82 445	82 452	82 458	82 465	82 471
668	82 478	82 484	82 491	82 497	82 504	82 510	82 517	82 523	82 530	82 536
669	82 543	82 549	82 556	82 562	82 569	82 575	82 582	82 588	82 595	82 601
670	82 607	82 614	82 620	82 627	82 633	82 640	82 646	82 653	82 659	82 666
671	82 672	82 679	82 685	82 692	82 698	82 705	82 711	82 718	82 724	82 730
672	82 737	82 743	82 750	82 756	82 763	82 769	82 776	82 782	82 789	82 795
673	82 802	82 808	82 814	82 821	82 827	82 834	82 840	82 847	82 853	82 860
674	82 866	82 872	82 879	82 885	82 892	82 898	82 905	82 911	82 918	82 924
675	82 930	82 937	82 943	82 950	82 956	82 963	82 969	82 975	82 982	82 988
676	82 995	83 001	83 008	83 014	83 020	83 027	83 033	83 040	83 046	83 052
677	83 059	83 065	83 072	83 078	83 085	83 091	83 097	83 104	83 110	83 117
678	83 123	83 129	83 136	83 142	83 149	83 155	83 161	83 168	83 174	83 181
679	83 187	83 193	83 200	83 206	83 213	83 219	83 225	83 232	83 238	83 245
680	83 251	83 257	83 264	83 270	83 276	83 283	83 289	83 296	83 302	83 308
681	83 315	83 321	83 327	83 334	83 340	83 347	83 353	83 359	83 366	83 372
682	83 378	83 385	83 391	83 398	83 404	83 410	83 417	83 423	83 429	83 436
683	83 442	83 448	83 455	83 461	83 467	83 474	83 480	83 487	83 493	83 499
684	83 506	83 512	83 518	83 525	83 531	83 537	83 544	83 550	83 556	83 563
685	83 569	83 575	83 582	83 588	83 594	83 601	83 607	83 613	83 620	83 626
686	83 632	83 639	83 645	83 651	83 658	83 664	83 670	83 677	83 683	83 689
687	83 696	83 702	83 708	83 715	83 721	83 727	83 734	83 740	83 746	83 753
688	83 759	83 765	83 771	83 778	83 784	83 790	83 797	83 803	83 809	83 816
689	83 822	83 828	83 835	83 841	83 847	83 853	83 860	83 866	83 872	83 879
690	83 885	83 891	83 897	83 904	83 910	83 916	83 923	83 929	83 935	83 942
691	83 948	83 954	83 960	83 967	83 973	83 979	83 985	83 992	83 998	84 004
692	84 011	84 017	84 023	84 029	84 036	84 042	84 048	84 055	84 061	84 067
693	84 073	84 080	84 086	84 092	84 098	84 105	84 111	84 117	84 123	84 130
694	84 136	84 142	84 148	84 155	84 161	84 167	84 173	84 180	84 186	84 192
695	84 198	84 205	84 211	84 217	84 223	84 230	84 236	84 242	84 248	84 255
696	84 261	84 267	84 273	84 280	84 286	84 292	84 298	84 305	84 311	84 317
697	84 323	84 330	84 336	84 342	84 348	84 354	84 361	84 367	84 373	84 379
698	84 386	84 392	84 398	84 404	84 410	84 417	84 423	84 429	84 435	84 442
699	84 448	84 454	84 460	84 466	84 473	84 479	84 485	84 491	84 497	84 504
700	84 510	84 516	84 522	84 528	84 535	84 541	84 547	84 553	84 559	84 566
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700—750

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700	84 510	84 516	84 522	84 528	84 535	84 541	84 547	84 553	84 559	84 566
701	84 572	84 578	84 584	84 590	84 597	84 603	84 609	84 615	84 621	84 628
702	84 634	84 640	84 646	84 652	84 658	84 665	84 671	84 677	84 683	84 689
703	84 696	84 702	84 708	84 714	84 720	84 726	84 733	84 739	84 745	84 751
704	84 757	84 763	84 770	84 776	84 782	84 788	84 794	84 800	84 807	84 813
705	84 819	84 825	84 831	84 837	84 844	84 850	84 856	84 862	84 868	84 874
706	84 880	84 887	84 893	84 899	84 905	84 911	84 917	84 924	84 930	84 936
707	84 942	84 948	84 954	84 960	84 967	84 973	84 979	84 985	84 991	84 997
708	85 003	85 009	85 016	85 022	85 028	85 034	85 040	85 046	85 052	85 058
709	85 065	85 071	85 077	85 083	85 089	85 095	85 101	85 107	85 114	85 120
710	85 126	85 132	85 138	85 144	85 150	85 156	85 163	85 169	85 175	85 181
711	85 187	85 193	85 199	85 205	85 211	85 217	85 224	85 230	85 236	85 242
712	85 248	85 254	85 260	85 266	85 272	85 278	85 285	85 291	85 297	85 303
713	85 309	85 315	85 321	85 327	85 333	85 339	85 345	85 352	85 358	85 364
714	85 370	85 376	85 382	85 388	85 394	85 400	85 406	85 412	85 418	85 425
715	85 431	85 437	85 443	85 449	85 455	85 461	85 467	85 473	85 479	85 485
716	85 491	85 497	85 503	85 509	85 516	85 522	85 528	85 534	85 540	85 546
717	85 552	85 558	85 564	85 570	85 576	85 582	85 588	85 594	85 600	85 606
718	85 612	85 618	85 625	85 631	85 637	85 643	85 649	85 655	85 661	85 667
719	85 673	85 679	85 685	85 691	85 697	85 703	85 709	85 715	85 721	85 727
720	85 733	85 739	85 745	85 751	85 757	85 763	85 769	85 775	85 781	85 788
721	85 794	85 800	85 806	85 812	85 818	85 824	85 830	85 836	85 842	85 848
722	85 854	85 860	85 866	85 872	85 878	85 884	85 890	85 896	85 902	85 908
723	85 914	85 920	85 926	85 932	85 938	85 944	85 950	85 956	85 962	85 968
724	85 974	85 980	85 986	85 992	85 998	86 004	86 010	86 016	86 022	86 028
725	86 034	86 040	86 046	86 052	86 058	86 064	86 070	86 076	86 082	86 088
726	86 094	86 100	86 106	86 112	86 118	86 124	86 130	86 136	86 141	86 147
727	86 153	86 159	86 165	86 171	86 177	86 183	86 189	86 195	86 201	86 207
728	86 213	86 219	86 225	86 231	86 237	86 243	86 249	86 255	86 261	86 267
729	86 273	86 279	86 285	86 291	86 297	86 303	86 308	86 314	86 320	86 326
730	86 332	86 338	86 344	86 350	86 356	86 362	86 368	86 374	86 380	86 386
731	86 392	86 398	86 404	86 410	86 415	86 421	86 427	86 433	86 439	86 445
732	86 451	86 457	86 463	86 469	86 475	86 481	86 487	86 493	86 499	86 504
733	86 510	86 516	86 522	86 528	86 534	86 540	86 546	86 552	86 558	86 564
734	86 570	86 576	86 581	86 587	86 593	86 599	86 605	86 611	86 617	86 623
735	86 629	86 635	86 641	86 646	86 652	86 658	86 664	86 670	86 676	86 682
736	86 688	86 694	86 700	86 705	86 711	86 717	86 723	86 729	86 735	86 741
737	86 747	86 753	86 759	86 764	86 770	86 776	86 782	86 788	86 794	86 800
738	86 806	86 812	86 817	86 823	86 829	86 835	86 841	86 847	86 853	86 859
739	86 864	86 870	86 876	86 882	86 888	86 894	86 900	86 906	86 911	86 917
740	86 923	86 929	86 935	86 941	86 947	86 953	86 958	86 964	86 970	86 976
741	86 982	86 988	86 994	86 999	87 005	87 011	87 017	87 023	87 029	87 035
742	87 040	87 046	87 052	87 058	87 064	87 070	87 075	87 081	87 087	87 093
743	87 099	87 105	87 111	87 116	87 122	87 128	87 134	87 140	87 146	87 151
744	87 157	87 163	87 169	87 175	87 181	87 186	87 192	87 198	87 204	87 210
745	87 216	87 221	87 227	87 233	87 239	87 245	87 251	87 256	87 262	87 268
746	87 274	87 280	87 286	87 291	87 297	87 303	87 309	87 315	87 320	87 326
747	87 332	87 338	87 344	87 349	87 355	87 361	87 367	87 373	87 379	87 384
748	87 390	87 396	87 402	87 408	87 413	87 419	87 425	87 431	87 437	87 442
749	87 448	87 454	87 460	87 466	87 471	87 477	87 483	87 489	87 495	87 500
750	87 506	87 512	87 518	87 523	87 529	87 535	87 541	87 547	87 552	87 558
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750	87 506	87 512	87 518	87 523	87 529	87 535	87 541	87 547	87 552	87 558
751	87 564	87 570	87 576	87 581	87 587	87 593	87 599	87 604	87 610	87 616
752	87 622	87 628	87 633	87 639	87 645	87 651	87 656	87 662	87 668	87 674
753	87 679	87 685	87 691	87 697	87 703	87 708	87 714	87 720	87 726	87 731
754	87 737	87 743	87 749	87 754	87 760	87 766	87 772	87 777	87 783	87 789
755	87 795	87 800	87 806	87 812	87 818	87 823	87 829	87 835	87 841	87 846
756	87 852	87 858	87 864	87 869	87 875	87 881	87 887	87 892	87 898	87 904
757	87 910	87 915	87 921	87 927	87 933	87 938	87 944	87 950	87 955	87 961
758	87 967	87 973	87 978	87 984	87 990	87 996	88 001	88 007	88 013	88 018
759	88 024	88 030	88 036	88 041	88 047	88 053	88 058	88 064	88 070	88 076
760	88 081	88 087	88 093	88 098	88 104	88 110	88 116	88 121	88 127	88 133
761	88 138	88 144	88 150	88 156	88 161	88 167	88 173	88 178	88 184	88 190
762	88 195	88 201	88 207	88 213	88 218	88 224	88 230	88 235	88 241	88 247
763	88 252	88 258	88 264	88 270	88 275	88 281	88 287	88 292	88 298	88 304
764	88 309	88 315	88 321	88 326	88 332	88 338	88 343	88 349	88 355	88 360
765	88 366	88 372	88 377	88 383	88 389	88 395	88 400	88 406	88 412	88 417
766	88 423	88 429	88 434	88 440	88 446	88 451	88 457	88 463	88 468	88 474
767	88 480	88 485	88 491	88 497	88 502	88 508	88 513	88 519	88 525	88 530
768	88 536	88 542	88 547	88 553	88 559	88 564	88 570	88 576	88 581	88 587
769	88 593	88 598	88 604	88 610	88 615	88 621	88 627	88 632	88 638	88 643
770	88 649	88 655	88 660	88 666	88 672	88 677	88 683	88 689	88 694	88 700
771	88 705	88 711	88 717	88 722	88 728	88 734	88 739	88 745	88 750	88 756
772	88 762	88 767	88 773	88 779	88 784	88 790	88 795	88 801	88 807	88 812
773	88 818	88 824	88 829	88 835	88 840	88 846	88 852	88 857	88 863	88 868
774	88 874	88 880	88 885	88 891	88 897	88 902	88 908	88 913	88 919	88 925
775	88 930	88 936	88 941	88 947	88 953	88 958	88 964	88 969	88 975	88 981
776	88 986	88 992	88 997	89 003	89 009	89 014	89 020	89 025	89 031	89 037
777	89 042	89 048	89 053	89 059	89 064	89 070	89 076	89 081	89 087	89 092
778	89 098	89 104	89 109	89 115	89 120	89 126	89 131	89 137	89 143	89 148
779	89 154	89 159	89 165	89 170	89 176	89 182	89 187	89 193	89 198	89 204
780	89 209	89 215	89 221	89 226	89 232	89 237	89 243	89 248	89 254	89 260
781	89 265	89 271	89 276	89 282	89 287	89 293	89 298	89 304	89 310	89 315
782	89 321	89 326	89 332	89 337	89 343	89 348	89 354	89 360	89 365	89 371
783	89 376	89 382	89 387	89 393	89 398	89 404	89 409	89 415	89 421	89 426
784	89 432	89 437	89 443	89 448	89 454	89 459	89 465	89 470	89 476	89 481
785	89 487	89 492	89 498	89 504	89 509	89 515	89 520	89 526	89 531	89 537
786	89 542	89 548	89 553	89 559	89 564	89 570	89 575	89 581	89 586	89 592
787	89 597	89 603	89 609	89 614	89 620	89 625	89 631	89 636	89 642	89 647
788	89 653	89 658	89 664	89 669	89 675	89 680	89 686	89 691	89 697	89 702
789	89 708	89 713	89 719	89 724	89 730	89 735	89 741	89 746	89 752	89 757
790	89 763	89 768	89 774	89 779	89 785	89 790	89 796	89 801	89 807	89 812
791	89 818	89 823	89 829	89 834	89 840	89 845	89 851	89 856	89 862	89 867
792	89 873	89 878	89 883	89 889	89 894	89 900	89 905	89 911	89 916	89 922
793	89 927	89 933	89 938	89 944	89 949	89 955	89 960	89 966	89 971	89 977
794	89 982	89 988	89 993	89 998	90 004	90 009	90 015	90 020	90 026	90 031
795	90 037	90 042	90 048	90 053	90 059	90 064	90 069	90 075	90 080	90 086
796	90 091	90 097	90 102	90 108	90 113	90 119	90 124	90 129	90 135	90 140
797	90 146	90 151	90 157	90 162	90 168	90 173	90 179	90 184	90 189	90 195
798	90 200	90 206	90 211	90 217	90 222	90 227	90 233	90 238	90 244	90 249
799	90 255	90 260	90 266	90 271	90 276	90 282	90 287	90 293	90 298	90 304
800	90 309	90 314	90 320	90 325	90 331	90 336	90 342	90 347	90 352	90 358
N	0	1	2	3	4	5	6	7	8	9

N	0	1	2	3	4	5	6	7	8	9
800	90 309	90 314	90 320	90 325	90 331	90 336	90 342	90 347	90 352	90 358
801	90 363	90 369	90 374	90 380	90 385	90 390	90 396	90 401	90 407	90 412
802	90 417	90 423	90 428	90 434	90 439	90 445	90 450	90 455	90 461	90 466
803	90 472	90 477	90 482	90 488	90 493	90 499	90 504	90 509	90 515	90 520
804	90 526	90 531	90 536	80 542	90 547	90 553	90 558	90 563	90 569	90 574
805	90 580	90 585	90 590	90 596	90 601	90 607	90 612	90 617	90 623	90 628
806	90 634	90 639	90 644	90 650	90 655	90 660	90 666	90 671	90 677	90 682
807	90 687	90 693	90 698	90 703	90 709	90 714	90 720	90 725	90 730	90 736
808	90 741	90 747	90 752	90 757	90 763	90 768	90 773	90 779	90 784	90 789
809	90 795	90 800	90 806	90 811	90 816	90 822	90 827	90 832	90 838	90 843
810	90 849	90 854	90 859	90 865	90 870	90 875	90 881	90 886	90 891	90 897
811	90 902	90 907	90 913	90 918	90 924	90 929	90 934	90 940	90 945	90 950
812	90 956	90 961	90 966	90 972	90 977	90 982	90 988	90 993	90 998	91 004
813	91 009	91 014	91 020	91 025	91 030	91 036	91 041	91 046	91 052	91 057
814	91 062	91 068	91 073	91 078	91 084	91 089	91 094	91 100	91 105	91 110
815	91 116	91 121	91 126	91 132	91 137	91 142	91 148	91 153	91 158	91 164
816	91 169	91 174	91 180	91 185	91 190	91 196	91 201	91 206	91 212	91 217
817	91 222	91 228	91 233	91 238	91 243	91 249	91 254	91 259	91 265	91 270
818	91 275	91 281	91 286	91 291	91 297	91 302	91 307	91 312	91 318	91 323
819	91 328	91 334	91 339	91 344	91 350	91 355	91 360	91 365	91 371	91 376
820	91 381	91 387	91 392	91 397	91 403	91 408	91 413	91 418	91 424	91 429
821	91 434	91 440	91 445	91 450	91 455	91 461	91 466	91 471	91 477	91 482
822	91 487	91 492	91 498	91 503	91 508	91 514	91 519	91 524	91 529	91 535
823	91 540	91 545	91 551	91 556	91 561	91 566	91 572	91 577	91 582	91 587
824	91 593	91 598	91 603	91 609	91 614	91 619	91 624	91 630	91 635	91 640
825	91 645	91 651	91 656	91 661	91 666	91 672	91 677	91 682	91 687	91 693
826	91 698	91 703	91 709	91 714	91 719	91 724	91 730	91 735	91 740	91 745
827	91 751	91 756	91 761	91 766	91 772	91 777	91 782	91 787	91 793	91 798
828	91 803	91 808	91 814	91 819	91 824	91 829	91 834	91 840	91 845	91 850
829	91 855	91 861	91 866	91 871	91 876	91 882	91 887	91 892	91 897	91 903
830	91 908	91 913	91 918	91 924	91 929	91 934	91 939	91 944	91 950	91 955
831	91 960	91 965	91 971	91 976	91 981	91 986	91 991	91 997	92 002	92 007
832	92 012	92 018	92 023	92 028	92 033	92 038	92 044	92 049	92 054	92 059
833	92 065	92 070	92 075	92 080	92 085	92 091	92 096	92 101	92 106	92 111
834	92 117	92 122	92 127	92 132	92 137	92 143	92 148	92 153	92 158	92 163
835	92 169	92 174	92 179	92 184	92 189	92 195	92 200	92 205	92 210	92 215
836	92 221	92 226	92 231	92 236	92 241	92 247	92 252	92 257	92 262	92 267
837	92 273	92 278	92 283	92 288	92 293	92 298	92 304	92 309	92 314	92 319
838	92 324	92 330	92 335	92 340	92 345	92 350	92 355	92 361	92 366	92 371
839	92 376	92 381	92 387	92 392	92 397	92 402	92 407	92 412	92 418	92 423
840	92 428	92 433	92 438	92 443	92 449	92 454	92 459	92 464	92 469	92 474
841	92 480	92 485	92 490	92 495	92 500	92 505	92 511	92 516	92 521	92 526
842	92 531	92 536	92 542	92 547	92 552	92 557	92 562	92 567	92 572	92 578
843	92 583	92 588	92 593	92 598	92 603	92 609	92 614	92 619	92 624	92 629
844	92 634	92 639	92 645	92 650	92 655	92 660	92 665	92 670	92 675	92 681
845	92 686	92 691	92 696	92 701	92 706	92 711	92 716	92 722	92 727	92 732
846	92 737	92 742	92 747	92 752	92 758	92 763	92 768	92 773	92 778	92 783
847	92 788	92 793	92 799	92 804	92 809	92 814	92 819	92 824	92 829	92 834
848	92 840	92 845	92 850	92 855	92 860	92 865	92 870	92 875	92 881	92 886
849	92 891	92 896	92 901	92 906	92 911	92 916	92 921	92 927	92 932	92 937
850	92 942	92 947	92 952	92 957	92 962	92 967	92 973	92 978	92 983	92 988
N	0	1	2	3	4	5	6	7	8	9

N	0	1	2	3	4	5	6	7	8	9
850	92 942	92 947	92 952	92 957	92 962	92 967	92 973	92 978	92 983	92 988
851	92 993	92 998	93 003	93 008	93 013	93 018	93 024	93 029	93 034	93 039
852	93 044	93 049	93 054	93 059	93 064	93 069	93 075	93 080	93 085	93 090
853	93 095	93 100	93 105	93 110	93 115	93 120	93 125	93 131	93 136	93 141
854	93 146	93 151	93 156	93 161	93 166	93 171	93 176	93 181	93 186	93 192
855	93 197	93 202	93 207	93 212	93 217	93 222	93 227	93 232	93 237	93 242
856	93 247	93 252	93 258	93 263	93 268	93 273	93 278	93 283	93 288	93 293
857	93 298	93 303	93 308	93 313	93 318	93 323	93 328	93 334	93 339	93 344
858	93 349	93 354	93 359	93 364	93 369	93 374	93 379	93 384	93 389	93 394
859	93 399	93 404	93 409	93 414	93 420	93 425	93 430	93 435	93 440	93 445
860	93 450	93 455	93 460	93 465	93 470	93 475	93 480	93 485	93 490	93 495
861	93 500	93 505	93 510	93 515	93 520	93 526	93 531	93 536	93 541	93 546
862	93 551	93 556	93 561	93 566	93 571	93 576	93 581	93 586	93 591	93 596
863	93 601	93 606	93 611	93 616	93 621	93 626	93 631	93 636	93 641	93 646
864	93 651	93 656	93 661	93 666	93 671	93 676	93 682	93 687	93 692	93 697
865	93 702	93 707	93 712	93 717	93 722	93 727	93 732	93 737	93 742	93 747
866	93 752	93 757	93 762	93 767	93 772	93 777	93 782	93 787	93 792	93 797
867	93 802	93 807	93 812	93 817	93 822	93 827	93 832	93 837	93 842	93 847
868	93 852	93 857	93 862	93 867	93 872	93 877	93 882	93 887	93 892	93 897
869	93 902	93 907	93 912	93 917	93 922	93 927	93 932	93 937	93 942	93 947
870	93 952	93 957	93 962	93 967	93 972	93 977	93 982	93 987	93 992	93 997
871	94 002	94 007	94 012	94 017	94 022	94 027	94 032	94 037	94 042	94 047
872	94 052	94 057	94 062	94 067	94 072	94 077	94 082	94 086	94 091	94 096
873	94 101	94 106	94 111	94 116	94 121	94 126	94 131	94 136	94 141	94 146
874	94 151	94 156	94 161	94 166	94 171	94 176	94 181	94 186	94 191	94 196
875	94 201	94 206	94 211	94 216	94 221	94 226	94 231	94 236	94 240	94 245
876	94 250	94 255	94 260	94 265	94 270	94 275	94 280	94 285	94 290	94 295
877	94 300	94 305	94 310	94 315	94 320	94 325	94 330	94 335	94 340	94 345
878	94 349	94 354	94 359	94 364	94 369	94 374	94 379	94 384	94 389	94 394
879	94 399	94 404	94 409	94 414	94 419	94 424	94 429	94 433	94 438	94 443
880	94 448	94 453	94 458	94 463	94 468	94 473	94 478	94 483	94 488	94 493
881	94 498	94 503	94 507	94 512	94 517	94 522	94 527	94 532	94 537	94 542
882	94 547	94 552	94 557	94 562	94 567	94 571	94 576	94 581	94 586	94 591
883	94 596	94 601	94 606	94 611	94 616	94 621	94 626	94 630	94 635	94 640
884	94 645	94 650	94 655	94 660	94 665	94 670	94 675	94 680	94 685	94 689
885	94 694	94 699	94 704	94 709	94 714	94 719	94 724	94 729	94 734	94 738
886	94 743	94 748	94 753	94 758	94 763	94 768	94 773	94 778	94 783	94 787
887	94 792	94 797	94 802	94 807	94 812	94 817	94 822	94 827	94 832	94 836
888	94 841	94 846	94 851	94 856	94 861	94 866	94 871	94 876	94 880	94 885
889	94 890	94 895	94 900	94 905	94 910	94 915	94 919	94 924	94 929	94 934
890	94 939	94 944	94 949	94 954	94 959	94 963	94 968	94 973	94 978	94 983
891	94 988	94 993	94 998	95 002	95 007	95 012	95 017	95 022	95 027	95 032
892	95 036	95 041	95 046	95 051	95 056	95 061	95 066	95 071	95 075	95 080
893	95 085	95 090	95 095	95 100	95 105	95 109	95 114	95 119	95 124	95 129
894	95 134	95 139	95 143	95 148	95 153	95 158	95 163	95 168	95 173	95 177
895	95 182	95 187	95 192	95 197	95 202	95 207	95 211	95 216	95 221	95 226
896	95 231	95 236	95 240	95 245	95 250	95 255	95 260	95 265	95 270	95 274
897	95 279	95 284	95 289	95 294	95 299	95 303	95 308	95 313	95 318	95 323
898	95 328	95 332	95 337	95 342	95 347	95 352	95 357	95 361	95 366	95 371
899	95 376	95 381	95 386	95 390	95 395	95 400	95 405	95 410	95 415	95 419
900	95 424	95 429	95 434	95 439	95 444	95 448	95 453	95 458	95 463	95 468
N	0	1	2	3	4	5	6	7	8	9

N	0	1	2	3	4	5	6	7	8	9
900	95 424	95 429	95 434	95 439	95 444	95 448	95 453	95 458	95 463	95 468
901	95 472	95 477	95 482	95 487	95 492	95 497	95 501	95 506	95 511	95 516
902	95 521	95 525	95 530	95 535	95 540	95 545	95 550	95 554	95 559	95 564
903	95 569	95 574	95 578	95 583	95 588	95 593	95 598	95 602	95 607	95 612
904	95 617	95 622	95 626	95 631	95 636	95 641	95 646	95 650	95 655	95 660
905	95 665	95 670	95 674	95 679	95 684	95 689	95 694	95 698	95 703	95 708
906	95 713	95 718	95 722	95 727	95 732	95 737	95 742	95 746	95 751	95 756
907	95 761	95 766	95 770	95 775	95 780	95 785	95 789	95 794	95 799	95 804
908	95 809	95 813	95 818	95 823	95 828	95 832	95 837	95 842	95 847	95 852
909	95 856	95 861	95 866	95 871	95 875	95 880	95 885	95 890	95 895	95 899
910	95 904	95 909	95 914	95 918	95 923	95 928	95 933	95 938	95 942	95 947
911	95 952	95 957	95 961	95 966	95 971	95 976	95 980	95 985	95 990	95 995
912	95 999	96 004	96 009	96 014	96 019	96 023	96 028	96 033	96 038	96 042
913	96 047	96 052	96 057	96 061	96 066	96 071	96 076	96 080	96 085	96 090
914	96 095	96 099	96 104	96 109	96 114	96 118	96 123	96 128	96 133	96 137
915	96 142	96 147	96 152	96 156	96 161	96 166	96 171	96 175	96 180	96 185
916	96 190	96 194	96 199	96 204	96 209	96 213	96 218	96 223	96 227	96 232
917	96 237	96 242	96 246	96 251	96 256	96 261	96 265	96 270	96 275	96 280
918	96 284	96 289	96 294	96 298	96 303	96 308	96 313	96 317	96 322	96 327
919	96 332	96 336	96 341	96 346	96 350	96 355	96 360	96 365	96 369	96 374
920	96 379	96 384	96 388	96 393	96 398	96 402	96 407	96 412	96 417	96 421
921	96 426	96 431	96 435	96 440	96 445	96 450	96 454	96 459	96 464	96 468
922	96 473	96 478	96 483	96 487	96 492	96 497	96 501	96 506	96 511	96 515
923	96 520	96 525	96 530	96 534	96 539	96 544	96 548	96 553	96 558	96 562
924	96 567	96 572	96 577	96 581	96 586	96 591	96 595	96 600	96 605	96 609
925	96 614	96 619	96 624	96 628	96 633	96 638	96 642	96 647	96 652	96 656
926	96 661	96 666	96 670	96 675	96 680	96 685	96 689	96 694	96 699	96 703
927	96 708	96 713	96 717	96 722	96 727	96 731	96 736	96 741	96 745	96 750
928	96 755	96 759	96 764	96 769	96 774	96 778	96 783	96 788	96 792	96 797
929	96 802	96 806	96 811	96 816	96 820	96 825	96 830	96 834	96 839	96 844
930	96 848	96 853	96 858	96 862	96 867	96 872	96 876	96 881	96 886	96 890
931	96 895	96 900	96 904	96 909	96 914	96 918	96 923	96 928	96 932	96 937
932	96 942	96 946	96 951	96 956	96 960	96 965	96 970	96 974	96 979	96 984
933	96 988	96 993	96 997	97 002	97 007	97 011	97 016	97 021	97 025	97 030
934	97 035	97 039	97 044	97 049	97 053	97 058	97 063	97 067	97 072	97 077
935	97 081	97 086	97 090	97 095	97 100	97 104	97 109	97 114	97 118	97 123
936	97 128	97 132	97 137	97 142	97 146	97 151	97 155	97 160	97 165	97 169
937	97 174	97 179	97 183	97 188	97 192	97 197	97 202	97 206	97 211	97 216
938	97 220	97 225	97 230	97 234	97 239	97 243	97 248	97 253	97 257	97 262
939	97 267	97 271	97 276	97 280	97 285	97 290	97 294	97 299	97 304	97 308
940	97 313	97 317	97 322	97 327	97 331	97 336	97 340	97 345	97 350	97 354
941	97 359	97 364	97 368	97 373	97 377	97 382	97 387	97 391	97 396	97 400
942	97 405	97 410	97 414	97 419	97 424	97 428	97 433	97 437	97 442	97 447
943	97 451	97 456	97 460	97 465	97 470	97 474	97 479	97 483	97 488	97 493
944	97 497	97 502	97 506	97 511	97 516	97 520	97 525	97 529	97 534	97 539
945	97 543	97 548	97 552	97 557	97 562	97 566	97 571	97 575	97 580	97 585
946	97 589	97 594	97 598	97 603	97 607	97 612	97 617	97 621	97 626	97 630
947	97 635	97 640	97 644	97 649	97 653	97 658	97 663	97 667	97 672	97 676
948	97 681	97 685	97 690	97 695	97 699	97 704	97 708	97 713	97 717	97 722
949	97 727	97 731	97 736	97 740	97 745	97 749	97 754	97 759	97 763	97 768
950	97 772	97 777	97 782	97 786	97 791	97 795	97 800	97 804	97 809	97 813
N	0	1	2	3	4	5	6	7	8	9

N	0	1	2	3	4	5	6	7	8	9
950	97 772	97 777	97 782	97 786	97 791	97 795	97 800	97 804	97 809	97 813
951	97 818	97 823	97 827	97 832	97 836	97 841	97 845	97 850	97 855	97 859
952	97 864	97 868	97 873	97 877	97 882	97 886	97 891	97 896	97 900	97 905
953	97 909	97 914	97 918	97 923	97 928	97 932	97 937	97 941	97 946	97 950
954	97 955	97 959	97 964	97 968	97 973	97 978	97 982	97 987	97 991	97 996
955	98 000	98 005	98 009	98 014	98 019	98 023	98 028	98 032	98 037	98 041
956	98 046	98 050	98 055	98 059	98 064	98 068	98 073	98 078	98 082	98 087
957	98 091	98 096	98 100	98 105	98 109	98 114	98 118	98 123	98 127	98 132
958	98 137	98 141	98 146	98 150	98 155	98 159	98 164	98 168	98 173	98 177
959	98 182	98 186	98 191	98 195	98 200	98 204	98 209	98 214	98 218	98 223
960	98 227	98 232	98 236	98 241	98 245	98 250	98 254	98 259	98 263	98 268
961	98 272	98 277	98 281	98 286	98 290	98 295	98 299	98 304	98 308	98 313
962	98 318	98 322	98 327	98 331	98 336	98 340	98 345	98 349	98 354	98 358
963	98 363	98 367	98 372	98 376	98 381	98 385	98 390	98 394	98 399	98 403
964	98 408	98 412	98 417	98 421	98 426	98 430	98 435	98 439	98 444	98 448
965	98 453	98 457	98 462	98 466	98 471	98 475	98 480	98 484	98 489	98 493
966	98 498	98 502	98 507	98 511	98 516	98 520	98 525	98 529	98 534	98 538
967	98 543	98 547	98 552	98 556	98 561	98 565	98 570	98 574	98 579	98 583
968	98 588	98 592	98 597	98 601	98 605	98 610	98 614	98 619	98 623	98 628
969	98 632	98 637	98 641	98 646	98 650	98 655	98 659	98 664	98 668	98 673
970	98 677	98 682	98 686	98 691	98 695	98 700	98 704	98 709	98 713	98 717
971	98 722	98 726	98 731	98 735	98 740	98 744	98 749	98 753	98 758	98 762
972	98 767	98 771	98 776	98 780	98 784	98 789	98 793	98 798	98 802	98 807
973	98 811	98 816	98 820	98 825	98 829	98 834	98 838	98 843	98 847	98 851
974	98 856	98 860	98 865	98 869	98 874	98 878	98 883	98 887	98 892	98 896
975	98 900	98 905	98 909	98 914	98 918	98 923	98 927	98 932	98 936	98 941
976	98 945	98 949	98 954	98 958	98 963	98 967	98 972	98 976	98 981	98 985
977	98 989	98 994	98 998	99 003	99 007	99 012	99 016	99 021	99 025	99 029
978	99 034	99 038	99 043	99 047	99 052	99 056	99 061	99 065	99 069	99 074
979	99 078	99 083	99 087	99 092	99 096	99 100	99 105	99 109	99 114	99 118
980	99 123	99 127	99 131	99 136	99 140	99 145	99 149	99 154	99 158	99 162
981	99 167	99 171	99 176	99 180	99 185	99 189	99 193	99 198	99 202	99 207
982	99 211	99 216	99 220	99 224	99 229	99 233	99 238	99 242	99 247	99 251
983	99 255	99 260	99 264	99 269	99 273	99 277	99 282	99 286	99 291	99 295
984	99 300	99 304	99 308	99 313	99 317	99 322	99 326	99 330	99 335	99 339
985	99 344	99 348	99 352	99 357	99 361	99 366	99 370	99 374	99 379	99 383
986	99 388	99 392	99 396	99 401	99 405	99 410	99 414	99 419	99 423	99 427
987	99 432	99 436	99 441	99 445	99 449	99 454	99 458	99 463	99 467	99 471
988	99 476	99 480	99 484	99 489	99 493	99 498	99 502	99 506	99 511	99 515
989	99 520	99 524	99 528	99 533	99 537	99 542	99 546	99 550	99 555	99 559
990	99 564	99 568	99 572	99 577	99 581	99 585	99 590	99 594	99 599	99 603
991	99 607	99 612	99 616	99 621	99 625	99 629	99 634	99 638	99 642	99 647
992	99 651	99 656	99 660	99 664	99 669	99 673	99 677	99 682	99 686	99 691
993	99 695	99 699	99 704	99 708	99 712	99 717	99 721	99 726	99 730	99 734
994	99 739	99 743	99 747	99 752	99 756	99 760	99 765	99 769	99 774	99 778
995	99 782	99 787	99 791	99 795	99 800	99 804	99 808	99 813	99 817	99 822
996	99 826	99 830	99 835	99 839	99 843	99 848	99 852	99 856	99 861	99 865
997	99 870	99 874	99 878	99 883	99 887	99 891	99 896	99 900	99 904	99 909
998	99 913	99 917	99 922	99 926	99 930	99 935	99 939	99 944	99 948	99 952
999	99 957	99 961	99 965	99 970	99 974	99 978	99 983	99 987	99 991	99 996
1000	00 000	00 004	00 009	00 013	00 017	00 022	00 026	00 030	00 035	00 039
N	0	1	2	3	4	5	6	7	8	9

TABLE II.—LOGARITHMS OF CONSTANTS.

		log
Circumference of the Circle in degrees	= 360	2.55 630 250
Circumference of the Circle in minutes	= 21 600	4.33 445 375
Circumference of the Circle in seconds	= 1 296 000	6.11 260 500
If the radius $r = 1$, half the Circumference of the Circle is $\pi = 3.14\,159\,265\,358\,979\,323\,846\,264\,338\,328$		0.49 714 987

Also:	log		log
$2\pi = 6.28\,318\,531$	0.79 817 987	$\pi^2 \doteq 9.86\,960\,440$	0.99 429 97$\underline{5}$
$4\pi = 12.56\,637\,061$	1.09 920 986	$\frac{1}{\pi^2} = 0.10\,132\,118$	9.00 570 025 — 10
$\frac{\pi}{2} = 1.57\,079\,633$	0.19 611 988	$\sqrt{\pi} = 1.77\,245\,385$	0.24 857 494
$\frac{\pi}{3} = 1.04\,719\,755$	0.02 002 862	$\frac{1}{\sqrt{\pi}} = 0.56\,418\,958$	9.75 142 506 — 10
$\frac{4\pi}{3} = 4.18\,879\,020$	0.62 208 861	$\sqrt{\frac{3}{\pi}} = 0.97\,720\,502$	9.98 998 569 — 10
$\frac{\pi}{4} = 0.78\,539\,816$	9.89 508 988 — 10	$\sqrt{\frac{4}{\pi}} = 1.12\,837\,917$	0.05 245 506
$\frac{\pi}{6} = 0.52\,359\,878$	9.71 899 862 — 10	$\sqrt[3]{\pi} = 1.46\,459\,189$	0.16 571 662
$\frac{1}{\pi} = 0.31\,830\,989$	9.50 285 013 — 10	$\frac{1}{\sqrt[3]{\pi}} = 0.68\,278\,406$	9.83 428 338 — 10
$\frac{1}{2\pi} = 0.15\,915\,494$	9.20 182 013 — 10	$\sqrt[3]{\pi^2} = 2.14\,502\,940$	0.33 143 32$\underline{5}$
$\frac{3}{\pi} = 0.95\,492\,966$	9.97 997 138 — 10	$\sqrt[3]{\frac{3}{4\pi}} = 0.62\,035\,049$	9.79 263 713 — 10
$\frac{4}{\pi} = 1.27\,323\,954$	0.10 491 012	$\sqrt[3]{\frac{\pi}{6}} = 0.80\,599\,598$	9.90 633 287 — 10
$\frac{3}{4\pi} = 0.23\,873\,241$	9.37 791 139 — 10		

	log
Arc a, whose length is equal to the radius r, is:	
in degrees ..... a° ..... $= \frac{180}{\pi}$ .... $= 57.29\,577\,951^\circ$..	1.75 812 263
in minutes ..... a' ..... $= \frac{10\,800}{\pi}$ ...... $= 3\,437.74\,677'$ ..	3.53 627 388
in seconds ..... a'' ..... $= \frac{648\,000}{\pi}$ ..... $= 206\,264.806''$ ..	5.31 442 513
Arc $2a$, whose length is equal to twice the radius, $2r$, is:	
in degrees ..... $2a^\circ$ .... $= \frac{360}{\pi}$ .... $= 114.59\,155\,903^\circ$	2.05 915 263
in minutes ..... $2a'$ .... $= \frac{21\,600}{\pi}$ ...... $= 6\,875.49\,354'$ ..	3.83 730 388
in seconds ..... $2a''$ .... $= \frac{1\,296\,000}{\pi}$ .... $= 412\,529.612''$ ..	5.61 545 513
If the radius $r = 1$, the length of the arc is:	
for 1 degree .... $\frac{1}{a^\circ}$ .... $= \frac{\pi}{180}$ .... $= 0.01\,745\,329$...	8.24 187 737 — 10
for 1 minute .... $\frac{1}{a'}$ .... $= \frac{\pi}{10\,800}$ ...... $= 0.00\,029\,089$...	6.46 372 612 — 10
for 1 second .... $\frac{1}{a''}$ .... $= \frac{\pi}{648\,000}$ ..... $= 0.00\,000\,48\underline{5}$...	4.68 557 487 — 10
for ½ degree .... $\frac{1}{2a^\circ}$ .... $= \frac{\pi}{360}$ .... $= 0.00\,872\,66\underline{5}$...	7.94 084 737 — 10
for ½ minute .... $\frac{1}{2a'}$ .... $= \frac{\pi}{21\,600}$ ...... $= 0.00\,014\,544$...	6.16 269 612 — 10
for ½ second .... $\frac{1}{2a''}$ .... $= \frac{\pi}{1\,296\,000}$ .... $= 0.00\,000\,242$...	4.38 454 487 — 10
Sin 1″ in the unit circle .... $= 0.00\,000\,48\underline{5}$...	4.68 557 487 — 10

TABLE III.

THE LOGARITHMS

OF THE

TRIGONOMETRIC FUNCTIONS:

From 0° to 0° 3′, or 89° 57′ to 90°, for every second;
From 0° to 2°, or 88° to 90°, for every ten seconds;
From 1° to 89°, for every minute.

Note. To all the logarithms −10 is to be appended.

log sin 0°

log tan = log sin
log cos = 10.00 000

″	0′	1′	2′	″	″	0′	1′	2′	″
0	—	6.46 373	6.76 476	60	30	6.16 270	6.63 982	6.86 167	30
1	4.68 557	6.47 090	6.76 836	59	31	6.17 694	6.64 462	6.86 455	29
2	4.98 660	6.47 797	6.77 193	58	32	6.19 072	6.64 936	6.86 742	28
3	5.16 270	6.48 492	6.77 548	57	33	6.20 409	6.65 406	6.87 027	27
4	5.28 763	6.49 175	6.77 900	56	34	6.21 705	6.65 870	6.87 310	26
5	5.38 454	6.49 849	6.78 248	55	35	6.22 964	6.66 330	6.87 591	25
6	5.46 373	6.50 512	6.78 595̲	54	36	6.24 188	6.66 785̲	6.87 870	24
7	5.53 067	6.51 165̲	6.78 938	53	37	6.25 378	6.67 235̲	6.88 147	23
8	5.58 866	6.51 808	6.79 278	52	38	6.26 536	6.67 680	6.88 423	22
9	5.63 982	6.52 442	6.79 616	51	39	6.27 664	6.68 121	6.88 697	21
10	5.68 557	6.53 067	6.79 952	50	40	6.28 763	6.68 557	6.88 969	20
11	5.72 697	6.53 683	6.80 285̲	49	41	6.29 836	6.68 990	6.89 240	19
12	5.76 476	6.54 291	6.80 615̲	48	42	6.30 882	6.69 418	6.89 509	18
13	5.79 952	6.54 890	6.80 943	47	43	6.31 904	6.69 841	6.89 776	17
14	5.83 170	6.55 481	6.81 268	46	44	6.32 903	6.70 261	6.90 042	16
15	5.86 167	6.56 064	6.81 591	45	45	6.33 879	6.70 676	6.90 306	15
16	5.88 969	6.56 639	6.81 911	44	46	6.34 833	6.71 088	6.90 568	14
17	5.91 602	6.57 207	6.82 230	43	47	6.35 767	6.71 496	6.90 829	13
18	5.94 085̲	6.57 767	6.82 545	42	48	6.36 682	6.71 900	6.91 088	12
19	5.96 433	6.58 320	6.82 859	41	49	6.37 577	6.72 300	6.91 346	11
20	5.98 660	6.58 866	6.83 170	40	50	6.38 454	6.72 697	6.91 602	10
21	6.00 779	6.59 406	6.83 479	39	51	6.39 315̲	6.73 090	6.91 857	9
22	6.02 800	6.59 939	6.83 786	38	52	6.40 158	6.73 479	6.92 110	8
23	6.04 730	6.60 465	6.84 091	37	53	6.40 985	6.73 865	6.92 362	7
24	6.06 579	6.60 985	6.84 394	36	54	6.41 797	6.74 248	6.92 612	6
25	6.08 351	6.61 499	6.84 694	35	55	6.42 594	6.74 627	6.92 861	5
26	6.10 055̲	6.62 007	6.84 993	34	56	6.43 376	6.75 003	6.93 109	4
27	6.11 694	6.62 509	6.85 289	33	57	6.44 145̲	6.75 376	6.93 355̲	3
28	6.13 273	6.63 006	6.85 584	32	58	6.44 900	6.75 746	6.93 599	2
29	6.14 797	6.63 496	6.85 876	31	59	6.45 643	6.76 112	6.93 843	1
30	6.16 270	6.63 982	6.86 167	30	60	6.46 373	6.76 476	6.94 085̲	0
″	59′	58′	57′	″	″	59′	58′	57′	″

log cot = log cos
log sin = 10.00 000

89° log cos

0°

′ ″	log sin	log tan	log cos	″ ′
40 0	8.06 578	8.06 581	9.99 997	0 20
10	8.06 758	8.06 761	9.99 997	50
20	8.06 938	8.06 941	9.99 997	40
30	8.07 117	8.07 120	9.99 997	30
40	8.07 295	8.07 299	9.99 997	20
50	8.07 473	8.07 476	9.99 997	10
41 0	8.07 650	8.07 653	9.99 997	0 19
10	8.07 826	8.07 829	9.99 997	50
20	8.08 002	8.08 005	9.99 997	40
30	8.08 176	8.08 180	9.99 997	30
40	8.08 350	8.08 354	9.99 997	20
50	8.08 524	8.08 527	9.99 997	10
42 0	8.08 696	8.08 700	9.99 997	0 18
10	8.08 868	8.08 872	9.99 997	50
20	8.09 040	8.09 043	9.99 997	40
30	8.09 210	8.09 214	9.99 997	30
40	8.09 380	8.09 384	9.99 997	20
50	8.09 550	8.09 553	9.99 997	10
43 0	8.09 718	8.09 722	9.99 997	0 17
10	8.09 886	8.09 890	9.99 997	50
20	8.10 054	8.10 057	9.99 997	40
30	8.10 220	8.10 224	9.99 997	30
40	8.10 386	8.10 390	9.99 997	20
50	8.10 552	8.10 555	9.99 996	10
44 0	8.10 717	8.10 720	9.99 996	0 16
10	8.10 881	8.10 884	9.99 996	50
20	8.11 044	8.11 048	9.99 996	40
30	8.11 207	8.11 211	9.99 996	30
40	8.11 370	8.11 373	9.99 996	20
50	8.11 531	8.11 535	9.99 996	10
45 0	8.11 693	8.11 696	9.99 996	0 15
10	8.11 853	8.11 857	9.99 996	50
20	8.12 013	8.12 017	9.99 996	40
30	8.12 172	8.12 176	9.99 996	30
40	8.12 331	8.12 335	9.99 996	20
50	8.12 489	8.12 493	9.99 996	10
46 0	8.12 647	8.12 651	9.99 996	0 14
10	8.12 804	8.12 808	9.99 996	50
20	8.12 961	8.12 965	9.99 996	40
30	8.13 117	8.13 121	9.99 996	30
40	8.13 272	8.13 276	9.99 996	20
50	8.13 427	8.13 431	9.99 996	10
47 0	8.13 581	8.13 585	9.99 996	0 13
10	8.13 735	8.13 739	9.99 996	50
20	8.13 888	8.13 892	9.99 996	40
30	8.14 041	8.14 045	9.99 996	30
40	8.14 193	8.14 197	9.99 996	20
50	8.14 344	8.14 348	9.99 996	10
48 0	8.14 495	8.14 500	9.99 996	0 12
10	8.14 646	8.14 650	9.99 996	50
20	8.14 796	8.14 800	9.99 996	40
30	8.14 945	8.14 950	9.99 996	30
40	8.15 094	8.15 099	9.99 996	20
50	8.15 243	8.15 247	9.99 996	10
49 0	8.15 391	8.15 395	9.99 996	0 11
10	8.15 538	8.15 543	9.99 996	50
20	8.15 685	8.15 690	9.99 996	40
30	8.15 832	8.15 836	9.99 996	30
40	8.15 978	8.15 982	9.99 995	20
50	8.16 123	8.16 128	9.99 995	10
50 0	8.16 268	8.16 273	9.99 995	0 10
′ ″	log cos	log cot	log sin	″ ′

′ ″	log sin	log tan	log cos	″ ′
50 0	8.16 268	8.16 273	9.99 995	0 10
10	8.16 413	8.16 417	9.99 995	50
20	8.16 557	8.16 561	9.99 995	40
30	8.16 700	8.16 705	9.99 995	30
40	8.16 843	8.16 848	9.99 995	20
50	8.16 986	8.16 991	9.99 995	10
51 0	8.17 128	8.17 133	9.99 995	0 9
10	8.17 270	8.17 275	9.99 995	50
20	8.17 411	8.17 416	9.99 995	40
30	8.17 552	8.17 557	9.99 995	30
40	8.17 692	8.17 697	9.99 995	20
50	8.17 832	8.17 837	9.99 995	10
52 0	8.17 971	8.17 976	9.99 995	0 8
10	8.18 110	8.18 115	9.99 995	50
20	8.18 249	8.18 254	9.99 995	40
30	8.18 387	8.18 392	9.99 995	30
40	8.18 524	8.18 530	9.99 995	20
50	8.18 662	8.18 667	9.99 995	10
53 0	8.18 798	8.18 804	9.99 995	0 7
10	8.18 935	8.18 940	9.99 995	50
20	8.19 071	8.19 076	9.99 995	40
30	8.19 206	8.19 212	9.99 995	30
40	8.19 341	8.19 347	9.99 995	20
50	8.19 476	8.19 481	9.99 995	10
54 0	8.19 610	8.19 616	9.99 995	0 6
10	8.19 744	8.19 749	9.99 995	50
20	8.19 877	8.19 883	9.99 995	40
30	8.20 010	8.20 016	9.99 995	30
40	8.20 143	8.20 149	9.99 995	20
50	8.20 275	8.20 281	9.99 994	10
55 0	8.20 407	8.20 413	9.99 994	0 5
10	8.20 538	8.20 544	9.99 994	50
20	8.20 669	8.20 675	9.99 994	40
30	8.20 800	8.20 806	9.99 994	30
40	8.20 930	8.20 936	9.99 994	20
50	8.21 060	8.21 066	9.99 994	10
56 0	8.21 189	8.21 195	9.99 994	0 4
10	8.21 319	8.21 324	9.99 994	50
20	8.21 447	8.21 453	9.99 994	40
30	8.21 576	8.21 581	9.99 994	30
40	8.21 703	8.21 709	9.99 944	20
50	8.21 831	8.21 837	9.99 994	10
57 0	8.21 958	8.21 964	9.99 994	0 3
10	8.22 085	8.22 091	9.99 994	50
20	8.22 211	8.22 217	9.99 994	40
30	8.22 337	8.22 343	9.99 994	30
40	8.22 463	8.22 469	9.99 994	20
50	8.22 588	8.22 595	9.99 994	10
58 0	8.22 713	8.22 720	9.99 994	0 2
10	8.22 838	8.22 844	9.99 994	50
20	8.22 962	8.22 968	9.99 994	40
30	8.23 086	8.23 092	9.99 994	30
40	8.23 210	8.23 216	9.99 994	20
50	8.23 333	8.23 339	9.99 994	10
59 0	8.23 456	8.23 462	9.99 994	0 1
10	8.23 578	8.23 585	9.99 994	50
20	8.23 700	8.23 707	9.99 994	40
30	8.23 822	8.23 829	9.99 993	30
40	8.23 944	8.23 950	9.99 993	20
50	8.24 065	8.24 071	9.99 993	10
60 0	8.24 186	8.24 192	9.99 993	0 0
′ ″	log cos	log cot	log sin	″ ′

89°

1°

′ ″	log sin	log tan	log cos	″ ′	′ ″	log sin	log tan	log cos	″ ′
0 0	8. 24 186	8. 24 192	9. 99 993	0 60	10 0	8. 30 879	8. 30 888	9. 99 991	0 50
10	8. 24 306	8. 24 313	9. 99 993	50	10	8. 30 983	8. 30 992	9. 99 991	50
20	8. 24 426	8. 24 433	9. 99 993	40	20	8. 31 086	8. 31 095	9. 99 991	40
30	8. 24 546	8. 24 553	9. 99 993	30	30	8. 31 188	8. 31 198	9. 99 991	30
40	8. 24 665	8. 24 672	9. 99 993	20	40	8. 31 291	8. 31 300	9. 99 991	20
50	8. 24 785	8. 24 791	9. 99 993	10	50	8. 31 393	8. 31 403	9. 99 991	10
1 0	8. 24 903	8. 24 910	9. 99 993	0 59	11 0	8. 31 495	8. 31 505	9. 99 991	0 49
10	8. 25 022	8. 25 029	9. 99 993	50	10	8. 31 597	8. 31 606	9. 99 991	50
20	8. 25 140	8. 25 147	9. 99 993	40	20	8. 31 699	8. 31 708	9. 99 991	40
30	8. 25 258	8. 25 265	9. 99 993	30	30	8. 31 800	8. 31 809	9. 99 991	30
40	8. 25 375	8. 25 382	9. 99 993	20	40	8. 31 901	8. 31 911	9. 99 991	20
50	8. 25 493	8. 25 500	9. 99 993	10	50	8. 32 002	8. 32 012	9. 99 991	10
2 0	8. 25 609	8. 25 616	9. 99 993	0 58	12 0	8. 32 103	8. 32 112	9. 99 990	0 48
10	8. 25 726	8. 25 733	9. 99 993	50	10	8. 32 203	8. 32 213	9. 99 990	50
20	8. 25 842	8. 25 849	9. 99 993	40	20	8. 32 303	8. 32 313	9. 99 990	40
30	8. 25 958	8. 25 965	9. 99 993	30	30	8. 32 403	8. 32 413	9. 99 990	30
40	8. 26 074	8. 26 081	9. 99 993	20	40	8. 32 503	8. 32 513	9. 99 990	20
50	8. 26 189	8. 26 196	9. 99 993	10	50	8. 32 602	8. 32 612	9. 99 990	10
3 0	8. 26 304	8. 26 312	9. 99 993	0 57	13 0	8. 32 702	8. 32 711	9. 99 990	0 47
10	8. 26 419	8. 26 426	9. 99 993	50	10	8. 32 801	8. 32 811	9. 99 990	50
20	8. 26 533	8. 26 541	9. 99 993	40	20	8. 32 899	8. 32 909	9. 99 990	40
30	8. 26 648	8. 26 655	9. 99 993	30	30	8. 32 998	8. 33 008	9. 99 990	30
40	8. 26 761	8. 26 769	9. 99 993	20	40	8. 33 096	8. 33 106	9. 99 990	20
50	8. 26 875	8. 26 882	9. 99 993	10	50	8. 33 195	8. 33 205	9. 99 990	10
4 0	8. 26 988	8. 26 996	9. 99 992	0 56	14 0	8. 33 292	8. 33 302	9. 99 990	0 46
10	8. 27 101	8. 27 109	9. 99 992	50	10	8. 33 390	8. 33 400	9. 99 990	50
20	8. 27 214	8. 27 221	9. 99 992	40	20	8. 33 488	8. 33 498	9. 99 990	40
30	8. 27 326	8. 27 334	9. 99 992	30	30	8. 33 585	8. 33 595	9. 99 990	30
40	8. 27 438	8. 27 446	9. 99 992	20	40	8. 33 682	8. 33 692	9. 99 990	20
50	8. 27 550	8. 27 558	9. 99 992	10	50	8. 33 779	8. 33 789	9. 99 990	10
5 0	8. 27 661	8. 27 669	9. 99 992	0 55	15 0	8. 33 875	8. 33 886	9. 99 990	0 45
10	8. 27 773	8. 27 780	9. 99 992	50	10	8. 33 972	8. 33 982	9. 99 990	50
20	8. 27 883	8. 27 891	9. 99 992	40	20	8. 34 068	8. 34 078	9. 99 990	40
30	8. 27 994	8. 28 002	9. 99 992	30	30	8. 34 164	8. 34 174	9. 99 990	30
40	8. 28 104	8. 28 112	9. 99 992	20	40	8. 34 260	8. 34 270	9. 99 989	20
50	8. 28 215	8. 28 223	9. 99 992	10	50	8. 34 355	8. 34 366	9. 99 989	10
6 0	8. 28 324	8. 28 332	9. 99 992	0 54	16 0	8. 34 450	8. 34 461	9. 99 989	0 44
10	8. 28 434	8. 28 442	9. 99 992	50	10	8. 34 546	8. 34 556	9. 99 989	50
20	8. 28 543	8. 28 551	9. 99 992	40	20	8. 34 640	8. 34 651	9. 99 989	40
30	8. 28 652	8. 28 660	9. 99 992	30	30	8. 34 735	8. 34 746	9. 99 989	30
40	8. 28 761	8. 28 769	9. 99 992	20	40	8. 34 830	8. 34 840	9. 99 989	20
50	8. 28 869	8. 28 877	9. 99 992	10	50	8. 34 924	8. 34 935	9. 99 989	10
7 0	8. 28 977	8. 28 986	9. 99 992	0 53	17 0	8. 35 018	8. 35 029	9. 99 989	0 43
10	8. 29 085	8. 29 094	9. 99 992	50	10	8. 35 112	8. 35 123	9. 99 989	50
20	8. 29 193	8. 29 201	9. 99 992	40	20	8. 35 206	8. 35 217	9. 99 989	40
30	8. 29 300	8. 29 309	9. 99 992	30	30	8. 35 299	8. 35 310	9. 99 989	30
40	8. 29 407	8. 29 416	9. 99 992	20	40	8. 35 392	8. 35 403	9. 99 989	20
50	8. 29 514	8. 29 523	9. 99 992	10	50	8. 35 485	8. 35 497	9. 99 989	10
8 0	8. 29 621	8. 29 629	9. 99 992	0 52	18 0	8. 35 578	8. 35 590	9. 99 989	0 42
10	8. 29 727	8. 29 736	9. 99 991	50	10	8. 35 671	8. 35 682	9. 99 989	50
20	8. 29 833	8. 29 842	9. 99 991	40	20	8. 35 764	8. 35 775	9. 99 989	40
30	8. 29 939	8. 29 947	9. 99 991	30	30	8. 35 856	8. 35 867	9. 99 989	30
40	8. 30 044	8. 30 053	9. 99 991	20	40	8. 35 948	8. 35 959	9. 99 989	20
50	8. 30 150	8. 30 158	9. 99 991	10	50	8. 36 040	8. 36 051	9. 99 989	10
9 0	8. 30 255	8. 30 263	9. 99 991	0 51	19 0	8. 36 131	8. 36 143	9. 99 989	0 41
10	8. 30 359	8. 30 368	9. 99 991	50	10	8. 36 223	8. 36 235	9. 99 988	50
20	8. 30 464	8. 30 473	9. 99 991	40	20	8. 36 314	8. 36 326	9. 99 988	40
30	8. 30 568	8. 30 577	9. 99 991	30	30	8. 36 405	8. 36 417	9. 99 988	30
40	8. 30 672	8. 30 681	9. 99 991	20	40	8. 36 496	8. 36 508	9. 99 988	20
50	8. 30 776	8. 30 785	9. 99 991	10	50	8. 36 587	8. 36 599	9. 99 988	10
10 0	8. 30 879	8. 30 888	9. 99 991	0 50	20 0	8. 36 678	8. 36 689	9. 99 988	0 40
′ ″	log cos	log cot	log sin	″ ′	′ ″	log cos	log cot	log sin	″ ′

88°

1°

′ ″	log sin	log tan	log cos	″ ′	′ ″	log sin	log tan	log cos	″ ′
20 0	8. 36 678	8. 36 689	9. 99 988	0 **40**	**30** 0	8. 41 792	8. 41 807	9. 99 985	0 **30**
10	8. 36 768	8. 36 780	9. 99 988	50	10	8. 41 872	8. 41 887	9. 99 985	50
20	8. 36 858	8. 36 870	9. 99 988	40	20	8. 41 952	8. 41 967	9. 99 985	40
30	8. 36 948	8. 36 960	9. 99 988	30	30	8. 42 032	8. 42 048	9. 99 985	30
40	8. 37 038	8. 37 050	9. 99 988	20	40	8. 42 112	8. 42 127	9. 99 985	20
50	8. 37 128	8. 37 140	9. 99 988	10	50	8. 42 192	8. 42 207	9. 99 985	10
21 0	8. 37 217	8. 37 229	9. 99 988	0 **39**	**31** 0	8. 42 272	8. 42 287	9. 99 985	0 **29**
10	8. 37 306	8. 37 318	9. 99 988	50	10	8. 42 351	8. 42 366	9. 99 985	50
20	8. 37 395	8. 37 408	9. 99 988	40	20	8. 42 430	8. 42 446	9. 99 985	40
30	8. 37 484	8. 37 497	9. 99 988	30	30	8. 42 510	8. 42 525	9. 99 985	30
40	8. 37 573	8. 37 585	9. 99 988	20	40	8. 42 589	8. 42 604	9. 99 985	20
50	8. 37 662	8. 37 674	9. 99 988	10	50	8. 42 667	8. 42 683	9. 99 985	10
22 0	8. 37 750	8. 37 762	9. 99 988	0 **38**	**32** 0	8. 42 746	8. 42 762	9. 99 984	0 **28**
10	8. 37 838	8. 37 850	9. 99 988	50	10	8. 42 825	8. 42 840	9. 99 984	50
20	8. 37 926	8. 37 938	9. 99 988	40	20	8. 42 903	8. 42 919	9. 99 984	40
30	8. 38 014	8. 38 026	9. 99 987	30	30	8. 42 982	8. 42 997	9. 99 984	30
40	8. 38 101	8. 38 114	9. 99 987	20	40	8. 43 060	8. 43 075	9. 99 984	20
50	8. 38 189	8. 38 202	9. 99 987	10	50	8. 43 138	8. 43 154	9. 99 984	10
23 0	8. 38 276	8. 38 289	9. 99 987	0 **37**	**33** 0	8. 43 216	8. 43 232	9. 99 984	0 **27**
10	8. 38 363	8. 38 376	9. 99 987	50	10	8. 43 293	8. 43 309	9. 99 984	50
20	8. 38 450	8. 38 463	9. 99 987	40	20	8. 43 371	8. 43 387	9. 99 984	40
30	8. 38 537	8. 38 550	9. 99 987	30	30	8. 43 448	8. 43 464	9. 99 984	30
40	8. 38 624	8. 38 636	9. 99 987	20	40	8. 43 526	8. 43 542	9. 99 984	20
50	8. 38 710	8. 38 723	9. 99 987	10	50	8. 43 603	8. 43 619	9. 99 984	10
24 0	8. 38 796	8. 38 809	9. 99 987	0 **36**	**34** 0	8. 43 680	8. 43 696	9. 99 984	0 **26**
10	8. 38 882	8. 38 895	9. 99 987	50	10	8. 43 757	8. 43 773	9. 99 984	50
20	8. 38 968	8. 38 981	9. 99 987	40	20	8. 43 834	8. 43 850	9. 99 984	40
30	8. 39 054	8. 39 067	9. 99 987	30	30	8. 43 910	8. 43 927	9. 99 984	30
40	8. 39 139	8. 39 153	9. 99 987	20	40	8. 43 987	8. 44 003	9. 99 984	20
50	8. 39 225	8. 39 238	9. 99 987	10	50	8. 44 063	8. 44 080	9. 99 983	10
25 0	8. 39 310	8. 39 323	9. 99 987	0 **35**	**35** 0	8. 44 139	8. 44 156	9. 99 983	0 **25**
10	8. 39 395	8. 39 408	9. 99 987	50	10	8. 44 216	8. 44 232	9. 99 983	50
20	8. 39 480	8. 39 493	9. 99 987	40	20	8. 44 292	8. 44 308	9. 99 983	40
30	8. 39 565	8. 39 578	9. 99 987	30	30	8. 44 367	8. 44 384	9. 99 983	30
40	8. 39 649	8. 39 663	9. 99 987	20	40	8. 44 443	8. 44 460	9. 99 983	20
50	8. 39 734	8. 39 747	9. 99 986	10	50	8. 44 519	8. 44 536	9. 99 983	10
26 0	8. 39 818	8. 39 832	9. 99 986	0 **34**	**36** 0	8. 44 594	8. 44 611	9. 99 983	0 **24**
10	8. 39 902	8. 39 916	9. 99 986	50	10	8. 44 669	8. 44 686	9. 99 983	50
20	8. 39 986	8. 40 000	9. 99 986	40	20	8. 44 745	8. 44 762	9. 99 983	40
30	8. 40 070	8. 40 083	9. 99 986	30	30	8. 44 820	8. 44 837	9. 99 983	30
40	8. 40 153	8. 40 167	9. 99 986	20	40	8. 44 895	8. 44 912	9. 99 983	20
50	8. 40 237	8. 40 251	9. 99 986	10	50	8. 44 969	8. 44 987	9. 99 983	10
27 0	8. 40 320	8. 40 334	9. 99 986	0 **33**	**37** 0	8. 45 044	8. 45 061	9. 99 983	0 **23**
10	8. 40 403	8. 40 417	9. 99 986	50	10	8. 45 119	8. 45 136	9. 99 983	50
20	8. 40 486	8. 40 500	9. 99 986	40	20	8. 45 193	8. 45 210	9. 99 983	40
30	8. 40 569	8. 40 583	9. 99 986	30	30	8. 45 267	8. 45 285	9. 99 983	30
40	8. 40 651	8. 40 665	9. 99 986	20	40	8. 45 341	8. 45 359	9. 99 982	20
50	8. 40 734	8. 40 748	9. 99 986	10	50	8. 45 415	8. 45 433	9. 99 982	10
28 0	8. 40 816	8. 40 830	9. 99 986	0 **32**	**38** 0	8. 45 489	8. 45 507	9. 99 982	0 **22**
10	8. 40 898	8. 40 913	9. 99 986	50	10	8. 45 563	8. 45 581	9. 99 982	50
20	8. 40 980	8. 40 995	9. 99 986	40	20	8. 45 637	8. 45 655	9. 99 982	40
30	8. 41 062	8. 41 077	9. 99 986	30	30	8. 45 710	8. 45 728	9. 99 982	30
40	8. 41 144	8. 41 158	9. 99 986	20	40	8. 45 784	8. 45 802	9. 99 982	20
50	8. 41 225	8. 41 240	9. 99 986	10	50	8. 45 857	8. 45 875	9. 99 982	10
29 0	8. 41 307	8. 41 321	9. 99 985	0 **31**	**39** 0	8. 45 930	8. 45 948	9. 99 982	0 **21**
10	8. 41 388	8. 41 403	9. 99 985	50	10	8. 46 003	8. 46 021	9. 99 982	50
20	8. 41 469	8. 41 484	9. 99 985	40	20	8. 46 076	8. 46 094	9. 99 982	40
30	8. 41 550	8. 41 565	9. 99 985	30	30	8. 46 149	8. 46 167	9. 99 982	30
40	8. 41 631	8. 41 646	9. 99 985	20	40	8. 46 222	8. 46 240	9. 99 982	20
50	8. 41 711	8. 41 726	9. 99 985	10	50	8. 46 294	8. 46 312	9. 99 982	10
30 0	8. 41 792	8. 41 807	9. 99 985	0 **30**	**40** 0	8. 46 366	8. 46 385	9. 99 982	0 **20**
′ ″	log cos	log cot	log sin	″ ′	′ ″	log cos	log cot	log sin	″ ′

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1°

′ ″	log sin	log tan	log cos	″ ′	′ ″	log sin	log tan	log cos	″ ′
40 0	8.46 366	8.46 385	9.99 982	0 20	50 0	8.50 504	8.50 527	9.99 978	0 10
10	8.46 439	8.46 457	9.99 982	50	10	8.50 570	8.50 593	9.99 978	50
20	8.46 511	8.46 529	9.99 982	40	20	8.50 636	8.50 658	9.99 978	40
30	8.46 583	8.46 602	9.99 981	30	30	8.50 701	8.50 724	9.99 978	30
40	8.46 655	8.46 674	9.99 981	20	40	8.50 767	8.50 789	9.99 977	20
50	8.46 727	8.46 745	9.99 981	10	50	8.50 832	8.50 855	9.99 977	10
41 0	8.46 799	8.46 817	9.99 981	0 19	51 0	8.50 897	8.50 920	9.99 977	0 9
10	8.46 870	8.46 889	9.99 981	50	10	8.50 963	8.50 985	9.99 977	50
20	8.46 942	8.46 960	9.99 981	40	20	8.51 028	8.51 050	9.99 977	40
30	8.47 013	8.47 032	9.99 981	30	30	8.51 092	8.51 115	9.99 977	30
40	8.47 084	8.47 103	9.99 981	20	40	8.51 157	8.51 180	9.99 977	20
50	8.47 155	8.47 174	9.99 981	10	50	8.51 222	8.51 245	9.99 977	10
42 0	8.47 226	8.47 245	9.99 981	0 18	52 0	8.51 287	8.51 310	9.99 977	0 8
10	8.47 297	8.47 316	9.99 981	50	10	8.51 351	8.51 374	9.99 977	50
20	8.47 368	8.47 387	9.99 981	40	20	8.51 416	8.51 439	9.99 977	40
30	8.47 439	8.47 458	9.99 981	30	30	8.51 480	8.51 503	9.99 977	30
40	8.47 509	8.47 528	9.99 981	20	40	8.51 544	8.51 568	9.99 977	20
50	8.47 580	8.47 599	9.99 981	10	50	8.51 609	8.51 632	9.99 977	10
43 0	8.47 650	8.47 669	9.99 981	0 17	53 0	8.51 673	8.51 696	9.99 977	0 7
10	8.47 720	8.47 740	9.99 980	50	10	8.51 737	8.51 760	9.99 976	50
20	8.47 790	8.47 810	9.99 980	40	20	8.51 801	8.51 824	9.99 976	40
30	8.47 860	8.47 880	9.99 980	30	30	8.51 864	8.51 888	9.99 976	30
40	8.47 930	8.47 950	9.99 980	20	40	8.51 928	8.51 952	9.99 976	20
50	8.48 000	8.48 020	9.99 980	10	50	8.51 992	8.52 015	9.99 976	10
44 0	8.48 069	8.48 090	9.99 980	0 16	54 0	8.52 055	8.52 079	9.99 976	0 6
10	8.48 139	8.48 159	9.99 980	50	10	8.52 119	8.52 143	9.99 976	50
20	8.48 208	8.48 228	9.99 980	40	20	8.52 182	8.52 206	9.99 976	40
30	8.48 278	8.48 298	9.99 980	30	30	8.52 245	8.52 269	9.99 976	30
40	8.48 347	8.48 367	9.99 980	20	40	8.52 308	8.52 332	9.99 976	20
50	8.48 416	8.48 436	9.99 980	10	50	8.52 371	8.52 396	9.99 976	10
45 0	8.48 485	8.48 505	9.99 980	0 15	55 0	8.52 434	8.52 459	9.99 976	0 5
10	8.48 554	8.48 574	9.99 980	50	10	8.52 497	8.52 522	9.99 976	50
20	8.48 622	8.48 643	9.99 980	40	20	8.52 560	8.52 584	9.99 976	40
30	8.48 691	8.48 711	9.99 980	30	30	8.52 623	8.52 647	9.99 975	30
40	8.48 760	8.48 780	9.99 979	20	40	8.52 685	8.52 710	9.99 975	20
50	8.48 828	8.48 849	9.99 979	10	50	8.52 748	8.52 772	9.99 975	10
46 0	8.48 896	8.48 917	9.99 979	0 14	56 0	8.52 810	8.52 835	9.99 975	0 4
10	8.48 965	8.48 985	9.99 979	50	10	8.52 872	8.52 897	9.99 975	50
20	8.49 033	8.49 053	9.99 979	40	20	8.52 935	8.52 960	9.99 975	40
30	8.49 101	8.49 121	9.99 979	30	30	8.52 997	8.53 022	9.99 975	30
40	8.49 169	8.49 189	9.99 979	20	40	8.53 059	8.53 084	9.99 975	20
50	8.49 236	8.49 257	9.99 979	10	50	8.53 121	8.53 146	9.99 975	10
47 0	8.49 304	8.49 325	9.99 979	0 13	57 0	8.53 183	8.53 208	9.99 975	0 3
10	8.49 372	8.49 393	9.99 979	50	10	8.53 245	8.53 270	9.99 975	50
20	8.49 439	8.49 460	9.99 979	40	20	8.53 306	8.53 332	9.99 975	40
30	8.49 506	8.49 528	9.99 979	30	30	8.53 368	8.53 393	9.99 975	30
40	8.49 574	8.49 595	9.99 979	20	40	8.53 429	8.53 455	9.99 975	20
50	8.49 641	8.49 662	9.99 979	10	50	8.53 491	8.53 516	9.99 974	10
48 0	8.49 708	8.49 729	9.99 979	0 12	58 0	8.53 552	8.53 578	9.99 974	0 2
10	8.49 775	8.49 796	9.99 979	50	10	8.53 614	8.53 639	9.99 974	50
20	8.49 842	8.49 863	9.99 978	40	20	8.53 675	8.53 700	9.99 974	40
30	8.49 908	8.49 930	9.99 978	30	30	8.53 736	8.53 762	9.99 974	30
40	8.49 975	8.49 997	9.99 978	20	40	8.53 797	8.53 823	9.99 974	20
50	8.50 042	8.50 063	9.99 978	10	50	8.53 858	8.53 884	9.99 974	10
49 0	8.50 108	8.50 130	9.99 978	0 11	59 0	8.53 919	8.53 945	9.99 974	0 1
10	8.50 174	8.50 196	9.99 978	50	10	8.53 979	8.54 005	9.99 974	50
20	8.50 241	8.50 263	9.99 978	40	20	8.54 040	8.54 066	9.99 974	40
30	8.50 307	8.50 329	9.99 978	30	30	8.54 101	8.54 127	9.99 974	30
40	8.50 373	8.50 395	9.99 978	20	40	8.54 161	8.54 187	9.99 974	20
50	8.50 439	8.50 461	9.99 978	10	50	8.54 222	8.54 248	9.99 974	10
50 0	8.50 504	8.50 527	9.99 978	0 10	60 0	8.54 282	8.54 308	9.99 974	0 0
′ ″	log cos	log cot	log sin	″ ′	′ ″	log cos	log cot	log sin	″ ′

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1°

′	log sin	log tan	log cot	log cos	′
	8	8	11	9	
0	24 186	24 192	75 808	99 993	60
1	24 903	24 910	75 090	99 993	59
2	25 609	25 616	74 384	99 993	58
3	26 304	26 312	73 688	99 993	57
4	26 988	26 996	73 004	99 992	56
5	27 661	27 669	72 331	99 992	55
6	28 324	28 332	71 668	99 992	54
7	28 977	28 986	71 014	99 992	53
8	29 621	29 629	70 371	99 992	52
9	30 255̲	30 263	69 737	99 991	51
10	30 879	30 888	69 112	99 991	50
11	31 495	31 505̲	68 495	99 991	49
12	32 103	32 112	67 888	99 990	48
13	32 702	32 711	67 289	99 990	47
14	33 292	33 302	66 698	99 990	46
15	33 875	33 886	66 114	99 990	45
16	34 450	34 461	65 539	99 989	44
17	35 018	35 029	64 971	99 989	43
18	35 578	35 590	64 410	99 989	42
19	36 131	36 143	63 857	99 989	41
20	36 678	36 689	63 311	99 988	40
21	37 217	37 229	62 771	99 988	39
22	37 75̲0	37 762	62 238	99 988	38
23	38 276	38 289	61 711	99 987	37
24	38 796	38 809	61 191	99 987	36
25	39 310	39 323	60 677	99 987	35
26	39 818	39 832	60 168	99 986	34
27	40 320	40 334	59 666	99 986	33
28	40 816	40 830	59 170	99 986	32
29	41 307	41 321	58 679	99 985	31
30	41 792	41 807	58 193	99 985	30
31	42 272	42 287	57 713	99 985̲	29
32	42 746	42 762	57 238	99 984	28
33	43 216	43 232	56 768	99 984	27
34	43 680	43 696	56 304	99 984	26
35	44 139	44 156	55 844	99 983	25
36	44 594	44 611	55 389	99 983	24
37	45 044	45 061	54 939	99 983	23
38	45 489	45 507	54 493	99 982	22
39	45 930	45 948	54 052	99 982	21
40	46 366	46 385̲	53 615	99 982	20
41	46 799	46 817	53 183	99 981	19
42	47 226	47 245	52 755̲	99 981	18
43	47 65̲0	47 669	52 331	99 981	17
44	48 069	48 089	51 911	99 980	16
45	48 485̲	48 505	51 495̲	99 980	15
46	48 896	48 917	51 083	99 979	14
47	49 304	49 325	50 675̲	99 979	13
48	49 708	49 729	50 271	99 979	12
49	50 108	50 130	49 870	99 978	11
50	50 504	50 527	49 473	99 978	10
51	50 897	50 920	49 080	99 977	9
52	51 287	51 310	48 690	99 977	8
53	51 673	51 696	48 304	99 977	7
54	52 055	52 079	47 921	99 976	6
55	52 434	52 459	47 541	99 976	5
56	52 810	52 835̲	47 165	99 975	4
57	53 183	53 208	46 792	99 975̲	3
58	53 552	53 578	46 422	99 974	2
59	53 919	53 945̲	46 055	99 974	1
60	54 282	54 308	45 692	99 974	0
	8	8	11	9	
′	log cos	log cot	log tan	log sin	′

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2°

′	log sin	log tan	log cot	log cos	′
	8	8	11	9	
0	54 282	54 308	45 692	99 974	60
1	54 642	54 669	45 331	99 973	59
2	54 999	55 027	44 973	99 973	58
3	55 354	55 382	44 618	99 972	57
4	55 705	55 734	44 266	99 972	56
5	56 054	56 083	43 917	99 971	55
6	56 400	56 429	43 571	99 971	54
7	56 743	56 773	43 227	99 970	53
8	57 084	57 114	42 886	99 970	52
9	57 421	57 452	42 548	99 969	51
10	57 757	57 788	42 212	99 969	50
11	58 089	58 121	41 879	99 968	49
12	58 419	58 451	41 549	99 968	48
13	58 747	58 779	41 221	99 967	47
14	59 072	59 105	40 895̲	99 967	46
15	59 395̲	59 428	40 572	99 967	45
16	59 715	59 749	40 251	99 966	44
17	60 033	60 068	39 932	99 966	43
18	60 349	60 384	39 616	99 965̲	42
19	60 662	60 698	39 302	99 964	41
20	60 973	61 009	38 991	99 964	40
21	61 282	61 319	38 681	99 963	39
22	61 589	61 626	38 374	99 963	38
23	61 894	61 931	38 069	99 962	37
24	62 196	62 234	37 766	99 962	36
25	62 497	62 535	37 465̲	99 961	35
26	62 795̲	62 834	37 166	99 961	34
27	63 091	63 131	36 869	99 960	33
28	63 385	63 426	36 574	99 960	32
29	63 678	63 718	36 282	99 959	31
30	63 968	64 009	35 991	99 959	30
31	64 256	64 298	35 702	99 958	29
32	64 543	64 585	35 415̲	99 958	28
33	64 827	64 870	35 130	99 957	27
34	65 110	65 154	34 846	99 956	26
35	65 391	65 435	34 565̲	99 956	25
36	65 670	65 715̲	34 285	99 955	24
37	65 947	65 993	34 007	99 955̲	23
38	66 223	66 269	33 731	99 954	22
39	66 497	66 543	33 457	99 954	21
40	66 769	66 816	33 184	99 953	20
41	67 039	67 087	32 913	99 952	19
42	67 308	67 356	32 644	99 952	18
43	67 575	67 624	32 376	99 951	17
44	67 841	67 890	32 110	99 951	16
45	68 104	68 154	31 846	99 95̲0	15
46	68 367	68 417	31 583	99 949	14
47	68 627	68 678	31 322	99 949	13
48	68 886	68 938	31 062	99 948	12
49	69 144	69 196	30 804	99 948	11
50	69 400	69 453	30 547	99 947	10
51	69 654	69 708	30 292	99 946	9
52	69 907	69 962	30 038	99 946	8
53	70 159	70 214	29 786	99 945̲	7
54	70 409	70 465̲	29 535	99 944	6
55	70 658	70 714	29 286	99 944	5
56	70 905̲	70 962	29 038	99 943	4
57	71 151	71 208	28 792	99 942	3
58	71 395	71 453	28 547	99 942	2
59	71 638	71 697	28 303	99 941	1
60	71 880	71 940	28 060	99 940	0
	8	8	11	9	
′	log cos	log cot	log tan	log sin	′

87°

3°

′	log sin	log tan	log cot	log cos	′
	8	8	11	9	
0	71 880	71 940	28 060	99 940	60
1	72 120	72 181	27 819	99 940	59
2	72 359	72 420	27 580	99 939	58
3	72 597	72 659	27 341	99 938	57
4	72 834	72 896	27 104	99 938	56
5	73 069	73 132	26 868	99 937	55
6	73 303	73 366	26 634	99 936	54
7	73 535	73 600	26 400	99 936	53
8	73 767	73 832	26 168	99 935	52
9	73 997	74 063	25 937	99 934	51
10	74 226	74 292	25 708	99 934	50
11	74 454	74 521	25 479	99 933	49
12	74 680	74 748	25 252	99 932	48
13	74 906	74 974	25 026	99 932	47
14	75 130	75 199	24 801	99 931	46
15	75 353	75 423	24 577	99 930	45
16	75 575	75 645	24 355	99 929	44
17	75 795	75 867	24 133	99 929	43
18	76 015	76 087	23 913	99 928	42
19	76 234	76 306	23 694	99 927	41
20	76 451	76 525	23 475	99 926	40
21	76 667	76 742	23 258	99 926	39
22	76 883	76 958	23 042	99 925	38
23	77 097	77 173	22 827	99 924	37
24	77 310	77 387	22 613	99 923	36
25	77 522	77 600	22 400	99 923	35
26	77 733	77 811	22 189	99 922	34
27	77 943	78 022	21 978	99 921	33
28	78 152	78 232	21 768	99 920	32
29	78 360	78 441	21 559	99 920	31
30	78 568	78 649	21 351	99 919	30
31	78 774	78 855	21 145	99 918	29
32	78 979	79 061	20 939	99 917	28
33	79 183	79 266	20 734	99 917	27
34	79 386	79 470	20 530	99 916	26
35	79 588	79 673	20 327	99 915	25
36	79 789	79 875	20 125	99 914	24
37	79 990	80 076	19 924	99 913	23
38	80 189	80 277	19 723	99 913	22
39	80 388	80 476	19 524	99 912	21
40	80 585	80 674	19 326	99 911	20
41	80 782	80 872	19 128	99 910	19
42	80 978	81 068	18 932	99 909	18
43	81 173	81 264	18 736	99 909	17
44	81 367	81 459	18 541	99 908	16
45	81 560	81 653	18 347	99 907	15
46	81 752	81 846	18 154	99 906	14
47	81 944	82 038	17 962	99 905	13
48	82 134	82 230	17 770	99 904	12
49	82 324	82 420	17 580	99 904	11
50	82 513	82 610	17 390	99 903	10
51	82 701	82 799	17 201	99 902	9
52	82 888	82 987	17 013	99 901	8
53	83 075	83 175	16 825	99 900	7
54	83 261	83 361	16 639	99 899	6
55	83 446	83 547	16 453	99 898	5
56	83 630	83 732	16 268	99 898	4
57	83 813	83 916	16 084	99 897	3
58	83 996	84 100	15 900	99 896	2
59	84 177	84 282	15 718	99 895	1
60	84 358	84 464	15 536	99 894	0
	8	8	11	9	
′	log cos	log cot	log tan	log sin	′

86°

4°

′	log sin	log tan	log cot	log cos	′
	8	8	11	9	
0	84 358	84 464	15 536	99 894	60
1	84 539	84 646	15 354	99 893	59
2	84 718	84 826	15 174	99 892	58
3	84 897	85 006	14 994	99 891	57
4	85 075	85 185	14 815	99 891	56
5	85 252	85 363	14 637	99 890	55
6	85 429	85 540	14 460	99 889	54
7	85 605	85 717	14 283	99 888	53
8	85 780	85 893	14 107	99 887	52
9	85 955	86 069	13 931	99 886	51
10	86 128	86 243	13 757	99 885	50
11	86 301	86 417	13 583	99 884	49
12	86 474	86 591	13 409	99 883	48
13	86 645	86 763	13 237	99 882	47
14	86 816	86 935	13 065	99 881	46
15	86 987	87 106	12 894	99 880	45
16	87 156	87 277	12 723	99 879	44
17	87 325	87 447	12 553	99 879	43
18	87 494	87 616	12 384	99 878	42
19	87 661	87 785	12 215	99 877	41
20	87 829	87 953	12 047	99 876	40
21	87 995	88 120	11 880	99 875	39
22	88 161	88 287	11 713	99 874	38
23	88 326	88 453	11 547	99 873	37
24	88 490	88 618	11 382	99 872	36
25	88 654	88 783	11 217	99 871	35
26	88 817	88 948	11 052	99 870	34
27	88 980	89 111	10 889	99 869	33
28	89 142	89 274	10 726	99 868	32
29	89 304	89 437	10 563	99 867	31
30	89 464	89 598	10 402	99 866	30
31	89 625	89 760	10 240	99 865	29
32	89 784	89 920	10 080	99 864	28
33	89 943	90 080	09 920	99 863	27
34	90 102	90 240	09 760	99 862	26
35	90 260	90 399	09 601	99 861	25
36	90 417	90 557	09 443	99 860	24
37	90 574	90 715	09 285	99 859	23
38	90 730	90 872	09 128	99 858	22
39	90 885	91 029	08 971	99 857	21
40	91 040	91 185	08 815	99 856	20
41	91 195	91 340	08 660	99 855	19
42	91 349	91 495	08 505	99 854	18
43	91 502	91 650	08 350	99 853	17
44	91 655	91 803	08 197	99 852	16
45	91 807	91 957	08 043	99 851	15
46	91 959	92 110	07 890	99 850	14
47	92 110	92 262	07 738	99 848	13
48	92 261	92 414	07 586	99 847	12
49	92 411	92 565	07 435	99 846	11
50	92 561	92 716	07 284	99 845	10
51	92 710	92 866	07 134	99 844	9
52	92 859	93 016	06 984	99 843	8
53	93 007	93 165	06 835	99 842	7
54	93 154	93 313	06 687	99 841	6
55	93 301	93 462	06 538	99 840	5
56	93 448	93 609	06 391	99 839	4
57	93 594	93 756	06 244	99 838	3
58	93 740	93 903	06 097	99 837	2
59	93 885	94 049	05 951	99 836	1
60	94 030	94 195	05 805	99 834	0
	8	8	11	9	
′	log cos	log cot	log tan	log sin	′

85°

5°

′	log sin	log tan	log cot	log cos	′
	—8—	—8—	—11—	—9—	
0	94 030	94 195	05 805̲	99 834	60
1	94 174	94 340	05 660	99 833	59
2	94 317	94 485	05 515̲	99 832	58
3	94 461	94 630	05 370	99 831	57
4	94 603	94 773	05 227	99 830	56
5	94 746	94 917	05 083	99 829	55
6	94 887	95 060	04 940	99 828	54
7	95 029	95 202	04 798	99 827	53
8	95 170	95 344	04 656	99 825	52
9	95 310	95 486	04 514	99 824	51
10	95 45̲0	95 627	04 373	99 823	50
11	95 589	95 767	04 233	99 822	49
12	95 728	95 908	04 092	99 821	48
13	95 867	96 047	03 953	99 820	47
14	96 005	96 187	03 813	99 819	46
15	96 143	96 325	03 675̲	99 817	45
16	96 280	96 464	03 536	99 816	44
17	96 417	96 602	03 398	99 815	43
18	96 553	96 739	03 261	99 814	42
19	96 689	96 877	03 123	99 813	41
20	96 825̲	97 013	02 987	99 812	40
21	96 960	97 15̲0	02 850	99 810	39
22	97 095̲	97 285	02 715̲	99 809	38
23	97 229	97 421	02 579	99 808	37
24	97 363	97 556	02 444	99 807	36
25	97 496	97 691	02 309	99 806	35
26	97 629	97 825̲	02 175	99 804	34
27	97 762	97 959	02 041	99 803	33
28	97 894	98 092	01 908	99 802	32
29	98 026	98 225	01 775̲	99 801	31
30	98 157	98 358	01 642	99 800	30
31	98 288	98 490	01 510	99 798	29
32	98 419	98 622	01 378	99 797	28
33	98 549	98 753	01 247	99 796	27
34	98 679	98 884	01 116	99 795̲	26
35	98 808	99 015̲	00 985	99 793	25
36	98 937	99 145	00 855̲	99 792	24
37	99 066	99 275	00 725̲	99 791	23
38	99 194	99 405̲	00 595	99 790	22
39	99 322	99 534	00 466	99 788	21
40	99 45̲0	99 662	00 338	99 787	20
41	99 577	99 791	00 209	99 786	19
42	99 704	99 919	00 081	99 785̲	18
43	99 830	00 046	99 954	99 783	17
44	99 956	00 174	99 826	99 782	16
45	00 082	00 301	99 699	99 781	15
46	00 207	00 427	99 573	99 780	14
47	00 332	00 553	99 447	99 778	13
48	00 456	00 679	99 321	99 777	12
49	00 581	00 805̲	99 195	99 776	11
50	00 704	00 930	99 070	99 775̲	10
51	00 828	01 055̲	98 945	99 773	9
52	00 951	01 179	98 821	99 772	8
53	01 074	01 303	98 697	99 771	7
54	01 196	01 427	98 573	99 769	6
55	01 318	01 550	98 45̲0	99 768	5
56	01 440	01 673	98 327	99 767	4
57	01 561	01 796	98 204	99 765	3
58	01 682	01 918	98 082	99 764	2
59	01 803	02 040	97 960	99 763	1
60	01 923	02 162	97 838	99 761	0
	—9—	—9—	—10—	—9—	
′	log cos	log cot	log tan	log sin	′

84°

6°

′	log sin	log tan	log cot	log cos	′
	—9—	—9—	—10—	—9—	
0	01 923	02 162	97 838	99 761	60
1	02 043	02 283	97 717	99 760	59
2	02 163	02 404	97 596	99 759	58
3	02 283	02 525	97 475̲	99 757	57
4	02 402	02 645	97 355̲	99 756	56
5	02 520	02 766	97 234	99 755̲	55
6	02 639	02 885	97 115̲	99 753	54
7	02 757	03 005̲	96 995	99 752	53
8	02 874	03 124	96 876	99 751	52
9	02 992	03 242	96 758	99 749	51
10	03 109	03 361	96 639	99 748	50
11	03 226	03 479	96 521	99 747	49
12	03 342	03 597	96 403	99 745	48
13	03 458	03 714	96 286	99 744	47
14	03 574	03 832	96 168	99 742	46
15	03 690	03 948	96 052	99 741	45
16	03 805̲	04 065	95 935̲	99 740	44
17	03 920	04 181	95 819	99 738	43
18	04 034	04 297	95 703	99 737	42
19	04 149	04 413	95 587	99 736	41
20	04 262	04 528	95 472	99 734	40
21	04 376	04 643	95 357	99 733	39
22	04 490	04 758	95 242	99 731	38
23	04 603	04 873	95 127	99 730	37
24	04 715	04 987	95 013	99 728	36
25	04 828	05 101	94 899	99 727	35
26	04 940	05 214	94 786	99 726	34
27	05 052	05 328	94 672	99 724	33
28	05 164	05 441	94 559	99 723	32
29	05 275̲	05 553	94 447	99 721	31
30	05 386	05 666	94 334	99 720	30
31	05 497	05 778	94 222	99 718	29
32	05 607	05 890	94 110	99 717	28
33	05 717	06 002	93 998	99 716	27
34	05 827	06 113	93 887	99 714	26
35	05 937	06 224	93 776	99 713	25
36	06 046	06 335̲	93 665	99 711	24
37	06 155	06 445	93 555̲	99 710	23
38	06 264	06 556	93 444	99 708	22
39	06 372	06 666	93 334	99 707	21
40	06 481	06 775	93 225̲	99 705	20
41	06 589	06 885̲	93 115	99 704	19
42	06 696	06 994	93 006	99 702	18
43	06 804	07 103	92 897	99 701	17
44	06 911	07 211	92 789	99 699	16
45	07 018	07 320	92 680	99 698	15
46	07 124	07 428	92 572	99 696	14
47	07 231	07 536	92 464	99 695̲	13
48	07 337	07 643	92 357	99 693	12
49	07 442	07 751	92 249	99 692	11
50	07 548	07 858	92 142	99 690	10
51	07 653	07 964	92 036	99 689	9
52	07 758	08 071	91 929	99 687	8
53	07 863	08 177	91 823	99 686	7
54	07 968	08 283	91 717	99 684	6
55	08 072	08 389	91 611	99 683	5
56	08 176	08 495̲	91 505	99 681	4
57	08 280	08 600	91 400	99 680	3
58	08 383	08 705	91 295̲	99 678	2
59	08 486	08 810	91 190	99 677	1
60	08 589	08 914	91 086	99 675	0
	—9—	—9—	—10—	—9—	
′	log cos	log cot	log tan	log sin	′

83°

7°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	08 589	08 914	91 086	99 675	60
1	08 692	09 019	90 981	99 674	59
2	08 795	09 123	90 877	99 672	58
3	08 897	09 227	90 773	99 670	57
4	08 999	09 330	90 670	99 669	56
5	09 101	09 434	90 566	99 667	55
6	09 202	09 537	90 463	99 666	54
7	09 304	09 640	90 360	99 664	53
8	09 405	09 742	90 258	99 663	52
9	09 506	09 845	90 155	99 661	51
10	09 606	09 947	90 053	99 659	50
11	09 707	10 049	89 951	99 658	49
12	09 807	10 150	89 850	99 656	48
13	09 907	10 252	89 748	99 655	47
14	10 006	10 353	89 647	99 653	46
15	10 106	10 454	89 546	99 651	45
16	10 205	10 555	89 445	99 650	44
17	10 304	10 656	89 344	99 648	43
18	10 402	10 756	89 244	99 647	42
19	10 501	10 856	89 144	99 645	41
20	10 599	10 956	89 044	99 643	40
21	10 697	11 056	88 944	99 642	39
22	10 795	11 155	88 845	99 640	38
23	10 893	11 254	88 746	99 638	37
24	10 990	11 353	88 647	99 637	36
25	11 087	11 452	88 548	99 635	35
26	11 184	11 551	88 449	99 633	34
27	11 281	11 649	88 351	99 632	33
28	11 377	11 747	88 253	99 630	32
29	11 474	11 845	88 155	99 629	31
30	11 570	11 943	88 057	99 627	30
31	11 666	12 040	87 960	99 625	29
32	11 761	12 138	87 862	99 624	28
33	11 857	12 235	87 765	99 622	27
34	11 952	12 332	87 668	99 620	26
35	12 047	12 428	87 572	99 618	25
36	12 142	12 525	87 475	99 617	24
37	12 236	12 621	87 379	99 615	23
38	12 331	12 717	87 283	99 613	22
39	12 425	12 813	87 187	99 612	21
40	12 519	12 909	87 091	99 610	20
41	12 612	13 004	86 996	99 608	19
42	12 706	13 099	86 901	99 607	18
43	12 799	13 194	86 806	99 605	17
44	12 892	13 289	86 711	99 603	16
45	12 985	13 384	86 616	99 601	15
46	13 078	13 478	86 522	99 600	14
47	13 171	13 573	86 427	99 598	13
48	13 263	13 667	86 333	99 596	12
49	13 355	13 761	86 239	99 595	11
50	13 447	13 854	86 146	99 593	10
51	13 539	13 948	86 052	99 591	9
52	13 630	14 041	85 959	99 589	8
53	13 722	14 134	85 866	99 588	7
54	13 813	14 227	85 773	99 586	6
55	13 904	14 320	85 680	99 584	5
56	13 994	14 412	85 588	99 582	4
57	14 085	14 504	85 496	99 581	3
58	14 175	14 597	85 403	99 579	2
59	14 266	14 688	85 312	99 577	1
60	14 356	14 780	85 220	99 575	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

82°

8°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	14 356	14 780	85 220	99 575	60
1	14 445	14 872	85 128	99 574	59
2	14 535	14 963	85 037	99 572	58
3	14 624	15 054	84 946	99 570	57
4	14 714	15 145	84 855	99 568	56
5	14 803	15 236	84 764	99 566	55
6	14 891	15 327	84 673	99 565	54
7	14 980	15 417	84 583	99 563	53
8	15 069	15 508	84 492	99 561	52
9	15 157	15 598	84 402	99 559	51
10	15 245	15 688	84 312	99 557	50
11	15 333	15 777	84 223	99 556	49
12	15 421	15 867	84 133	99 554	48
13	15 508	15 956	84 044	99 552	47
14	15 596	16 046	83 954	99 550	46
15	15 683	16 135	83 865	99 548	45
16	15 770	16 224	83 776	99 546	44
17	15 857	16 312	83 688	99 545	43
18	15 944	16 401	83 599	99 543	42
19	16 030	16 489	83 511	99 541	41
20	16 116	16 577	83 423	99 539	40
21	16 203	16 665	83 335	99 537	39
22	16 289	16 753	83 247	99 535	38
23	16 374	16 841	83 159	99 533	37
24	16 460	16 928	83 072	99 532	36
25	16 545	17 016	82 984	99 530	35
26	16 631	17 103	82 897	99 528	34
27	16 716	17 190	82 810	99 526	33
28	16 801	17 277	82 723	99 524	32
29	16 886	17 363	82 637	99 522	31
30	16 970	17 450	82 550	99 520	30
31	17 055	17 536	82 464	99 518	29
32	17 139	17 622	82 378	99 517	28
33	17 223	17 708	82 292	99 515	27
34	17 307	17 794	82 206	99 513	26
35	17 391	17 880	82 120	99 511	25
36	17 474	17 965	82 035	99 509	24
37	17 558	18 051	81 949	99 507	23
38	17 641	18 136	81 864	99 505	22
39	17 724	18 221	81 779	99 503	21
40	17 807	18 306	81 694	99 501	20
41	17 890	18 391	81 609	99 499	19
42	17 973	18 475	81 525	99 497	18
43	18 055	18 560	81 440	99 495	17
44	18 137	18 644	81 356	99 494	16
45	18 220	18 728	81 272	99 492	15
46	18 302	18 812	81 188	99 490	14
47	18 383	18 896	81 104	99 488	13
48	18 465	18 979	81 021	99 486	12
49	18 547	19 063	80 937	99 484	11
50	18 628	19 146	80 854	99 482	10
51	18 709	19 229	80 771	99 480	9
52	18 790	19 312	80 688	99 478	8
53	18 871	19 395	80 605	99 476	7
54	18 952	19 478	80 522	99 474	6
55	19 033	19 561	80 439	99 472	5
56	19 113	19 643	80 357	99 470	4
57	19 193	19 725	80 275	99 468	3
58	19 273	19 807	80 193	99 466	2
59	19 353	19 889	80 111	99 464	1
60	19 433	19 971	80 029	99 462	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

81°

9°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	19 433	19 971	80 029	99 462	60
1	19 513	20 053	79 947	99 460	59
2	19 592	20 134	79 866	99 458	58
3	19 672	20 216	79 784	99 456	57
4	19 751	20 297	79 703	99 454	56
5	19 830	20 378	79 622	99 452	55
6	19 909	20 459	79 541	99 450	54
7	19 988	20 540	79 460	99 448	53
8	20 067	20 621	79 379	99 446	52
9	20 145	20 701	79 299	99 444	51
10	20 223	20 782	79 218	99 442	50
11	20 302	20 862	79 138	99 440	49
12	20 380	20 942	79 058	99 438	48
13	20 458	21 022	78 978	99 436	47
14	20 535	21 102	78 898	99 434	46
15	20 613	21 182	78 818	99 432	45
16	20 691	21 261	78 739	99 429	44
17	20 768	21 341	78 659	99 427	43
18	20 845	21 420	78 580	99 425	42
19	20 922	21 499	78 501	99 423	41
20	20 999	21 578	78 422	99 421	40
21	21 076	21 657	78 343	99 419	39
22	21 153	21 736	78 264	99 417	38
23	21 229	21 814	78 186	99 415	37
24	21 306	21 893	78 107	99 413	36
25	21 382	21 971	78 029	99 411	35
26	21 458	22 049	77 951	99 409	34
27	21 534	22 127	77 873	99 407	33
28	21 610	22 205	77 795	99 404	32
29	21 685	22 283	77 717	99 402	31
30	21 761	22 361	77 639	99 400	30
31	21 836	22 438	77 562	99 398	29
32	21 912	22 516	77 484	99 396	28
33	21 987	22 593	77 407	99 394	27
34	22 062	22 670	77 330	99 392	26
35	22 137	22 747	77 253	99 390	25
36	22 211	22 824	77 176	99 388	24
37	22 286	22 901	77 099	99 385	23
38	22 361	22 977	77 023	99 383	22
39	22 435	23 054	76 946	99 381	21
40	22 509	23 130	76 870	99 379	20
41	22 583	23 206	76 794	99 377	19
42	22 657	23 283	76 717	99 375	18
43	22 731	23 359	76 641	99 372	17
44	22 805	23 435	76 565	99 370	16
45	22 878	23 510	76 490	99 368	15
46	22 952	23 586	76 414	99 366	14
47	23 025	23 661	76 339	99 364	13
48	23 098	23 737	76 263	99 362	12
49	23 171	23 812	76 188	99 359	11
50	23 244	23 887	76 113	99 357	10
51	23 317	23 962	76 038	99 355	9
52	23 390	24 037	75 963	99 353	8
53	23 462	24 112	75 888	99 351	7
54	23 535	24 186	75 814	99 348	6
55	23 607	24 261	75 739	99 346	5
56	23 679	24 335	75 665	99 344	4
57	23 752	24 410	75 590	99 342	3
58	23 823	24 484	75 516	99 340	2
59	23 895	24 558	75 442	99 337	1
60	23 967	24 632	75 368	99 335	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

80°

10°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	23 967	24 632	75 368	99 335	60
1	24 039	24 706	75 294	99 333	59
2	24 110	24 779	75 221	99 331	58
3	24 181	24 853	75 147	99 328	57
4	24 253	24 926	75 074	99 326	56
5	24 324	25 000	75 000	99 324	55
6	24 395	25 073	74 927	99 322	54
7	24 466	25 146	74 854	99 319	53
8	24 536	25 219	74 781	99 317	52
9	24 607	25 292	74 708	99 315	51
10	24 677	25 365	74 635	99 313	50
11	24 748	25 437	74 563	99 310	49
12	24 818	25 510	74 490	99 308	48
13	24 888	25 582	74 418	99 306	47
14	24 958	25 655	74 345	99 304	46
15	25 028	25 727	74 273	99 301	45
16	25 098	25 799	74 201	99 299	44
17	25 168	25 871	74 129	99 297	43
18	25 237	25 943	74 057	99 294	42
19	25 307	26 015	73 985	99 292	41
20	25 376	26 086	73 914	99 290	40
21	25 445	26 158	73 842	99 288	39
22	25 514	26 229	73 771	99 285	38
23	25 583	26 301	73 699	99 283	37
24	25 652	26 372	73 628	99 281	36
25	25 721	26 443	73 557	99 278	35
26	25 790	26 514	73 486	99 276	34
27	25 858	26 585	73 415	99 274	33
28	25 927	26 655	73 345	99 271	32
29	25 995	26 726	73 274	99 269	31
30	26 063	26 797	73 203	99 267	30
31	26 131	26 867	73 133	99 264	29
32	26 199	26 937	73 063	99 262	28
33	26 267	27 008	72 992	99 260	27
34	26 335	27 078	72 922	99 257	26
35	26 403	27 148	72 852	99 255	25
36	26 470	27 218	72 782	99 252	24
37	26 538	27 288	72 712	99 250	23
38	26 605	27 357	72 643	99 248	22
39	26 672	27 427	72 573	99 245	21
40	26 739	27 496	72 504	99 243	20
41	26 806	27 566	72 434	99 241	19
42	26 873	27 635	72 365	99 238	18
43	26 940	27 704	72 296	99 236	17
44	27 007	27 773	72 227	99 233	16
45	27 073	27 842	72 158	99 231	15
46	27 140	27 911	72 089	99 229	14
47	27 206	27 980	72 020	99 226	13
48	27 273	28 049	71 951	99 224	12
49	27 339	28 117	71 883	99 221	11
50	27 405	28 186	71 814	99 219	10
51	27 471	28 254	71 746	99 217	9
52	27 537	28 323	71 677	99 214	8
53	27 602	28 391	71 609	99 212	7
54	27 668	28 459	71 541	99 209	6
55	27 734	28 527	71 473	99 207	5
56	27 799	28 595	71 405	99 204	4
57	27 864	28 662	71 338	99 202	3
58	27 930	28 730	71 270	99 200	2
59	27 995	28 798	71 202	99 197	1
60	28 060	28 865	71 135	99 195	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

79°

11°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	28 060	28 865	71 135	99 195	60
1	28 125	28 933	71 067	99 192	59
2	28 190	29 000	71 000	99 190	58
3	28 254	29 067	70 933	99 187	57
4	28 319	29 134	70 866	99 185	56
5	28 384	29 201	70 799	99 182	55
6	28 448	29 268	70 732	99 180	54
7	28 512	29 335	70 665	99 177	53
8	28 577	29 402	70 598	99 175	52
9	28 641	29 468	70 532	99 172	51
10	28 705	29 535	70 465	99 170	50
11	28 769	29 601	70 399	99 167	49
12	28 833	29 668	70 332	99 165	48
13	28 896	29 734	70 266	99 162	47
14	28 960	29 800	70 200	99 160	46
15	29 024	29 866	70 134	99 157	45
16	29 087	29 932	70 068	99 155	44
17	29 150	29 998	70 002	99 152	43
18	29 214	30 064	69 936	99 150	42
19	29 277	30 130	69 870	99 147	41
20	29 340	30 195	69 805	99 145	40
21	29 403	30 261	69 739	99 142	39
22	29 466	30 326	69 674	99 140	38
23	29 529	30 391	69 609	99 137	37
24	29 591	30 457	69 543	99 135	36
25	29 654	30 522	69 478	99 132	35
26	29 716	30 587	69 413	99 130	34
27	29 779	30 652	69 348	99 127	33
28	29 841	30 717	69 283	99 124	32
29	29 903	30 782	69 218	99 122	31
30	29 966	30 846	69 154	99 119	30
31	30 028	30 911	69 089	99 117	29
32	30 090	30 975	69 025	99 114	28
33	30 151	31 040	68 960	99 112	27
34	30 213	31 104	68 896	99 109	26
35	30 275	31 168	68 832	99 106	25
36	30 336	31 233	68 767	99 104	24
37	30 398	31 297	68 703	99 101	23
38	30 459	31 361	68 639	99 099	22
39	30 521	31 425	68 575	99 096	21
40	30 582	31 489	68 511	99 093	20
41	30 643	31 552	68 448	99 091	19
42	30 704	31 616	68 384	99 088	18
43	30 765	31 679	68 321	99 086	17
44	30 826	31 743	68 257	99 083	16
45	30 887	31 806	68 194	99 080	15
46	30 947	31 870	68 130	99 078	14
47	31 008	31 933	68 067	99 075	13
48	31 068	31 996	68 004	99 072	12
49	31 129	32 059	67 941	99 070	11
50	31 189	32 122	67 878	99 067	10
51	31 250	32 185	67 815	99 064	9
52	31 310	32 248	67 752	99 062	8
53	31 370	32 311	67 689	99 059	7
54	31 430	32 373	67 627	99 056	6
55	31 490	32 436	67 564	99 054	5
56	31 549	32 498	67 502	99 051	4
57	31 609	32 561	67 439	99 048	3
58	31 669	32 623	67 377	99 046	2
59	31 728	32 685	67 315	99 043	1
60	31 788	32 747	67 253	99 040	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

78°

12°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	31 788	32 747	67 253	99 040	60
1	31 847	32 810	67 190	99 038	59
2	31 907	32 872	67 128	99 035	58
3	31 966	32 933	67 067	99 032	57
4	32 025	32 995	67 005	99 030	56
5	32 084	33 057	66 943	99 027	55
6	32 143	33 119	66 881	99 024	54
7	32 202	33 180	66 820	99 022	53
8	32 261	33 242	66 758	99 019	52
9	32 319	33 303	66 697	99 016	51
10	32 378	33 365	66 635	99 013	50
11	32 437	33 426	66 574	99 011	49
12	32 495	33 487	66 513	99 008	48
13	32 553	33 548	66 452	99 005	47
14	32 612	33 609	66 391	99 002	46
15	32 670	33 670	66 330	99 000	45
16	32 728	33 731	66 269	98 997	44
17	32 786	33 792	66 208	98 994	43
18	32 844	33 853	66 147	98 991	42
19	32 902	33 913	66 087	98 989	41
20	32 960	33 974	66 026	98 986	40
21	33 018	34 034	65 966	98 983	39
22	33 075	34 095	65 905	98 980	38
23	33 133	34 155	65 845	98 978	37
24	33 190	34 215	65 785	98 975	36
25	33 248	34 276	65 724	98 972	35
26	33 305	34 336	65 664	98 969	34
27	33 362	34 396	65 604	98 967	33
28	33 420	34 456	65 544	98 964	32
29	33 477	34 516	65 484	98 961	31
30	33 534	34 576	65 424	98 958	30
31	33 591	34 635	65 365	98 955	29
32	33 647	34 695	65 305	98 953	28
33	33 704	34 755	65 245	98 950	27
34	33 761	34 814	65 186	98 947	26
35	33 818	34 874	65 126	98 944	25
36	33 874	34 933	65 067	98 941	24
37	33 931	34 992	65 008	98 938	23
38	33 987	35 051	64 949	98 936	22
39	34 043	35 111	64 889	98 933	21
40	34 100	35 170	64 830	98 930	20
41	34 156	35 229	64 771	98 927	19
42	34 212	35 288	64 712	98 924	18
43	34 268	35 347	64 653	98 921	17
44	34 324	35 405	64 595	98 919	16
45	34 380	35 464	64 536	98 916	15
46	34 436	35 523	64 477	98 913	14
47	34 491	35 581	64 419	98 910	13
48	34 547	35 640	64 360	98 907	12
49	34 602	35 698	64 302	98 904	11
50	34 658	35 757	64 243	98 901	10
51	34 713	35 815	64 185	98 898	9
52	34 769	35 873	64 127	98 896	8
53	34 824	35 931	64 069	98 893	7
54	34 879	35 989	64 011	98 890	6
55	34 934	36 047	63 953	98 887	5
56	34 989	36 105	63 895	98 884	4
57	35 044	36 163	63 837	98 881	3
58	35 099	36 221	63 779	98 878	2
59	35 154	36 279	63 721	98 875	1
60	35 209	36 336	63 664	98 872	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

77°

13°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	35 209	36 336	63 664	98 872	60
1	35 263	36 394	63 606	98 869	59
2	35 318	36 452	63 548	98 867	58
3	35 373	36 509	63 491	98 864	57
4	35 427	36 566	63 434	98 861	56
5	35 481	36 624	63 376	98 858	55
6	35 536	36 681	63 319	98 855̲	54
7	35 590	36 738	63 262	98 852	53
8	35 644	36 795	63 205̲	98 849	52
9	35 698	36 852	63 148	98 846	51
10	35 752	36 909	63 091	98 843	50
11	35 806	36 966	63 034	98 840	49
12	35 860	37 023	62 977	98 837	48
13	35 914	37 080	62 920	98 834	47
14	35 968	37 137	62 863	98 831	46
15	36 022	37 193	62 807	98 828	45
16	36 075	37 25̲0	62 750	98 825	44
17	36 129	37 306	62 694	98 822	43
18	36 182	37 363	62 637	98 819	42
19	36 236	37 419	62 581	98 816	41
20	36 289	37 476	62 524	98 813	40
21	36 342	37 532	62 468	98 810	39
22	36 395	37 588	62 412	98 807	38
23	36 449	37 644	62 356	98 804	37
24	36 502	37 700	62 300	98 801	36
25	36 555̲	37 756	62 244	98 798	35
26	36 608	37 812	62 188	98 795	34
27	36 660	37 868	62 132	98 792	33
28	36 713	37 924	62 076	98 789	32
29	36 766	37 980	62 020	98 786	31
30	36 819	38 035	61 965̲	98 783	30
31	36 871	38 091	61 909	98 780	29
32	36 924	38 147	61 853	98 777	28
33	36 976	38 202	61 798	98 774	27
34	37 028	38 257	61 743	98 771	26
35	37 081	38 313	61 687	98 768	25
36	37 133	38 368	61 632	98 765̲	24
37	37 185	38 423	61 577	98 762	23
38	37 237	38 479	61 521	98 759	22
39	37 289	38 534	61 466	98 756	21
40	37 341	38 589	61 411	98 753	20
41	37 393	38 644	61 356	98 75̲0	19
42	37 445	38 699	61 301	98 746	18
43	37 497	38 754	61 246	98 743	17
44	37 549	38 808	61 192	98 740	16
45	37 600	38 863	61 137	98 737	15
46	37 652	38 918	61 082	98 734	14
47	37 703	38 972	61 028	98 731	13
48	37 755̲	39 027	60 973	98 728	12
49	37 806	39 082	60 918	98 725̲	11
50	37 858	39 136	60 864	98 722	10
51	37 909	39 190	60 810	98 719	9
52	37 960	39 245̲	60 755	98 715	8
53	38 011	39 299	60 701	98 712	7
54	38 062	39 353	60 647	98 709	6
55	38 113	39 407	60 593	98 706	5
56	38 164	39 461	60 539	98 703	4
57	38 215	39 515	60 485̲	98 700	3
58	38 266	39 569	60 431	98 697	2
59	38 317	39 623	60 377	98 694	1
60	38 368	39 677	60 323	98 690	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

76°

14°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	38 368	39 677	60 323	98 690	60
1	38 418	39 731	60 269	98 687	59
2	38 469	39 785̲	60 215	98 684	58
3	38 519	39 838	60 162	98 681	57
4	38 570	39 892	60 108	98 678	56
5	38 620	39 945	60 055̲	98 675̲	55
6	38 670	39 999	60 001	98 671	54
7	38 721	40 052	59 948	98 668	53
8	38 771	40 106	59 894	98 665	52
9	38 821	40 159	59 841	98 662	51
10	38 871	40 212	59 788	98 659	50
11	38 921	40 266	59 734	98 656	49
12	38 971	40 319	59 681	98 652	48
13	39 021	40 372	59 628	98 649	47
14	39 071	40 425̲	59 575	98 646	46
15	39 121	40 478	59 522	98 643	45
16	39 170	40 531	59 469	98 640	44
17	39 220	40 584	59 416	98 636	43
18	39 270	40 636	59 364	98 633	42
19	39 319	40 689	59 311	98 630	41
20	39 369	40 742	59 258	98 627	40
21	39 418	40 795̲	59 205	98 623	39
22	39 467	40 847	59 153	98 620	38
23	39 517	40 900	59 100	98 617	37
24	39 566	40 952	59 048	98 614	36
25	39 615̲	41 005̲	58 995	98 610	35
26	39 664	41 057	58 943	98 607	34
27	39 713	41 109	58 891	98 604	33
28	39 762	41 161	58 839	98 601	32
29	39 811	41 214	58 786	98 597	31
30	39 860	41 266	58 734	98 594	30
31	39 909	41 318	58 682	98 591	29
32	39 958	41 370	58 630	98 588	28
33	40 006	41 422	58 578	98 584	27
34	40 055̲	41 474	58 526	98 581	26
35	40 103	41 526	58 474	98 578	25
36	40 152	41 578	58 422	98 574	24
37	40 200	41 629	58 371	98 571	23
38	40 249	41 681	58 319	98 568	22
39	40 297	41 733	58 267	98 565̲	21
40	40 346	41 784	58 216	98 561	20
41	40 394	41 836	58 164	98 558	19
42	40 442	41 887	58 113	98 555̲	18
43	40 490	41 939	58 061	98 551	17
44	40 538	41 990	58 010	98 548	16
45	40 586	42 041	57 959	98 545̲	15
46	40 634	42 093	57 907	98 541	14
47	40 682	42 144	57 856	98 538	13
48	40 730	42 195	57 805̲	98 535̲	12
49	40 778	42 246	57 754	98 531	11
50	40 825	42 297	57 703	98 528	10
51	40 873	42 348	57 652	98 525̲	9
52	40 921	42 399	57 601	98 521	8
53	40 968	42 450	57 55̲0	98 518	7
54	41 016	42 501	57 499	98 515̲	6
55	41 063	42 552	57 448	98 511	5
56	41 111	42 603	57 397	98 508	4
57	41 158	42 653	57 347	98 505̲	3
58	41 205	42 704	57 296	98 501	2
59	41 252	42 755̲	57 245	98 498	1
60	41 300	42 805	57 195̲	98 494	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

75°

15°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	41 300	42 805	57 195	98 494	60
1	41 347	42 856	57 144	98 491	59
2	41 394	42 906	57 094	98 488	58
3	41 441	42 957	57 043	98 484	57
4	41 488	43 007	56 993	98 481	56
5	41 535	43 057	56 943	98 477	55
6	41 582	43 108	56 892	98 474	54
7	41 628	43 158	56 842	98 471	53
8	41 675	43 208	56 792	98 467	52
9	41 722	43 258	56 742	98 464	51
10	41 768	43 308	56 692	98 460	50
11	41 815	43 358	56 642	98 457	49
12	41 861	43 408	56 592	98 453	48
13	41 908	43 458	56 542	98 450	47
14	41 954	43 508	56 492	98 447	46
15	42 001	43 558	56 442	98 443	45
16	42 047	43 607	56 393	98 440	44
17	42 093	43 657	56 343	98 436	43
18	42 140	43 707	56 293	98 433	42
19	42 186	43 756	56 244	98 429	41
20	42 232	43 806	56 194	98 426	40
21	42 278	43 855	56 145	98 422	39
22	42 324	43 905	56 095	98 419	38
23	42 370	43 954	56 046	98 415	37
24	42 416	44 004	55 996	98 412	36
25	42 461	44 053	55 947	98 409	35
26	42 507	44 102	55 898	98 405	34
27	42 553	44 151	55 849	98 402	33
28	42 599	44 201	55 799	98 398	32
29	42 644	44 250	55 750	98 395	31
30	42 690	44 299	55 701	98 391	30
31	42 735	44 348	55 652	98 388	29
32	42 781	44 397	55 603	98 384	28
33	42 826	44 446	55 554	98 381	27
34	42 872	44 495	55 505	98 377	26
35	42 917	44 544	55 456	98 373	25
36	42 962	44 592	55 408	98 370	24
37	43 008	44 641	55 359	98 366	23
38	43 053	44 690	55 310	98 363	22
39	43 098	44 738	55 262	98 359	21
40	43 143	44 787	55 213	98 356	20
41	43 188	44 836	55 164	98 352	19
42	43 233	44 884	55 116	98 349	18
43	43 278	44 933	55 067	98 345	17
44	43 323	44 981	55 019	98 342	16
45	43 367	45 029	54 971	98 338	15
46	43 412	45 078	54 922	98 334	14
47	43 457	45 126	54 874	98 331	13
48	43 502	45 174	54 826	98 327	12
49	43 546	45 222	54 778	98 324	11
50	43 591	45 271	54 729	98 320	10
51	43 635	45 319	54 681	98 317	9
52	43 680	45 367	54 633	98 313	8
53	43 724	45 415	54 585	98 309	7
54	43 769	45 463	54 537	98 306	6
55	43 813	45 511	54 489	98 302	5
56	43 857	45 559	54 441	98 299	4
57	43 901	45 606	54 394	98 295	3
58	43 946	45 654	54 346	98 291	2
59	43 990	45 702	54 298	98 288	1
60	44 034	45 750	54 250	98 284	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

74°

16°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	44 034	45 750	54 250	98 284	60
1	44 078	45 797	54 203	98 281	59
2	44 122	45 845	54 155	98 277	58
3	44 166	45 892	54 108	98 273	57
4	44 210	45 940	54 060	98 270	56
5	44 253	45 987	54 013	98 266	55
6	44 297	46 035	53 965	98 262	54
7	44 341	46 082	53 918	98 259	53
8	44 385	46 130	53 870	98 255	52
9	44 428	46 177	53 823	98 251	51
10	44 472	46 224	53 776	98 248	50
11	44 516	46 271	53 729	98 244	49
12	44 559	46 319	53 681	98 240	48
13	44 602	46 366	53 634	98 237	47
14	44 646	46 413	53 587	98 233	46
15	44 689	46 460	53 540	98 229	45
16	44 733	46 507	53 493	98 226	44
17	44 776	46 554	53 446	98 222	43
18	44 819	46 601	53 399	98 218	42
19	44 862	46 648	53 352	98 215	41
20	44 905	46 694	53 306	98 211	40
21	44 948	46 741	53 259	98 207	39
22	44 992	46 788	53 212	98 204	38
23	45 035	46 835	53 165	98 200	37
24	45 077	46 881	53 119	98 196	36
25	45 120	46 928	53 072	98 192	35
26	45 163	46 975	53 025	98 189	34
27	45 206	47 021	52 979	98 185	33
28	45 249	47 068	52 932	98 181	32
29	45 292	47 114	52 886	98 177	31
30	45 334	47 160	52 840	98 174	30
31	45 377	47 207	52 793	98 170	29
32	45 419	47 253	52 747	98 166	28
33	45 462	47 299	52 701	98 162	27
34	45 504	47 346	52 654	98 159	26
35	45 547	47 392	52 608	98 155	25
36	45 589	47 438	52 562	98 151	24
37	45 632	47 484	52 516	98 147	23
38	45 674	47 530	52 470	98 144	22
39	45 716	47 576	52 424	98 140	21
40	45 758	47 622	52 378	98 136	20
41	45 801	47 668	52 332	98 132	19
42	45 843	47 714	52 286	98 129	18
43	45 885	47 760	52 240	98 125	17
44	45 927	47 806	52 194	98 121	16
45	45 969	47 852	52 148	98 117	15
46	46 011	47 897	52 103	98 113	14
47	46 053	47 943	52 057	98 110	13
48	46 095	47 989	52 011	98 106	12
49	46 136	48 035	51 965	98 102	11
50	46 178	48 080	51 920	98 098	10
51	46 220	48 126	51 874	98 094	9
52	46 262	48 171	51 829	98 090	8
53	46 303	48 217	51 783	98 087	7
54	46 345	48 262	51 738	98 083	6
55	46 386	48 307	51 693	98 079	5
56	46 428	48 353	51 647	98 075	4
57	46 469	48 398	51 602	98 071	3
58	46 511	48 443	51 557	98 067	2
59	46 552	48 489	51 511	98 063	1
60	46 594	48 534	51 466	98 060	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

73°

17°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	46 594	48 534	51 466	98 060	60
1	46 635	48 579	51 421	98 056	59
2	46 676	48 624	51 376	98 052	58
3	46 717	48 669	51 331	98 048	57
4	46 758	48 714	51 286	98 044	56
5	46 800	48 759	51 241	98 040	55
6	46 841	48 804	51 196	98 036	54
7	46 882	48 849	51 151	98 032	53
8	46 923	48 894	51 106	98 029	52
9	46 964	48 939	51 061	98 025	51
10	47 005	48 984	51 016	98 021	50
11	47 045	49 029	50 971	98 017	49
12	47 086	49 073	50 927	98 013	48
13	47 127	49 118	50 882	98 009	47
14	47 168	49 163	50 837	98 005	46
15	47 209	49 207	50 793	98 001	45
16	47 249	49 252	50 748	97 997	44
17	47 290	49 296	50 704	97 993	43
18	47 330	49 341	50 659	97 989	42
19	47 371	49 385	50 615	97 986	41
20	47 411	49 430	50 570	97 982	40
21	47 452	49 474	50 526	97 978	39
22	47 492	49 519	50 481	97 974	38
23	47 533	49 563	50 437	97 970	37
24	47 573	49 607	50 393	97 966	36
25	47 613	49 652	50 348	97 962	35
26	47 654	49 696	50 304	97 958	34
27	47 694	49 740	50 260	97 954	33
28	47 734	49 784	50 216	97 950	32
29	47 774	49 828	50 172	97 946	31
30	47 814	49 872	50 128	97 942	30
31	47 854	49 916	50 084	97 938	29
32	47 894	49 960	50 040	97 934	28
33	47 934	50 004	49 996	97 930	27
34	47 974	50 048	49 952	97 926	26
35	48 014	50 092	49 908	97 922	25
36	48 054	50 136	49 864	97 918	24
37	48 094	50 180	49 820	97 914	23
38	48 133	50 223	49 777	97 910	22
39	48 173	50 267	49 733	97 906	21
40	48 213	50 311	49 689	97 902	20
41	48 252	50 355	49 645	97 898	19
42	48 292	50 398	49 602	97 894	18
43	48 332	50 442	49 558	97 890	17
44	48 371	50 485	49 515	97 886	16
45	48 411	50 529	49 471	97 882	15
46	48 450	50 572	49 428	97 878	14
47	48 490	50 616	49 384	97 874	13
48	48 529	50 659	49 341	97 870	12
49	48 568	50 703	49 297	97 866	11
50	48 607	50 746	49 254	97 861	10
51	48 647	50 789	49 211	97 857	9
52	48 686	50 833	49 167	97 853	8
53	48 725	50 876	49 124	97 849	7
54	48 764	50 919	49 081	97 845	6
55	48 803	50 962	49 038	97 841	5
56	48 842	51 005	48 995	97 837	4
57	48 881	51 048	48 952	97 833	3
58	48 920	51 092	48 908	97 829	2
59	48 959	51 135	48 865	97 825	1
60	48 998	51 178	48 822	97 821	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

72°

18°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	48 998	51 178	48 822	97 821	60
1	49 037	51 221	48 779	97 817	59
2	49 076	51 264	48 736	97 812	58
3	49 115	51 306	48 694	97 808	57
4	49 153	51 349	48 651	97 804	56
5	49 192	51 392	48 608	97 800	55
6	49 231	51 435	48 565	97 796	54
7	49 269	51 478	48 522	97 792	53
8	49 308	51 520	48 480	97 788	52
9	49 347	51 563	48 437	97 784	51
10	49 385	51 606	48 394	97 779	50
11	49 424	51 648	48 352	97 775	49
12	49 462	51 691	48 309	97 771	48
13	49 500	51 734	48 266	97 767	47
14	49 539	51 776	48 224	97 763	46
15	49 577	51 819	48 181	97 759	45
16	49 615	51 861	48 139	97 754	44
17	49 654	51 903	48 097	97 750	43
18	49 692	51 946	48 054	97 746	42
19	49 730	51 988	48 012	97 742	41
20	49 768	52 031	47 969	97 738	40
21	49 806	52 073	47 927	97 734	39
22	49 844	52 115	47 885	97 729	38
23	49 882	52 157	47 843	97 725	37
24	49 920	52 200	47 800	97 721	36
25	49 958	52 242	47 758	97 717	35
26	49 996	52 284	47 716	97 713	34
27	50 034	52 326	47 674	97 708	33
28	50 072	52 368	47 632	97 704	32
29	50 110	52 410	47 590	97 700	31
30	50 148	52 452	47 548	97 696	30
31	50 185	52 494	47 506	97 691	29
32	50 223	52 536	47 464	97 687	28
33	50 261	52 578	47 422	97 683	27
34	50 298	52 620	47 380	97 679	26
35	50 336	52 661	47 339	97 674	25
36	50 374	52 703	47 297	97 670	24
37	50 411	52 745	47 255	97 666	23
38	50 449	52 787	47 213	97 662	22
39	50 486	52 829	47 171	97 657	21
40	50 523	52 870	47 130	97 653	20
41	50 561	52 912	47 088	97 649	19
42	50 598	52 953	47 047	97 645	18
43	50 635	52 995	47 005	97 640	17
44	50 673	53 037	46 963	97 636	16
45	50 710	53 078	46 922	97 632	15
46	50 747	53 120	46 880	97 628	14
47	50 784	53 161	46 839	97 623	13
48	50 821	53 202	46 798	97 619	12
49	50 858	53 244	46 756	97 615	11
50	50 896	53 285	46 715	97 610	10
51	50 933	53 327	46 673	97 606	9
52	50 970	53 368	46 632	97 602	8
53	51 007	53 409	46 591	97 597	7
54	51 043	53 450	46 550	97 593	6
55	51 080	53 492	46 508	97 589	5
56	51 117	53 533	46 467	97 584	4
57	51 154	53 574	46 426	97 580	3
58	51 191	53 615	46 385	97 576	2
59	51 227	53 656	46 344	97 571	1
60	51 264	53 697	46 303	97 567	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

71°

19°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	51 264	53 697	46 303	97 567	60
1	51 301	53 738	46 262	97 563	59
2	51 338	53 779	46 221	97 558	58
3	51 374	53 820	46 180	97 554	57
4	51 411	53 861	46 139	97 55̲5	56
5	51 447	53 902	46 098	97 545	55
6	51 484	53 943	46 057	97 541	54
7	51 520	53 984	46 016	97 536	53
8	51 557	54 025̲	45 975	97 532	52
9	51 593	54 065	45 935̲	97 528	51
10	51 629	54 106	45 894	97 523	50
11	51 666	54 147	45 853	97 519	49
12	51 702	54 187	45 813	97 515̲	48
13	51 738	54 228	45 772	97 510	47
14	51 774	54 269	45 731	97 506	46
15	51 811	54 309	45 691	97 501	45
16	51 847	54 35̲0	45 650	97 497	44
17	51 883	54 390	45 610	97 492	43
18	51 919	54 431	45 569	97 488	42
19	51 955	54 471	45 529	97 484	41
20	51 991	54 512	45 488	97 479	40
21	52 027	54 552	45 448	97 475̲	39
22	52 063	54 593	45 407	97 470	38
23	52 099	54 633	45 367	97 466	37
24	52 135̲	54 673	45 327	97 461	36
25	52 171	54 714	45 286	97 457	35
26	52 207	54 754	45 246	97 453	34
27	52 242	54 794	45 206	97 448	33
28	52 278	54 835̲	45 165	97 444	32
29	52 314	54 875̲	45 125	97 439	31
30	52 35̲0	54 915̲	45 085	97 435̲	30
31	52 385	54 955	45 045̲	97 430	29
32	52 421	54 995	45 005̲	97 426	28
33	52 456	55 035	44 965̲	97 421	27
34	52 492	55 075	44 925̲	97 417	26
35	52 527	55 115	44 885̲	97 412	25
36	52 563	55 155	44 845̲	97 408	24
37	52 598	55 195	44 805̲	97 403	23
38	52 634	55 235	44 765̲	97 399	22
39	52 669	55 275	44 725̲	97 394	21
40	52 705̲	55 315̲	44 685	97 390	20
41	52 740	55 355̲	44 645	97 385	19
42	52 775	55 395̲	44 605	97 381	18
43	52 811	55 434	44 566	97 376	17
44	52 846	55 474	44 526	97 372	16
45	52 881	55 514	44 486	97 367	15
46	52 916	55 554	44 446	97 363	14
47	52 951	55 593	44 407	97 358	13
48	52 986	55 633	44 367	97 353	12
49	53 021	55 673	44 327	97 349	11
50	53 056	55 712	44 288	97 344	10
51	53 092	55 752	44 248	97 340	9
52	53 126	55 791	44 209	97 335	8
53	53 161	55 831	44 169	97 331	7
54	53 196	55 870	44 130	97 326	6
55	53 231	55 910	44 090	97 322	5
56	53 266	55 949	44 051	97 317	4
57	53 301	55 989	44 011	97 312	3
58	53 336	56 028	43 972	97 308	2
59	53 370	56 067	43 933	97 303	1
60	53 405	56 107	43 893	97 299	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

70°

20°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	53 405	56 107	43 893	97 299	60
1	53 440	56 146	43 854	97 294	59
2	53 475̲	56 185	43 815̲	97 289	58
3	53 509	56 224	43 776	97 285̲	57
4	53 544	56 264	43 736	97 280	56
5	53 578	56 303	43 697	97 276	55
6	53 613	56 342	43 658	97 271	54
7	53 647	56 381	43 619	97 266	53
8	53 682	56 420	43 580	97 262	52
9	53 716	56 459	43 541	97 257	51
10	53 751	56 498	43 502	97 252	50
11	53 785	56 537	43 463	97 248	49
12	53 819	56 576	43 424	97 243	48
13	53 854	56 615	43 385̲	97 238	47
14	53 888	56 654	43 346	97 234	46
15	53 922	56 693	43 307	97 229	45
16	53 957	56 732	43 268	97 224	44
17	53 991	56 771	43 229	97 220	43
18	54 025̲	56 810	43 190	97 215	42
19	54 059	56 849	43 151	97 210	41
20	54 093	56 887	43 113	97 206	40
21	54 127	56 926	43 074	97 201	39
22	54 161	56 965̲	43 035	97 196	38
23	54 195	57 004	42 996	97 192	37
24	54 229	57 042	42 958	97 187	36
25	54 263	57 081	42 919	97 182	35
26	54 297	57 120	42 880	97 178	34
27	54 331	57 158	42 842	97 173	33
28	54 365̲	57 197	42 803	97 168	32
29	54 399	57 235	42 765̲	97 163	31
30	54 433	57 274	42 726	97 159	30
31	54 466	57 312	42 688	97 154	29
32	54 500	57 351	42 649	97 149	28
33	54 534	57 389	42 611	97 145̲	27
34	54 567	57 428	42 572	97 140	26
35	54 601	57 466	42 534	97 135	25
36	54 635̲	57 504	42 496	97 130	24
37	54 668	57 543	42 457	97 126	23
38	54 702	57 581	42 419	97 121	22
39	54 735	57 619	42 381	97 116	21
40	54 769	57 658	42 342	97 111	20
41	54 802	57 696	42 304	97 107	19
42	54 836	57 734	42 266	97 102	18
43	54 869	57 772	42 228	97 097	17
44	54 903	57 810	42 190	97 092	16
45	54 936	57 849	42 151	97 087	15
46	54 969	57 887	42 113	97 083	14
47	55 003	57 925̲	42 075	97 078	13
48	55 036	57 963	42 037	97 073	12
49	55 069	58 001	41 999	97 068	11
50	55 102	58 039	41 961	97 063	10
51	55 136	58 077	41 923	97 059	9
52	55 169	58 115̲	41 885	97 054	8
53	55 202	58 153	41 847	97 049	7
54	55 235̲	58 191	41 809	97 044	6
55	55 268	58 229	41 771	97 039	5
56	55 301	58 267	41 733	97 035̲	4
57	55 334	58 304	41 696	97 030	3
58	55 367	58 342	41 658	97 025̲	2
59	55 400	58 380	41 620	97 020	1
60	55 433	58 418	41 582	97 015	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

69°

21°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	55 433	58 418	41 582	97 015	60
1	55 466	58 455	41 545	97 010	59
2	55 499	58 493	41 507	97 005	58
3	55 532	58 531	41 469	97 001	57
4	55 564	58 569	41 431	96 996	56
5	55 597	58 606	41 394	96 991	55
6	55 630	58 644	41 356	96 986	54
7	55 663	58 681	41 319	96 981	53
8	55 695	58 719	41 281	96 976	52
9	55 728	58 757	41 243	96 971	51
10	55 761	58 794	41 206	96 966	50
11	55 793	58 832	41 168	96 962	49
12	55 826	58 869	41 131	96 957	48
13	55 858	58 907	41 093	96 952	47
14	55 891	58 944	41 056	96 947	46
15	55 923	58 981	41 019	96 942	45
16	55 956	59 019	40 981	96 937	44
17	55 988	59 056	40 944	96 932	43
18	56 021	59 094	40 906	96 927	42
19	56 053	59 131	40 869	96 922	41
20	56 085	59 168	40 832	96 917	40
21	56 118	59 205	40 795	96 912	39
22	56 150	59 243	40 757	96 907	38
23	56 182	59 280	40 720	96 903	37
24	56 215	59 317	40 683	96 898	36
25	56 247	59 354	40 646	96 893	35
26	56 279	59 391	40 609	96 888	34
27	56 311	59 429	40 571	96 883	33
28	56 343	59 466	40 534	96 878	32
29	56 375	59 503	40 497	96 873	31
30	56 408	59 540	40 460	96 868	30
31	56 440	59 577	40 423	96 863	29
32	56 472	59 614	40 386	96 858	28
33	56 504	59 651	40 349	96 853	27
34	56 536	59 688	40 312	96 848	26
35	56 568	59 725	40 275	96 843	25
36	56 599	59 762	40 238	96 838	24
37	56 631	59 799	40 201	96 833	23
38	56 663	59 835	40 165	96 828	22
39	56 695	59 872	40 128	96 823	21
40	56 727	59 909	40 091	96 818	20
41	56 759	59 946	40 054	96 813	19
42	56 790	59 983	40 017	96 808	18
43	56 822	60 019	39 981	96 803	17
44	56 854	60 056	39 944	96 798	16
45	56 886	60 093	39 907	96 793	15
46	56 917	60 130	39 870	96 788	14
47	56 949	60 166	39 834	96 783	13
48	56 980	60 203	39 797	96 778	12
49	57 012	60 240	39 760	96 772	11
50	57 044	60 276	39 724	96 767	10
51	57 075	60 313	39 687	96 762	9
52	57 107	60 349	39 651	96 757	8
53	57 138	60 386	39 614	96 752	7
54	57 169	60 422	39 578	96 747	6
55	57 201	60 459	39 541	96 742	5
56	57 232	60 495	39 505	96 737	4
57	57 264	60 532	39 468	96 732	3
58	57 295	60 568	39 432	96 727	2
59	57 326	60 605	39 395	96 722	1
60	57 358	60 641	39 359	96 717	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

68°

22°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	57 358	60 641	39 359	96 717	60
1	57 389	60 677	39 323	96 711	59
2	57 420	60 714	39 286	96 706	58
3	57 451	60 750	39 250	96 701	57
4	57 482	60 786	39 214	96 696	56
5	57 514	60 823	39 177	96 691	55
6	57 545	60 859	39 141	96 686	54
7	57 576	60 895	39 105	96 681	53
8	57 607	60 931	39 069	96 676	52
9	57 638	60 967	39 033	96 670	51
10	57 669	61 004	38 996	96 665	50
11	57 700	61 040	38 960	96 660	49
12	57 731	61 076	38 924	96 655	48
13	57 762	61 112	38 888	96 650	47
14	57 793	61 148	38 852	96 645	46
15	57 824	61 184	38 816	96 640	45
16	57 855	61 220	38 780	96 634	44
17	57 885	61 256	38 744	96 629	43
18	57 916	61 292	38 708	96 624	42
19	57 947	61 328	38 672	96 619	41
20	57 978	61 364	38 636	96 614	40
21	58 008	61 400	38 600	96 608	39
22	58 039	61 436	38 564	96 603	38
23	58 070	61 472	38 528	96 598	37
24	58 101	61 508	38 492	96 593	36
25	58 131	61 544	38 456	96 588	35
26	58 162	61 579	38 421	96 582	34
27	58 192	61 615	38 385	96 577	33
28	58 223	61 651	38 349	96 572	32
29	58 253	61 687	38 313	96 567	31
30	58 284	61 722	38 278	96 562	30
31	58 314	61 758	38 242	96 556	29
32	58 345	61 794	38 206	96 551	28
33	58 375	61 830	38 170	96 546	27
34	58 406	61 865	38 135	96 541	26
35	58 436	61 901	38 099	96 535	25
36	58 467	61 936	38 064	96 530	24
37	58 497	61 972	38 028	96 525	23
38	58 527	62 008	37 992	96 520	22
39	58 557	62 043	37 957	96 514	21
40	58 588	62 079	37 921	96 509	20
41	58 618	62 114	37 886	96 504	19
42	58 648	62 150	37 850	96 498	18
43	58 678	62 185	37 815	96 493	17
44	58 709	62 221	37 779	96 488	16
45	58 739	62 256	37 744	96 483	15
46	58 769	62 292	37 708	96 477	14
47	58 799	62 327	37 673	96 472	13
48	58 829	62 362	37 638	96 467	12
49	58 859	62 398	37 602	96 461	11
50	58 889	62 433	37 567	96 456	10
51	58 919	62 468	37 532	96 451	9
52	58 949	62 504	37 496	96 445	8
53	58 979	62 539	37 461	96 440	7
54	59 009	62 574	37 426	96 435	6
55	59 039	62 609	37 391	96 429	5
56	59 069	62 645	37 355	96 424	4
57	59 098	62 680	37 320	96 419	3
58	59 128	62 715	37 285	96 413	2
59	59 158	62 750	37 250	96 408	1
60	59 188	62 785	37 215	96 403	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

67°

23°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	59 188	62 785	37 215	96 403	60
1	59 218	62 820	37 180	96 397	59
2	59 247	62 855	37 145	96 392	58
3	59 277	62 890	37 110	96 387	57
4	59 307	62 926	37 074	96 381	56
5	59 336	62 961	37 039	96 376	55
6	59 366	62 996	37 004	96 370	54
7	59 396	63 031	36 969	96 365	53
8	59 425	63 066	36 934	96 360	52
9	59 455	63 101	36 899	96 354	51
10	59 484	63 135	36 865	96 349	50
11	59 514	63 170	36 830	96 343	49
12	59 543	63 205	36 795	96 338	48
13	59 573	63 240	36 760	96 333	47
14	59 602	63 275	36 725	96 327	46
15	59 632	63 310	36 690	96 322	45
16	59 661	63 345	36 655	96 316	44
17	59 690	63 379	36 621	96 311	43
18	59 720	63 414	36 586	96 305	42
19	59 749	63 449	36 551	96 300	41
20	59 778	63 484	36 516	96 294	40
21	59 808	63 519	36 481	96 289	39
22	59 837	63 553	36 447	96 284	38
23	59 866	63 588	36 412	96 278	37
24	59 895	63 623	36 377	96 273	36
25	59 924	63 657	36 343	96 267	35
26	59 954	63 692	36 308	96 262	34
27	59 983	63 726	36 274	96 256	33
28	60 012	63 761	36 239	96 251	32
29	60 041	63 796	36 204	96 245	31
30	60 070	63 830	36 170	96 240	30
31	60 099	63 865	36 135	96 234	29
32	60 128	63 899	36 101	96 229	28
33	60 157	63 934	36 066	96 223	27
34	60 186	63 968	36 032	96 218	26
35	60 215	64 003	35 997	96 212	25
36	60 244	64 037	35 963	96 207	24
37	60 273	64 072	35 928	96 201	23
38	60 302	64 106	35 894	96 196	22
39	60 331	64 140	35 860	96 190	21
40	60 359	64 175	35 825	96 185	20
41	60 388	64 209	35 791	96 179	19
42	60 417	64 243	35 757	96 174	18
43	60 446	64 278	35 722	96 168	17
44	60 474	64 312	35 688	96 162	16
45	60 503	64 346	35 654	96 157	15
46	60 532	64 381	35 619	96 151	14
47	60 561	64 415	35 585	96 146	13
48	60 589	64 449	35 551	96 140	12
49	60 618	64 483	35 517	96 135	11
50	60 646	64 517	35 483	96 129	10
51	60 675	64 552	35 448	96 123	9
52	60 704	64 586	35 414	96 118	8
53	60 732	64 620	35 380	96 112	7
54	60 761	64 654	35 346	96 107	6
55	60 789	64 688	35 312	96 101	5
56	60 818	64 722	35 278	96 095	4
57	60 846	64 756	35 244	96 090	3
58	60 875	64 790	35 210	96 084	2
59	60 903	64 824	35 176	96 079	1
60	60 931	64 858	35 142	96 073	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

66°

24°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	60 931	64 858	35 142	96 073	60
1	60 960	64 892	35 108	96 067	59
2	60 988	64 926	35 074	96 062	58
3	61 016	64 960	35 040	96 056	57
4	61 045	64 994	35 006	96 050	56
5	61 073	65 028	34 972	96 045	55
6	61 101	65 062	34 938	96 039	54
7	61 129	65 096	34 904	96 034	53
8	61 158	65 130	34 870	96 028	52
9	61 186	65 164	34 836	96 022	51
10	61 214	65 197	34 803	96 017	50
11	61 242	65 231	34 769	96 011	49
12	61 270	65 265	34 735	96 005	48
13	61 298	65 299	34 701	96 000	47
14	61 326	65 333	34 667	95 994	46
15	61 354	65 366	34 634	95 988	45
16	61 382	65 400	34 600	95 982	44
17	61 411	65 434	34 566	95 977	43
18	61 438	65 467	34 533	95 971	42
19	61 466	65 501	34 499	95 965	41
20	61 494	65 535	34 465	95 960	40
21	61 522	65 568	34 432	95 954	39
22	61 550	65 602	34 398	95 948	38
23	61 578	65 636	34 364	95 942	37
24	61 606	65 669	34 331	95 937	36
25	61 634	65 703	34 297	95 931	35
26	61 662	65 736	34 264	95 925	34
27	61 689	65 770	34 230	95 920	33
28	61 717	65 803	34 197	95 914	32
29	61 745	65 837	34 163	95 908	31
30	61 773	65 870	34 130	95 902	30
31	61 800	65 904	34 096	95 897	29
32	61 828	65 937	34 063	95 891	28
33	61 856	65 971	34 029	95 885	27
34	61 883	66 004	33 996	95 879	26
35	61 911	66 038	33 962	95 873	25
36	61 939	66 071	33 929	95 868	24
37	61 966	66 104	33 896	95 862	23
38	61 994	66 138	33 862	95 856	22
39	62 021	66 171	33 829	95 850	21
40	62 049	66 204	33 796	95 844	20
41	62 076	66 238	33 762	95 839	19
42	62 104	66 271	33 729	95 833	18
43	62 131	66 304	33 696	95 827	17
44	62 159	66 337	33 663	95 821	16
45	62 186	66 371	33 629	95 815	15
46	62 214	66 404	33 596	95 810	14
47	62 241	66 437	33 563	95 804	13
48	62 268	66 470	33 530	95 798	12
49	62 296	66 503	33 497	95 792	11
50	62 323	66 537	33 463	95 786	10
51	62 350	66 570	33 430	95 780	9
52	62 377	66 603	33 397	95 775	8
53	62 405	66 636	33 364	95 769	7
54	62 432	66 669	33 331	95 763	6
55	62 459	66 702	33 298	95 757	5
56	62 486	66 735	33 265	95 751	4
57	62 513	66 768	33 232	95 745	3
58	62 541	66 801	33 199	95 739	2
59	62 568	66 834	33 166	95 733	1
60	62 595	66 867	33 133	95 728	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

65°

25°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	62 595	66 867	33 133	95 728	60
1	62 622	66 900	33 100	95 722	59
2	62 649	66 933	33 067	95 716	58
3	62 676	66 966	33 034	95 710	57
4	62 703	66 999	33 001	95 704	56
5	62 730	67 032	32 968	95 698	55
6	62 757	67 065	32 935	95 692	54
7	62 784	67 098	32 902	95 686	53
8	62 811	67 131	32 869	95 680	52
9	62 838	67 163	32 837	95 674	51
10	62 865	67 196	32 804	95 668	50
11	62 892	67 229	32 771	95 663	49
12	62 918	67 262	32 738	95 657	48
13	62 945	67 295	32 705	95 651	47
14	62 972	67 327	32 673	95 645	46
15	62 999	67 360	32 640	95 639	45
16	63 026	67 393	32 607	95 633	44
17	63 052	67 426	32 574	95 627	43
18	63 079	67 458	32 542	95 621	42
19	63 106	67 491	32 509	95 615	41
20	63 133	67 524	32 476	95 609	40
21	63 159	67 556	32 444	95 603	39
22	63 186	67 589	32 411	95 597	38
23	63 213	67 622	32 378	95 591	37
24	63 239	67 654	32 346	95 585	36
25	63 266	67 687	32 313	95 579	35
26	63 292	67 719	32 281	95 573	34
27	63 319	67 752	32 248	95 567	33
28	63 345	67 785	32 215	95 561	32
29	63 372	67 817	32 183	95 555	31
30	63 398	67 850	32 150	95 549	30
31	63 425	67 882	32 118	95 543	29
32	63 451	67 915	32 085	95 537	28
33	63 478	67 947	32 053	95 531	27
34	63 504	67 980	32 020	95 525	26
35	63 531	68 012	31 988	95 519	25
36	63 557	68 044	31 956	95 513	24
37	63 583	68 077	31 923	95 507	23
38	63 610	68 109	31 891	95 500	22
39	63 636	68 142	31 858	95 494	21
40	63 662	68 174	31 826	95 488	20
41	63 689	68 206	31 794	95 482	19
42	63 715	68 239	31 761	95 476	18
43	63 741	68 271	31 729	95 470	17
44	63 767	68 303	31 697	95 464	16
45	63 794	68 336	31 664	95 458	15
46	63 820	68 368	31 632	95 452	14
47	63 846	68 400	31 600	95 446	13
48	63 872	68 432	31 568	95 440	12
49	63 898	68 465	31 535	95 434	11
50	63 924	68 497	31 503	95 427	10
51	63 950	68 529	31 471	95 421	9
52	63 976	68 561	31 439	95 415	8
53	64 002	68 593	31 407	95 409	7
54	64 028	68 626	31 374	95 403	6
55	64 054	68 658	31 342	95 397	5
56	64 080	68 690	31 310	95 391	4
57	64 106	68 722	31 278	95 384	3
58	64 132	68 754	31 246	95 378	2
59	64 158	68 786	31 214	95 372	1
60	64 184	68 818	31 182	95 366	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

64°

26°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	64 184	68 818	31 182	95 366	60
1	64 210	68 850	31 150	95 360	59
2	64 236	68 882	31 118	95 354	58
3	64 262	68 914	31 086	95 348	57
4	64 288	68 946	31 054	95 341	56
5	64 313	68 978	31 022	95 335	55
6	64 339	69 010	30 990	95 329	54
7	64 365	69 042	30 958	95 323	53
8	64 391	69 074	30 926	95 317	52
9	64 417	69 106	30 894	95 310	51
10	64 442	69 138	30 862	95 304	50
11	64 468	69 170	30 830	95 298	49
12	64 494	69 202	30 798	95 292	48
13	64 519	69 234	30 766	95 286	47
14	64 545	69 266	30 734	95 279	46
15	64 571	69 298	30 702	95 273	45
16	64 596	69 329	30 671	95 267	44
17	64 622	69 361	30 639	95 261	43
18	64 647	69 393	30 607	95 254	42
19	64 673	69 425	30 575	95 248	41
20	64 698	69 457	30 543	95 242	40
21	64 724	69 488	30 512	95 236	39
22	64 749	69 520	30 480	95 229	38
23	64 775	69 552	30 448	95 223	37
24	64 800	69 584	30 416	95 217	36
25	64 826	69 615	30 385	95 211	35
26	64 851	69 647	30 353	95 204	34
27	64 877	69 679	30 321	95 198	33
28	64 902	69 710	30 290	95 192	32
29	64 927	69 742	30 258	95 185	31
30	64 953	69 774	30 226	95 179	30
31	64 978	69 805	30 195	95 173	29
32	65 003	69 837	30 163	95 167	28
33	65 029	69 868	30 132	95 160	27
34	65 054	69 900	30 100	95 154	26
35	65 079	69 932	30 068	95 148	25
36	65 104	69 963	30 037	95 141	24
37	65 130	69 995	30 005	95 135	23
38	65 155	70 026	29 974	95 129	22
39	65 180	70 058	29 942	95 122	21
40	65 205	70 089	29 911	95 116	20
41	65 230	70 121	29 879	95 110	19
42	65 255	70 152	29 848	95 103	18
43	65 281	70 184	29 816	95 097	17
44	65 306	70 215	29 785	95 090	16
45	65 331	70 247	29 753	95 084	15
46	65 356	70 278	29 722	95 078	14
47	65 381	70 309	29 691	95 071	13
48	65 406	70 341	29 659	95 065	12
49	65 431	70 372	29 628	95 059	11
50	65 456	70 404	29 596	95 052	10
51	65 481	70 435	29 565	95 046	9
52	65 506	70 466	29 534	95 039	8
53	65 531	70 498	29 502	95 033	7
54	65 556	70 529	29 471	95 027	6
55	65 580	70 560	29 440	95 020	5
56	65 605	70 592	29 408	95 014	4
57	65 630	70 623	29 377	95 007	3
58	65 655	70 654	29 346	95 001	2
59	65 680	70 685	29 315	94 995	1
60	65 705	70 717	29 283	94 988	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

63°

27°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	65 705	70 717	29 283	94 988	60
1	65 729	70 748	29 252	94 982	59
2	65 754	70 779	29 221	94 975	58
3	65 779	70 810	29 190	94 969	57
4	65 804	70 841	29 159	94 962	56
5	65 828	70 873	29 127	94 956	55
6	65 853	70 904	29 096	94 949	54
7	65 878	70 935	29 065	94 943	53
8	65 902	70 966	29 034	94 936	52
9	65 927	70 997	29 003	94 930	51
10	65 952	71 028	28 972	94 923	50
11	65 976	71 059	28 941	94 917	49
12	66 001	71 090	28 910	94 911	48
13	66 025	71 121	28 879	94 904	47
14	66 050	71 153	28 847	94 898	46
15	66 075	71 184	28 816	94 891	45
16	66 099	71 215	28 785	94 885	44
17	66 124	71 246	28 754	94 878	43
18	66 148	71 277	28 723	94 871	42
19	66 173	71 308	28 692	94 865	41
20	66 197	71 339	28 661	94 858	40
21	66 221	71 370	28 630	94 852	39
22	66 246	71 401	28 599	94 845	38
23	66 270	71 431	28 569	94 839	37
24	66 295	71 462	28 538	94 832	36
25	66 319	71 493	28 507	94 826	35
26	66 343	71 524	28 476	94 819	34
27	66 368	71 555	28 445	94 813	33
28	66 392	71 586	28 414	94 806	32
29	66 416	71 617	28 383	94 799	31
30	66 441	71 648	28 352	94 793	30
31	66 465	71 679	28 321	94 786	29
32	66 489	71 709	28 291	94 780	28
33	66 513	71 740	28 260	94 773	27
34	66 537	71 771	28 229	94 767	26
35	66 562	71 802	28 198	94 760	25
36	66 586	71 833	28 167	94 753	24
37	66 610	71 863	28 137	94 747	23
38	66 634	71 894	28 106	94 740	22
39	66 658	71 925	28 075	94 734	21
40	66 682	71 955	28 045	94 727	20
41	66 706	71 986	28 014	94 720	19
42	66 731	72 017	27 983	94 714	18
43	66 755	72 048	27 952	94 707	17
44	66 779	72 078	27 922	94 700	16
45	66 803	72 109	27 891	94 694	15
46	66 827	72 140	27 860	94 687	14
47	66 851	72 170	27 830	94 680	13
48	66 875	72 201	27 799	94 674	12
49	66 899	72 231	27 769	94 667	11
50	66 922	72 262	27 738	94 660	10
51	66 946	72 293	27 707	94 654	9
52	66 970	72 323	27 677	94 647	8
53	66 994	72 354	27 646	94 640	7
54	67 018	72 384	27 616	94 634	6
55	67 042	72 415	27 585	94 627	5
56	67 066	72 445	27 555	94 620	4
57	67 090	72 476	27 524	94 614	3
58	67 113	72 506	27 494	94 607	2
59	67 137	72 537	27 463	94 600	1
60	67 161	72 567	27 433	94 593	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

62°

28°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	67 161	72 567	27 433	94 593	60
1	67 185	72 598	27 402	94 587	59
2	67 208	72 628	27 372	94 580	58
3	67 232	72 659	27 341	94 573	57
4	67 256	72 689	27 311	94 567	56
5	67 280	72 720	27 280	94 560	55
6	67 303	72 750	27 250	94 553	54
7	67 327	72 780	27 220	94 546	53
8	67 350	72 811	27 189	94 540	52
9	67 374	72 841	27 159	94 533	51
10	67 398	72 872	27 128	94 526	50
11	67 421	72 902	27 098	94 519	49
12	67 445	72 932	27 068	94 513	48
13	67 468	72 963	27 037	94 506	47
14	67 492	72 993	27 007	94 499	46
15	67 515	73 023	26 977	94 492	45
16	67 539	73 054	26 946	94 485	44
17	67 562	73 084	26 916	94 479	43
18	67 586	73 114	26 886	94 472	42
19	67 609	73 144	26 856	94 465	41
20	67 633	73 175	26 825	94 458	40
21	67 656	73 205	26 795	94 451	39
22	67 680	73 235	26 765	94 445	38
23	67 703	73 265	26 735	94 438	37
24	67 726	73 295	26 705	94 431	36
25	67 750	73 326	26 674	94 424	35
26	67 773	73 356	26 644	94 417	34
27	67 796	73 386	26 614	94 410	33
28	67 820	73 416	26 584	94 404	32
29	67 843	73 446	26 554	94 397	31
30	67 866	73 476	26 524	94 390	30
31	67 890	73 507	26 493	94 383	29
32	67 913	73 537	26 463	94 376	28
33	67 936	73 567	26 433	94 369	27
34	67 959	73 597	26 403	94 362	26
35	67 982	73 627	26 373	94 355	25
36	68 006	73 657	26 343	94 349	24
37	68 029	73 687	26 313	94 342	23
38	68 052	73 717	26 283	94 335	22
39	68 075	73 747	26 253	94 328	21
40	68 098	73 777	26 223	94 321	20
41	68 121	73 807	26 193	94 314	19
42	68 144	73 837	26 163	94 307	18
43	68 167	73 867	26 133	94 300	17
44	68 190	73 897	26 103	94 293	16
45	68 213	73 927	26 073	94 286	15
46	68 237	73 957	26 043	94 279	14
47	68 260	73 987	26 013	94 273	13
48	68 283	74 017	25 983	94 266	12
49	68 305	74 047	25 953	94 259	11
50	68 328	74 077	25 923	94 252	10
51	68 351	74 107	25 893	94 245	9
52	68 374	74 137	25 863	94 238	8
53	68 397	74 166	25 834	94 231	7
54	68 420	74 196	25 804	94 224	6
55	68 443	74 226	25 774	94 217	5
56	68 466	74 256	25 744	94 210	4
57	68 489	74 286	25 714	94 203	3
58	68 512	74 316	25 684	94 196	2
59	68 534	74 345	25 655	94 189	1
60	68 557	74 375	25 625	94 182	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

61°

29°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	68 557	74 375	25 625	94 182	60
1	68 580	74 405	25 595	94 175	59
2	68 603	74 435	25 565	94 168	58
3	68 625	74 465	25 535	94 161	57
4	68 648	74 494	25 506	94 154	56
5	68 671	74 524	25 476	94 147	55
6	68 694	74 554	25 446	94 140	54
7	68 716	74 583	25 417	94 133	53
8	68 739	74 613	25 387	94 126	52
9	68 762	74 643	25 357	94 119	51
10	68 784	74 673	25 327	94 112	50
11	68 807	74 702	25 298	94 105	49
12	68 829	74 732	25 268	94 098	48
13	68 852	74 762	25 238	94 090	47
14	68 875	74 791	25 209	94 083	46
15	68 897	74 821	25 179	94 076	45
16	68 920	74 851	25 149	94 069	44
17	68 942	74 880	25 120	94 062	43
18	68 965	74 910	25 090	94 055	42
19	68 987	74 939	25 061	94 048	41
20	69 010	74 969	25 031	94 041	40
21	69 032	74 998	25 002	94 034	39
22	69 055	75 028	24 972	94 027	38
23	69 077	75 058	24 942	94 020	37
24	69 100	75 087	24 913	94 012	36
25	69 122	75 117	24 883	94 005	35
26	69 144	75 146	24 854	93 998	34
27	69 167	75 176	24 824	93 991	33
28	69 189	75 205	24 795	93 984	32
29	69 212	75 235	24 765	93 977	31
30	69 234	75 264	24 736	93 970	30
31	69 256	75 294	24 706	93 963	29
32	69 279	75 323	24 677	93 955	28
33	69 301	75 353	24 647	93 948	27
34	69 323	75 382	24 618	93 941	26
35	69 345	75 411	24 589	93 934	25
36	69 368	75 441	24 559	93 927	24
37	69 390	75 470	24 530	93 920	23
38	69 412	75 500	24 500	93 912	22
39	69 434	75 529	24 471	93 905	21
40	69 456	75 558	24 442	93 898	20
41	69 479	75 588	24 412	93 891	19
42	69 501	75 617	24 383	93 884	18
43	69 523	75 647	24 353	93 876	17
44	69 545	75 676	24 324	93 869	16
45	69 567	75 705	24 295	93 862	15
46	69 589	75 735	24 265	93 855	14
47	69 611	75 764	24 236	93 847	13
48	69 633	75 793	24 207	93 840	12
49	69 655	75 822	24 178	93 833	11
50	69 677	75 852	24 148	93 826	10
51	69 699	75 881	24 119	93 819	9
52	69 721	75 910	24 090	93 811	8
53	69 743	75 939	24 061	93 804	7
54	69 765	75 969	24 031	93 797	6
55	69 787	75 998	24 002	93 789	5
56	69 809	76 027	23 973	93 782	4
57	69 831	76 056	23 944	93 775	3
58	69 853	76 086	23 914	93 768	2
59	69 875	76 115	23 885	93 760	1
60	69 897	76 144	23 856	93 753	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

60°

30°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	69 897	76 144	23 856	93 753	60
1	69 919	76 173	23 827	93 746	59
2	69 941	76 202	23 798	93 738	58
3	69 963	76 231	23 769	93 731	57
4	69 984	76 261	23 739	93 724	56
5	70 006	76 290	23 710	93 717	55
6	70 028	76 319	23 681	93 709	54
7	70 050	76 348	28 652	93 702	53
8	70 072	76 377	23 623	93 695	52
9	70 093	76 406	23 594	93 687	51
10	70 115	76 435	23 565	93 680	50
11	70 137	76 464	23 536	93 673	49
12	70 159	76 493	23 507	93 665	48
13	70 180	76 522	23 478	93 658	47
14	70 202	76 551	23 449	93 650	46
15	70 224	76 580	23 420	93 643	45
16	70 245	76 609	23 391	93 636	44
17	70 267	76 639	23 361	93 628	43
18	70 288	76 668	23 332	93 621	42
19	70 310	76 697	23 303	93 614	41
20	70 332	76 725	23 275	93 606	40
21	70 353	76 754	23 246	93 599	39
22	70 375	76 783	23 217	93 591	38
23	70 396	76 812	23 188	93 584	37
24	70 418	76 841	23 159	93 577	36
25	70 439	76 870	23 130	93 569	35
26	70 461	76 899	23 101	93 562	34
27	70 482	76 928	23 072	93 554	33
28	70 504	76 957	23 043	93 547	32
29	70 525	76 986	23 014	93 539	31
30	70 547	77 015	22 985	93 532	30
31	70 568	77 044	22 956	93 525	29
32	70 590	77 073	22 927	93 517	28
33	70 611	77 101	22 899	93 510	27
34	70 633	77 130	22 870	93 502	26
35	70 654	77 159	22 841	93 495	25
36	70 675	77 188	22 812	93 487	24
37	70 697	77 217	22 783	93 480	23
38	70 718	77 246	22 754	93 472	22
39	70 739	77 274	22 726	93 465	21
40	70 761	77 303	22 697	93 457	20
41	70 782	77 332	22 668	93 450	19
42	70 803	77 361	22 639	93 442	18
43	70 824	77 390	22 610	93 435	17
44	70 846	77 418	22 582	93 427	16
45	70 867	77 447	22 553	93 420	15
46	70 888	77 476	22 524	93 412	14
47	70 909	77 505	22 495	93 405	13
48	70 931	77 533	22 467	93 397	12
49	70 952	77 562	22 438	93 390	11
50	70 973	77 591	22 409	93 382	10
51	70 994	77 619	22 381	93 375	9
52	71 015	77 648	22 352	93 367	8
53	71 036	77 677	22 323	93 360	7
54	71 058	77 706	22 294	93 352	6
55	71 079	77 734	22 266	93 344	5
56	71 100	77 763	22 237	93 337	4
57	71 121	77 791	22 209	93 329	3
58	71 142	77 820	22 180	93 322	2
59	71 163	77 849	22 151	93 314	1
60	71 184	77 877	22 123	93 307	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

59°

31°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	71 184	77 877	22 123	93 307	60
1	71 205	77 906	22 094	93 299	59
2	71 226	77 935	22 065	93 291	58
3	71 247	77 963	22 037	93 284	57
4	71 268	77 992	22 008	93 276	56
5	71 289	78 020	21 980	93 269	55
6	71 310	78 049	21 951	93 261	54
7	71 331	78 077	21 923	93 253	53
8	71 352	78 106	21 894	93 246	52
9	71 373	78 135	21 865	93 238	51
10	71 393	78 163	21 837	93 230	50
11	71 414	78 192	21 808	93 223	49
12	71 435	78 220	21 780	93 215	48
13	71 456	78 249	21 751	93 207	47
14	71 477	78 277	21 723	93 200	46
15	71 498	78 306	21 694	93 192	45
16	71 519	78 334	21 666	93 184	44
17	71 539	78 363	21 637	93 177	43
18	71 560	78 391	21 609	93 169	42
19	71 581	78 419	21 581	93 161	41
20	71 602	78 448	21 552	93 154	40
21	71 622	78 476	21 524	93 146	39
22	71 643	78 505	21 495	93 138	38
23	71 664	78 533	21 467	93 131	37
24	71 685	78 562	21 438	93 123	36
25	71 705	78 590	21 410	93 115	35
26	71 726	78 618	21 382	93 108	34
27	71 747	78 647	21 353	93 100	33
28	71 767	78 675	21 325	93 092	32
29	71 788	78 704	21 296	93 084	31
30	71 809	78 732	21 268	93 077	30
31	71 829	78 760	21 240	93 069	29
32	71 850	78 789	21 211	93 061	28
33	71 870	78 817	21 183	93 053	27
34	71 891	78 845	21 155	93 046	26
35	71 911	78 874	21 126	93 038	25
36	71 932	78 902	21 098	93 030	24
37	71 952	78 930	21 070	93 022	23
38	71 973	78 959	21 041	93 014	22
39	71 994	78 987	21 013	93 007	21
40	72 014	79 015	20 985	92 999	20
41	72 034	79 043	20 957	92 991	19
42	72 055	79 072	20 928	92 983	18
43	72 075	79 100	20 900	92 976	17
44	72 096	79 128	20 872	92 968	16
45	72 116	79 156	20 844	92 960	15
46	72 137	79 185	20 815	92 952	14
47	72 157	79 213	20 787	92 944	13
48	72 177	79 241	20 759	92 936	12
49	72 198	79 269	20 731	92 929	11
50	72 218	79 297	20 703	92 921	10
51	72 238	79 326	20 674	92 913	9
52	72 259	79 354	20 646	92 905	8
53	72 279	79 382	20 618	92 897	7
54	72 299	79 410	20 590	92 889	6
55	72 320	79 438	20 562	92 881	5
56	72 340	79 466	20 534	92 874	4
57	72 360	79 495	20 505	92 866	3
58	72 381	79 523	20 477	92 858	2
59	72 401	79 551	20 449	92 850	1
60	72 421	79 579	20 421	92 842	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

58°

32°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	72 421	79 579	20 421	92 842	60
1	72 441	79 607	20 393	92 834	59
2	72 461	79 635	20 365	92 826	58
3	72 482	79 663	20 337	92 818	57
4	72 502	79 691	20 309	92 810	56
5	72 522	79 719	20 281	92 803	55
6	72 542	79 747	20 253	92 795	54
7	72 562	79 776	20 224	92 787	53
8	72 582	79 804	20 196	92 779	52
9	72 602	79 832	20 168	92 771	51
10	72 622	79 860	20 140	92 763	50
11	72 643	79 888	20 112	92 755	49
12	72 663	79 916	20 084	92 747	48
13	72 683	79 944	20 056	92 739	47
14	72 703	79 972	20 028	92 731	46
15	72 723	80 000	20 000	92 723	45
16	72 743	80 028	19 972	92 715	44
17	72 763	80 056	19 944	92 707	43
18	72 783	80 084	19 916	92 699	42
19	72 803	80 112	19 888	92 691	41
20	72 823	80 140	19 860	92 683	40
21	72 843	80 168	19 832	92 675	39
22	72 863	80 195	19 805	92 667	38
23	72 883	80 223	19 777	92 659	37
24	72 902	80 251	19 749	92 651	36
25	72 922	80 279	19 721	92 643	35
26	72 942	80 307	19 693	92 635	34
27	72 962	80 335	19 665	92 627	33
28	72 982	80 363	19 637	92 619	32
29	73 002	80 391	19 609	92 611	31
30	73 022	80 419	19 581	92 603	30
31	73 041	80 447	19 553	92 595	29
32	73 061	80 474	19 526	92 587	28
33	73 081	80 502	19 498	92 579	27
34	73 101	80 530	19 470	92 571	26
35	73 121	80 558	19 442	92 563	25
36	73 140	80 586	19 414	92 555	24
37	73 160	80 614	19 386	92 546	23
38	73 180	80 642	19 358	92 538	22
39	73 200	80 669	19 331	92 530	21
40	73 219	80 697	19 303	92 522	20
41	73 239	80 725	19 275	92 514	19
42	73 259	80 753	19 247	92 506	18
43	73 278	80 781	19 219	92 498	17
44	73 298	80 808	19 192	92 490	16
45	73 318	80 836	19 164	92 482	15
46	73 337	80 864	19 136	92 473	14
47	73 357	80 892	19 108	92 465	13
48	73 377	80 919	19 081	92 457	12
49	73 396	80 947	19 053	92 449	11
50	73 416	80 975	19 025	92 441	10
51	73 435	81 003	18 997	92 433	9
52	73 455	81 030	18 970	92 425	8
53	73 474	81 058	18 942	92 416	7
54	73 494	81 086	18 914	92 408	6
55	73 513	81 113	18 887	92 400	5
56	73 533	81 141	18 859	92 392	4
57	73 552	81 169	18 831	92 384	3
58	73 572	81 196	18 804	92 376	2
59	73 591	81 224	18 776	92 367	1
60	73 611	81 252	18 748	92 359	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

57°

33°

′	log sin −9−	log tan −9−	log cot −10−	log cos −9−	′
0	73 611	81 252	18 748	92 359	60
1	73 630	81 279	18 721	92 351	59
2	73 650	81 307	18 693	92 343	58
3	73 669	81 335	18 665	92 335	57
4	73 689	81 362	18 638	92 326	56
5	73 708	81 390	18 610	92 318	55
6	73 727	81 418	18 582	92 310	54
7	73 747	81 445	18 555	92 302	53
8	73 766	81 473	18 527	92 293	52
9	73 785	81 500	18 500	92 285	51
10	73 805	81 528	18 472	92 277	50
11	73 824	81 556	18 444	92 269	49
12	73 843	81 583	18 417	92 260	48
13	73 863	81 611	18 389	92 252	47
14	73 882	81 638	18 362	92 244	46
15	73 901	81 666	18 334	92 235	45
16	73 921	81 693	18 307	92 227	44
17	73 940	81 721	18 279	92 219	43
18	73 959	81 748	18 252	92 211	42
19	73 978	81 776	18 224	92 202	41
20	73 997	81 803	18 197	92 194	40
21	74 017	81 831	18 169	92 186	39
22	74 036	81 858	18 142	92 177	38
23	74 055	81 886	18 114	92 169	37
24	74 074	81 913	18 087	92 161	36
25	74 093	81 941	18 059	92 152	35
26	74 113	81 968	18 032	92 144	34
27	74 132	81 996	18 004	92 136	33
28	74 151	82 023	17 977	92 127	32
29	74 170	82 051	17 949	92 119	31
30	74 189	82 078	17 922	92 111	30
31	74 208	82 106	17 894	92 102	29
32	74 227	82 133	17 867	92 094	28
33	74 246	82 161	17 839	92 086	27
34	74 265	82 188	17 812	92 077	26
35	74 284	82 215	17 785	92 069	25
36	74 303	82 243	17 757	92 060	24
37	74 322	82 270	17 730	92 052	23
38	74 341	82 298	17 702	92 044	22
39	74 360	82 325	17 675	92 035	21
40	74 379	82 352	17 648	92 027	20
41	74 398	82 380	17 620	92 018	19
42	74 417	82 407	17 593	92 010	18
43	74 436	82 435	17 565	92 002	17
44	74 455	82 462	17 538	91 993	16
45	74 474	82 489	17 511	91 985	15
46	74 493	82 517	17 483	91 976	14
47	74 512	82 544	17 456	91 968	13
48	74 531	82 571	17 429	91 959	12
49	74 549	82 599	17 401	91 951	11
50	74 568	82 626	17 374	91 942	10
51	74 587	82 653	17 347	91 934	9
52	74 606	82 681	17 319	91 925	8
53	74 625	82 708	17 292	91 917	7
54	74 644	82 735	17 265	91 908	6
55	74 662	82 762	17 238	91 900	5
56	74 681	82 790	17 210	91 891	4
57	74 700	82 817	17 183	91 883	3
58	74 719	82 844	17 156	91 874	2
59	74 737	82 871	17 129	91 866	1
60	74 756	82 899	17 101	91 857	0
′	−9− log cos	−9− log cot	−10− log tan	−9− log sin	′

56°

34°

′	log sin −9−	log tan −9−	log cot −10−	log cos −9−	′
0	74 756	82 899	17 101	91 857	60
1	74 775	82 926	17 074	91 849	59
2	74 794	82 953	17 047	91 840	58
3	74 812	82 980	17 020	91 832	57
4	74 831	83 008	16 992	91 823	56
5	74 850	83 035	16 965	91 815	55
6	74 868	83 062	16 938	91 806	54
7	74 887	83 089	16 911	91 798	53
8	74 906	83 117	16 883	91 789	52
9	74 924	83 144	16 856	91 781	51
10	74 943	83 171	16 829	91 772	50
11	74 961	83 198	16 802	91 763	49
12	74 980	83 225	16 775	91 755	48
13	74 999	83 252	16 748	91 746	47
14	75 017	83 280	16 720	91 738	46
15	75 036	83 307	16 693	91 729	45
16	75 054	83 334	16 666	91 720	44
17	75 073	83 361	16 639	91 712	43
18	75 091	83 388	16 612	91 703	42
19	75 110	83 415	16 585	91 695	41
20	75 128	83 442	16 558	91 686	40
21	75 147	83 470	16 530	91 677	39
22	75 165	83 497	16 503	91 669	38
23	75 184	83 524	16 476	91 660	37
24	75 202	83 551	16 449	91 651	36
25	75 221	83 578	16 422	91 643	35
26	75 239	83 605	16 395	91 634	34
27	75 258	83 632	16 368	91 625	33
28	75 276	83 659	16 341	91 617	32
29	75 294	83 686	16 314	91 608	31
30	75 313	83 713	16 287	91 599	30
31	75 331	83 740	16 260	91 591	29
32	75 350	83 768	16 232	91 582	28
33	75 368	83 795	16 205	91 573	27
34	75 386	83 822	16 178	91 565	26
35	75 405	83 849	16 151	91 556	25
36	75 423	83 876	16 124	91 547	24
37	75 441	83 903	16 097	91 538	23
38	75 459	83 930	16 070	91 530	22
39	75 478	83 957	16 043	91 521	21
40	75 496	83 984	16 016	91 512	20
41	75 514	84 011	15 989	91 504	19
42	75 533	84 038	15 962	91 495	18
43	75 551	84 065	15 935	91 486	17
44	75 569	84 092	15 908	91 477	16
45	75 587	84 119	15 881	91 469	15
46	75 605	84 146	15 854	91 460	14
47	75 624	84 173	15 827	91 451	13
48	75 642	84 200	15 800	91 442	12
49	75 660	84 227	15 773	91 433	11
50	75 678	84 254	15 746	91 425	10
51	75 696	84 280	15 720	91 416	9
52	75 714	84 307	15 693	91 407	8
53	75 733	84 334	15 666	91 398	7
54	75 751	84 361	15 639	91 389	6
55	75 769	84 388	15 612	91 381	5
56	75 787	84 415	15 585	91 372	4
57	75 805	84 442	15 558	91 363	3
58	75 823	84 469	15 531	91 354	2
59	75 841	84 496	15 504	91 345	1
60	75 859	84 523	15 477	91 336	0
′	−9− log cos	−9− log cot	−10− log tan	−9− log sin	′

55°

35°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	75 859	84 523	15 477	91 336	60
1	75 877	84 55̲0	15 450	91 328	59
2	75 895	84 576	15 424	91 319	58
3	75 913	84 603	15 397	91 310	57
4	75 931	84 630	15 370	91 301	56
5	75 949	84 657	15 343	91 292	55
6	75 967	84 684	15 316	91 283	54
7	75 985	84 711	15 289	91 274	53
8	76 003	84 738	15 262	91 266	52
9	76 021	84 764	15 236	91 257	51
10	76 039	84 791	15 209	91 248	50
11	76 057	84 818	15 182	91 239	49
12	76 075̲	84 845̲	15 155	91 230	48
13	76 093	84 872	15 128	91 221	47
14	76 111	84 899	15 101	91 212	46
15	76 129	84 925	15 075̲	91 203	45
16	76 146	84 952	15 048	91 194	44
17	76 164	84 979	15 021	91 185	43
18	76 182	85 006	14 994	91 176	42
19	76 200	85 033	14 967	91 167	41
20	76 218	85 059	14 941	91 158	40
21	76 236	85 086	14 914	91 149	39
22	76 253	85 113	14 887	91 141	38
23	76 271	85 140	14 860	91 132	37
24	76 289	85 166	14 834	91 123	36
25	76 307	85 193	14 807	91 114	35
26	76 324	85 220	14 780	91 105̲	34
27	76 342	85 247	14 753	91 096	33
28	76 360	85 273	14 727	91 087	32
29	76 378	85 300	14 700	91 078	31
30	76 395	85 327	14 673	91 069	30
31	76 413	85 354	14 646	91 060	29
32	76 431	85 380	14 620	91 051	28
33	76 448	85 407	14 593	91 042	27
34	76 466	85 434	14 566	91 033	26
35	76 484	85 460	14 540	91 023	25
36	76 501	85 487	14 513	91 014	24
37	76 519	85 514	14 486	91 005	23
38	76 537	85 540	14 460	90 996	22
39	76 554	85 567	14 433	90 987	21
40	76 572	85 594	14 406	90 978	20
41	76 590	85 620	14 380	90 969	19
42	76 607	85 647	14 353	90 960	18
43	76 625̲	85 674	14 326	90 951	17
44	76 642	85 700	14 300	90 942	16
45	76 660	85 727	14 273	90 933	15
46	76 677	85 754	14 246	90 924	14
47	76 695̲	85 780	14 220	90 915̲	13
48	76 712	85 807	14 193	90 906	12
49	76 730	85 834	14 166	90 896	11
50	76 747	85 860	14 140	90 887	10
51	76 765̲	85 887	14 113	90 878	9
52	76 782	85 913	14 087	90 869	8
53	76 800	85 940	14 060	90 860	7
54	76 817	85 967	14 033	90 851	6
55	76 835̲	85 993	14 007	90 842	5
56	76 852	86 020	13 980	90 832	4
57	76 870	86 046	13 954	90 823	3
58	76 887	86 073	13 927	90 814	2
59	76 904	86 100	13 900	90 805̲	1
60	76 922	86 126	13 874	90 796	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

54°

36°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	76 922	86 126	13 874	90 796	60
1	76 939	86 153	13 847	90 787	59
2	76 957	86 179	13 821	90 777	58
3	76 974	86 206	13 794	90 768	57
4	76 991	86 232	13 768	90 759	56
5	77 009	86 259	13 741	90 75̲0	55
6	77 026	86 285	13 715̲	90 741	54
7	77 043	86 312	13 688	90 731	53
8	77 061	86 338	13 662	90 722	52
9	77 078	86 365	13 635̲	90 713	51
10	77 095	86 392	13 608	90 704	50
11	77 112	86 418	13 582	90 694	49
12	77 130	86 445̲	13 555	90 685	48
13	77 147	86 471	13 529	90 676	47
14	77 164	86 498	13 502	90 667	46
15	77 181	86 524	13 476	90 657	45
16	77 199	86 551	13 449	90 648	44
17	77 216	86 577	13 423	90 639	43
18	77 233	86 603	13 397	90 630	42
19	77 250	86 630	13 370	90 620	41
20	77 268	86 656	13 344	90 611	40
21	77 285̲	86 683	13 317	90 602	39
22	77 302	86 709	13 291	90 592	38
23	77 319	86 736	13 264	90 583	37
24	77 336	86 762	13 238	90 574	36
25	77 353	86 789	13 211	90 565̲	35
26	77 370	86 815	13 185̲	90 555	34
27	77 387	86 842	13 158	90 546	33
28	77 405̲	86 868	13 132	90 537	32
29	77 422	86 894	13 106	90 527	31
30	77 439	86 921	13 079	90 518	30
31	77 456	86 947	13 053	90 509	29
32	77 473	86 974	13 026	90 499	28
33	77 490	87 000	13 000	90 490	27
34	77 507	87 027	12 973	90 480	26
35	77 524	87 053	12 947	90 471	25
36	77 541	87 079	12 921	90 462	24
37	77 558	87 106	12 894	90 452	23
38	77 575	87 132	12 868	90 443	22
39	77 592	87 158	12 842	90 434	21
40	77 609	87 185̲	12 815	90 424	20
41	77 626	87 211	12 789	90 415̲	19
42	77 643	87 238	12 762	90 405	18
43	77 660	87 264	12 736	90 396	17
44	77 677	87 290	12 710	90 386	16
45	77 694	87 317	12 683	90 377	15
46	77 711	87 343	12 657	90 368	14
47	77 728	87 369	12 631	90 358	13
48	77 744	87 396	12 604	90 349	12
49	77 761	87 422	12 578	90 339	11
50	77 778	87 448	12 552	90 330	10
51	77 795	87 475̲	12 525	90 320	9
52	77 812	87 501	12 499	90 311	8
53	77 829	87 527	12 473	90 301	7
54	77 846	87 554	12 446	90 292	6
55	77 862	87 580	12 420	90 282	5
56	77 879	87 606	12 394	90 273	4
57	77 896	87 633	12 367	90 263	3
58	77 913	87 659	12 341	90 254	2
59	77 930	87 685	12 315̲	90 244	1
60	77 946	87 711	12 289	90 235̲	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

53°

37°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	77 946	87 711	12 289	90 235	60
1	77 963	87 738	12 262	90 225	59
2	77 980	87 764	12 236	90 216	58
3	77 997	87 790	12 210	90 206	57
4	78 013	87 817	12 183	90 197	56
5	78 030	87 843	12 157	90 187	55
6	78 047	87 869	12 131	90 178	54
7	78 063	87 895	12 105	90 168	53
8	78 080	87 922	12 078	90 159	52
9	78 097	87 948	12 052	90 149	51
10	78 113	87 974	12 026	90 139	50
11	78 130	88 000	12 000	90 130	49
12	78 147	88 027	11 973	90 120	48
13	78 163	88 053	11 947	90 111	47
14	78 180	88 079	11 921	90 101	46
15	78 197	88 105	11 895	90 091	45
16	78 213	88 131	11 869	90 082	44
17	78 230	88 158	11 842	90 072	43
18	78 246	88 184	11 816	90 063	42
19	78 263	88 210	11 790	90 053	41
20	78 280	88 236	11 764	90 043	40
21	78 296	88 262	11 738	90 034	39
22	78 313	88 289	11 711	90 024	38
23	78 329	88 315	11 685	90 014	37
24	78 346	88 341	11 659	90 005	36
25	78 362	88 367	11 633	89 995	35
26	78 379	88 393	11 607	89 985	34
27	78 395	88 420	11 580	89 976	33
28	78 412	88 446	11 554	89 966	32
29	78 428	88 472	11 528	89 956	31
30	78 445	88 498	11 502	89 947	30
31	78 461	88 524	11 476	89 937	29
32	78 478	88 550	11 450	89 927	28
33	78 494	88 577	11 423	89 918	27
34	78 510	88 603	11 397	89 908	26
35	78 527	88 629	11 371	89 898	25
36	78 543	88 655	11 345	89 888	24
37	78 560	88 681	11 319	89 879	23
38	78 576	88 707	11 293	89 869	22
39	78 592	88 733	11 267	89 859	21
40	78 609	88 759	11 241	89 849	20
41	78 625	88 786	11 214	89 840	19
42	78 642	88 812	11 188	89 830	18
43	78 658	88 838	11 162	89 820	17
44	78 674	88 864	11 136	89 810	16
45	78 691	88 890	11 110	89 801	15
46	78 707	88 916	11 084	89 791	14
47	78 723	88 942	11 058	89 781	13
48	78 739	88 968	11 032	89 771	12
49	78 756	88 994	11 006	89 761	11
50	78 772	89 020	10 980	89 752	10
51	78 788	89 046	10 954	89 742	9
52	78 805	89 073	10 927	89 732	8
53	78 821	89 099	10 901	89 722	7
54	78 837	89 125	10 875	89 712	6
55	78 853	89 151	10 849	89 702	5
56	78 869	89 177	10 823	89 693	4
57	78 886	89 203	10 797	89 683	3
58	78 902	89 229	10 771	89 673	2
59	78 918	89 255	10 745	89 663	1
60	78 934	89 281	10 719	89 653	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

52°

38°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	78 934	89 281	10 719	89 653	60
1	78 950	89 307	10 693	89 643	59
2	78 967	89 333	10 667	89 633	58
3	78 983	89 359	10 641	89 624	57
4	78 999	89 385	10 615	89 614	56
5	79 015	89 411	10 589	89 604	55
6	79 031	89 437	10 563	89 594	54
7	79 047	89 463	10 537	89 584	53
8	79 063	89 489	10 511	89 574	52
9	79 079	89 515	10 485	89 564	51
10	79 095	89 541	10 459	89 554	50
11	79 111	89 567	10 433	89 544	49
12	79 128	89 593	10 407	89 534	48
13	79 144	89 619	10 381	89 524	47
14	79 160	89 645	10 355	89 514	46
15	79 176	89 671	10 329	89 504	45
16	79 192	89 697	10 303	89 495	44
17	79 208	89 723	10 277	89 485	43
18	79 224	89 749	10 251	89 475	42
19	79 240	89 775	10 225	89 465	41
20	79 256	89 801	10 199	89 455	40
21	79 272	89 827	10 173	89 445	39
22	79 288	89 853	10 147	89 435	38
23	79 304	89 879	10 121	89 425	37
24	79 319	89 905	10 095	89 415	36
25	79 335	89 931	10 069	89 405	35
26	79 351	89 957	10 043	89 395	34
27	79 367	89 983	10 017	89 385	33
28	79 383	90 009	09 991	89 375	32
29	79 399	90 035	09 965	89 364	31
30	79 415	90 061	09 939	89 354	30
31	79 431	90 086	09 914	89 344	29
32	79 447	90 112	09 888	89 334	28
33	79 463	90 138	09 862	89 324	27
34	79 478	90 164	09 836	89 314	26
35	79 494	90 190	09 810	89 304	25
36	79 510	90 216	09 784	89 294	24
37	79 526	90 242	09 758	89 284	23
38	79 542	90 268	09 732	89 274	22
39	79 558	90 294	09 706	89 264	21
40	79 573	90 320	09 680	89 254	20
41	79 589	90 346	09 654	89 244	19
42	79 605	90 371	09 629	89 233	18
43	79 621	90 397	09 603	89 223	17
44	79 636	90 423	09 577	89 213	16
45	79 652	90 449	09 551	89 203	15
46	79 668	90 475	09 525	89 193	14
47	79 684	90 501	09 499	89 183	13
48	79 699	90 527	09 473	89 173	12
49	79 715	90 553	09 447	89 162	11
50	79 731	90 578	09 422	89 152	10
51	79 746	90 604	09 396	89 142	9
52	79 762	90 630	09 370	89 132	8
53	79 778	90 656	09 344	89 122	7
54	79 793	90 682	09 318	89 112	6
55	79 809	90 708	09 292	89 101	5
56	79 825	90 734	09 266	89 091	4
57	79 840	90 759	09 241	89 081	3
58	79 856	90 785	09 215	89 071	2
59	79 872	90 811	09 189	89 060	1
60	79 887	90 837	09 163	89 050	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

51°

39°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	79 887	90 837	09 163	89 050	60
1	79 903	90 863	09 137	89 040	59
2	79 918	90 889	09 111	89 030	58
3	79 934	90 914	09 086	89 020	57
4	79 950	90 940	09 060	89 009	56
5	79 965	90 966	09 034	88 999	55
6	79 981	90 992	09 008	88 989	54
7	79 996	91 018	08 982	88 978	53
8	80 012	91 043	08 957	88 968	52
9	80 027	91 069	08 931	88 958	51
10	80 043	91 095	08 905	88 948	50
11	80 058	91 121	08 879	88 937	49
12	80 074	91 147	08 853	88 927	48
13	80 089	91 172	08 828	88 917	47
14	80 105	91 198	08 802	88 906	46
15	80 120	91 224	08 776	88 896	45
16	80 136	91 250	08 750	88 886	44
17	80 151	91 276	08 724	88 875	43
18	80 166	91 301	08 699	88 865	42
19	80 182	91 327	08 673	88 855	41
20	80 197	91 353	08 647	88 844	40
21	80 213	91 379	08 621	88 834	39
22	80 228	91 404	08 596	88 824	38
23	80 244	91 430	08 570	88 813	37
24	80 259	91 456	08 544	88 803	36
25	80 274	91 482	08 518	88 793	35
26	80 290	91 507	08 493	88 782	34
27	80 305	91 533	08 467	88 772	33
28	80 320	91 559	08 441	88 761	32
29	80 336	91 585	08 415	88 751	31
30	80 351	91 610	08 390	88 741	30
31	80 366	91 636	08 364	88 730	29
32	80 382	91 662	08 338	88 720	28
33	80 397	91 688	08 312	88 709	27
34	80 412	91 713	08 287	88 699	26
35	80 428	91 739	08 261	88 688	25
36	80 443	91 765	08 235	88 678	24
37	80 458	91 791	08 209	88 668	23
38	80 473	91 816	08 184	88 657	22
39	80 489	91 842	08 158	88 647	21
40	80 504	91 868	08 132	88 636	20
41	80 519	91 893	08 107	88 626	19
42	80 534	91 919	08 081	88 615	18
43	80 550	91 945	08 055	88 605	17
44	80 565	91 971	08 029	88 594	16
45	80 580	91 996	08 004	88 584	15
46	80 595	92 022	07 978	88 573	14
47	80 610	92 048	07 952	88 563	13
48	80 625	92 073	07 927	88 552	12
49	80 641	92 099	07 901	88 542	11
50	80 656	92 125	07 875	88 531	10
51	80 671	92 150	07 850	88 521	9
52	80 686	92 176	07 824	88 510	8
53	80 701	92 202	07 798	88 499	7
54	80 716	92 227	07 773	88 489	6
55	80 731	92 253	07 747	88 478	5
56	80 746	92 279	07 721	88 468	4
57	80 762	92 304	07 696	88 457	3
58	80 777	92 330	07 670	88 447	2
59	80 792	92 356	07 644	88 436	1
60	80 807	92 381	07 619	88 425	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

50°

40°

′	log sin	log tan	log cot	log cos	′
	9	9	10	9	
0	80 807	92 381	07 619	88 425	60
1	80 822	92 407	07 593	88 415	59
2	80 837	92 433	07 567	88 404	58
3	80 852	92 458	07 542	88 394	57
4	80 867	92 484	07 516	88 383	56
5	80 882	92 510	07 490	88 372	55
6	80 897	92 535	07 465	88 362	54
7	80 912	92 561	07 439	88 351	53
8	80 927	92 587	07 413	88 340	52
9	80 942	92 612	07 388	88 330	51
10	80 957	92 638	07 362	88 319	50
11	80 972	92 663	07 337	88 308	49
12	80 987	92 689	07 311	88 298	48
13	81 002	92 715	07 285	88 287	47
14	81 017	92 740	07 260	88 276	46
15	81 032	92 766	07 234	88 266	45
16	81 047	92 792	07 208	88 255	44
17	81 061	92 817	07 183	88 244	43
18	81 076	92 843	07 157	88 234	42
19	81 091	92 868	07 132	88 223	41
20	81 106	92 894	07 106	88 212	40
21	81 121	92 920	07 080	88 201	39
22	81 136	92 945	07 055	88 191	38
23	81 151	92 971	07 029	88 180	37
24	81 166	92 996	07 004	88 169	36
25	81 180	93 022	06 978	88 158	35
26	81 195	93 048	06 952	88 148	34
27	81 210	93 073	06 927	88 137	33
28	81 225	93 099	06 901	88 126	32
29	81 240	93 124	06 876	88 115	31
30	81 254	93 150	06 850	88 105	30
31	81 269	93 175	06 825	88 094	29
32	81 284	93 201	06 799	88 083	28
33	81 299	93 227	06 773	88 072	27
34	81 314	93 252	06 748	88 061	26
35	81 328	93 278	06 722	88 051	25
36	81 343	93 303	06 697	88 040	24
37	81 358	93 329	06 671	88 029	23
38	81 372	93 354	06 646	88 018	22
39	81 387	93 380	06 620	88 007	21
40	81 402	93 406	06 594	87 996	20
41	81 417	93 431	06 569	87 985	19
42	81 431	93 457	06 543	87 975	18
43	81 446	93 482	06 518	87 964	17
44	81 461	93 508	06 492	87 953	16
45	81 475	93 533	06 467	87 942	15
46	81 490	93 559	06 441	87 931	14
47	81 505	93 584	06 416	87 920	13
48	81 519	93 610	06 390	87 909	12
49	81 534	93 636	06 364	87 898	11
50	81 549	93 661	06 339	87 887	10
51	81 563	93 687	06 313	87 877	9
52	81 578	93 712	06 288	87 866	8
53	81 592	93 738	06 262	87 855	7
54	81 607	93 763	06 237	87 844	6
55	81 622	93 789	06 211	87 833	5
56	81 636	93 814	06 186	87 822	4
57	81 651	93 840	06 160	87 811	3
58	81 665	93 865	06 135	87 800	2
59	81 680	93 891	06 109	87 789	1
60	81 694	93 916	06 084	87 778	0
	9	9	10	9	
′	log cos	log cot	log tan	log sin	′

49°

41°

′	log sin	log tan	log cot	log cos	′
	—9—	—9—	—10—	—9—	
0	81 694	93 916	06 084	87 778	60
1	81 709	93 942	06 058	87 767	59
2	81 723	93 967	06 033	87 756	58
3	81 738	93 993	06 007	87 745	57
4	81 752	94 018	05 982	87 734	56
5	81 767	94 044	05 956	87 723	55
6	81 781	94 069	05 931	87 712	54
7	81 796	94 095	05 905	87 701	53
8	81 810	94 120	05 880	87 690	52
9	81 825	94 146	05 854	87 679	51
10	81 839	94 171	05 829	87 668	50
11	81 854	94 197	05 803	87 657	49
12	81 868	94 222	05 778	87 646	48
13	81 882	94 248	05 752	87 635	47
14	81 897	94 273	05 727	87 624	46
15	81 911	94 299	05 701	87 613	45
16	81 926	94 324	05 676	87 601	44
17	81 940	94 350	05 650	87 590	43
18	81 955	94 375	05 625	87 579	42
19	81 969	94 401	05 599	87 568	41
20	81 983	94 426	05 574	87 557	40
21	81 998	94 452	05 548	87 546	39
22	82 012	94 477	05 523	87 535	38
23	82 026	94 503	05 497	87 524	37
24	82 041	94 528	05 472	87 513	36
25	82 055	94 554	05 446	87 501	35
26	82 069	94 579	05 421	87 490	34
27	82 084	94 604	05 396	87 479	33
28	82 098	94 630	05 370	87 468	32
29	82 112	94 655	05 345	87 457	31
30	82 126	94 681	05 319	87 446	30
31	82 141	94 706	05 294	87 434	29
32	82 155	94 732	05 268	87 423	28
33	82 169	94 757	05 243	87 412	27
34	82 184	94 783	05 217	87 401	26
35	82 198	94 808	05 192	87 390	25
36	82 212	94 834	05 166	87 378	24
37	82 226	94 859	05 141	87 367	23
38	82 240	94 884	05 116	87 356	22
39	82 255	94 910	05 090	87 345	21
40	82 269	94 935	05 065	87 334	20
41	82 283	94 961	05 039	87 322	19
42	82 297	94 986	05 014	87 311	18
43	82 311	95 012	04 988	87 300	17
44	82 326	95 037	04 963	87 288	16
45	82 340	95 062	04 938	87 277	15
46	82 354	95 088	04 912	87 266	14
47	82 368	95 113	04 887	87 255	13
48	82 382	95 139	04 861	87 243	12
49	82 396	95 164	04 836	87 232	11
50	82 410	95 190	04 810	87 221	10
51	82 424	95 215	04 785	87 209	9
52	82 439	95 240	04 760	87 198	8
53	82 453	95 266	04 734	87 187	7
54	82 467	95 291	04 709	87 175	6
55	82 481	95 317	04 683	87 164	5
56	82 495	95 342	04 658	87 153	4
57	82 509	95 368	04 632	87 141	3
58	82 523	95 393	04 607	87 130	2
59	82 537	95 418	04 582	87 119	1
60	82 551	95 444	04 556	87 107	0
	—9—	—9—	—10—	—9—	
′	log cos	log cot	log tan	log sin	′

48°

42°

′	log sin	log tan	log cot	log cos	′
	—9—	—9—	—10—	—9—	
0	82 551	95 444	04 556	87 107	60
1	82 565	95 469	04 531	87 096	59
2	82 579	95 495	04 505	87 085	58
3	82 593	95 520	04 480	87 073	57
4	82 607	95 545	04 455	87 062	56
5	82 621	95 571	04 429	87 050	55
6	82 635	95 596	04 404	87 039	54
7	82 649	95 622	04 378	87 028	53
8	82 663	95 647	04 353	87 016	52
9	82 677	95 672	04 328	87 005	51
10	82 691	95 698	04 302	86 993	50
11	82 705	95 723	04 277	86 982	49
12	82 719	95 748	04 252	86 970	48
13	82 733	95 774	04 226	86 959	47
14	82 747	95 799	04 201	86 947	46
15	82 761	95 825	04 175	86 936	45
16	82 775	95 850	04 150	86 924	44
17	82 788	95 875	04 125	86 913	43
18	82 802	95 901	04 099	86 902	42
19	82 816	95 926	04 074	86 890	41
20	82 830	95 952	04 048	86 879	40
21	82 844	95 977	04 023	86 867	39
22	82 858	96 002	03 998	86 855	38
23	82 872	96 028	03 972	86 844	37
24	82 885	96 053	03 947	86 832	36
25	82 899	96 078	03 922	86 821	35
26	82 913	96 104	03 896	86 809	34
27	82 927	96 129	03 871	86 798	33
28	82 941	96 155	03 845	86 786	32
29	82 955	96 180	03 820	86 775	31
30	82 968	96 205	03 795	86 763	30
31	82 982	96 231	03 769	86 752	29
32	82 996	96 256	03 744	86 740	28
33	83 010	96 281	03 719	86 728	27
34	83 023	96 307	03 693	86 717	26
35	83 037	96 332	03 668	86 705	25
36	83 051	96 357	03 643	86 694	24
37	83 065	96 383	03 617	86 682	23
38	83 078	96 408	03 592	86 670	22
39	83 092	96 433	03 567	86 659	21
40	83 106	96 459	03 541	86 647	20
41	83 120	96 484	03 516	86 635	19
42	83 133	96 510	03 490	86 624	18
43	83 147	96 535	03 465	86 612	17
44	83 161	96 560	03 440	86 600	16
45	83 174	96 586	03 414	86 589	15
46	83 188	96 611	03 389	86 577	14
47	83 202	96 636	03 364	86 565	13
48	83 215	96 662	03 338	86 554	12
49	83 229	96 687	03 313	86 542	11
50	83 242	96 712	03 288	86 530	10
51	83 256	96 738	03 262	86 518	9
52	83 270	96 763	03 237	86 507	8
53	83 283	96 788	03 212	86 495	7
54	83 297	96 814	03 186	86 483	6
55	83 310	96 839	03 161	86 472	5
56	83 324	96 864	03 136	86 460	4
57	83 338	96 890	03 110	86 448	3
58	83 351	96 915	03 085	86 436	2
59	83 365	96 940	03 060	86 425	1
60	83 378	96 966	03 034	86 413	0
	—9—	—9—	—10—	—9—	
′	log cos	log cot	log tan	log sin	′

47°

43°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	83 378	96 966	03 034	86 413	60
1	83 392	96 991	03 009	86 401	59
2	83 405	97 016	02 984	86 389	58
3	83 419	97 042	02 958	86 377	57
4	83 432	97 067	02 933	86 366	56
5	83 446	97 092	02 908	86 354	55
6	83 459	97 118	02 882	86 342	54
7	83 473	97 143	02 857	86 330	53
8	83 486	97 168	02 832	86 318	52
9	83 500	97 193	02 807	86 306	51
10	83 513	97 219	02 781	86 295	50
11	83 527	97 244	02 756	86 283	49
12	83 540	97 269	02 731	86 271	48
13	83 554	97 295	02 705	86 259	47
14	83 567	97 320	02 680	86 247	46
15	83 581	97 345	02 655	86 235	45
16	83 594	97 371	02 629	86 223	44
17	83 608	97 396	02 604	86 211	43
18	83 621	97 421	02 579	86 200	42
19	83 634	97 447	02 553	86 188	41
20	83 648	97 472	02 528	86 176	40
21	83 661	97 497	02 503	86 164	39
22	83 674	97 523	02 477	86 152	38
23	83 688	97 548	02 452	86 140	37
24	83 701	97 573	02 427	86 128	36
25	83 715	97 598	02 402	86 116	35
26	83 728	97 624	02 376	86 104	34
27	83 741	97 649	02 351	86 092	33
28	83 755	97 674	02 326	86 080	32
29	83 768	97 700	02 300	86 068	31
30	83 781	97 725	02 275	86 056	30
31	83 795	97 750	02 250	86 044	29
32	83 808	97 776	02 224	86 032	28
33	83 821	97 801	02 199	86 020	27
34	83 834	97 826	02 174	86 008	26
35	83 848	97 851	02 149	85 996	25
36	83 861	97 877	02 123	85 984	24
37	83 874	97 902	02 098	85 972	23
38	83 887	97 927	02 073	85 960	22
39	83 901	97 953	02 047	85 948	21
40	83 914	97 978	02 022	85 936	20
41	83 927	98 003	01 997	85 924	19
42	83 940	98 029	01 971	85 912	18
43	83 954	98 054	01 946	85 900	17
44	83 967	98 079	01 921	85 888	16
45	83 980	98 104	01 896	85 876	15
46	83 993	98 130	01 870	85 864	14
47	84 006	98 155	01 845	85 851	13
48	84 020	98 180	01 820	85 839	12
49	84 033	98 206	01 794	85 827	11
50	84 046	98 231	01 769	85 815	10
51	84 059	98 256	01 744	85 803	9
52	84 072	98 281	01 719	85 791	8
53	84 085	98 307	01 693	85 779	7
54	84 098	98 332	01 668	85 766	6
55	84 112	98 357	01 643	85 754	5
56	84 125	98 383	01 617	85 742	4
57	84 138	98 408	01 592	85 730	3
58	84 151	98 433	01 567	85 718	2
59	84 164	98 458	01 542	85 706	1
60	84 177	98 484	01 516	85 693	0
′	9 log cos	9 log cot	10 log tan	9 log sin	′

46°

44°

′	log sin 9	log tan 9	log cot 10	log cos 9	′
0	84 177	98 484	01 516	85 693	60
1	84 190	98 509	01 491	85 681	59
2	84 203	98 534	01 466	85 669	58
3	84 216	98 560	01 440	85 657	57
4	84 229	98 585	01 415	85 645	56
5	84 242	98 610	01 390	85 632	55
6	84 255	98 635	01 365	85 620	54
7	84 269	98 661	01 339	85 608	53
8	84 282	98 686	01 314	85 596	52
9	84 295	98 711	01 289	85 583	51
10	84 308	98 737	01 263	85 571	50
11	84 321	98 762	01 238	85 559	49
12	84 334	98 787	01 213	85 547	48
13	84 347	98 812	01 188	85 534	47
14	84 360	98 838	01 162	85 522	46
15	84 373	98 863	01 137	85 510	45
16	84 385	98 888	01 112	85 497	44
17	84 398	98 913	01 087	85 485	43
18	84 411	98 939	01 061	85 473	42
19	84 424	98 964	01 036	85 460	41
20	84 437	98 989	01 011	85 448	40
21	84 450	99 015	00 985	85 436	39
22	84 463	99 040	00 960	85 423	38
23	84 476	99 065	00 935	85 411	37
24	84 489	99 090	00 910	85 399	36
25	84 502	99 116	00 884	85 386	35
26	84 515	99 141	00 859	85 374	34
27	84 528	99 166	00 834	85 361	33
28	84 540	99 191	00 809	85 349	32
29	84 553	99 217	00 783	85 337	31
30	84 566	99 242	00 758	85 324	30
31	84 579	99 267	00 733	85 312	29
32	84 592	99 293	00 707	85 299	28
33	84 605	99 318	00 682	85 287	27
34	84 618	99 343	00 657	85 274	26
35	84 630	99 368	00 632	85 262	25
36	84 643	99 394	00 606	85 250	24
37	84 656	99 419	00 581	85 237	23
38	84 669	99 444	00 556	85 225	22
39	84 682	99 469	00 531	85 212	21
40	84 694	99 495	00 505	85 200	20
41	84 707	99 520	00 480	85 187	19
42	84 720	99 545	00 455	85 175	18
43	84 733	99 570	00 430	85 162	17
44	84 745	99 596	00 404	85 150	16
45	84 758	99 621	00 379	85 137	15
46	84 771	99 646	00 354	85 125	14
47	84 784	99 672	00 328	85 112	13
48	84 796	99 697	00 303	85 100	12
49	84 809	99 722	00 278	85 087	11
50	84 822	99 747	00 253	85 074	10
51	84 835	99 773	00 227	85 062	9
52	84 847	99 798	00 202	85 049	8
53	84 860	99 823	00 177	85 037	7
54	84 873	99 848	00 152	85 024	6
55	84 885	99 874	00 126	85 012	5
56	84 898	99 899	00 101	84 999	4
57	84 911	99 924	00 076	84 986	3
58	84 923	99 949	00 051	84 974	2
59	84 936	99 975	00 025	84 961	1
60	84 949	00 000	00 000	84 949	0
′	9 log cos	10 log cot	10 log tan	9 log sin	′

45°

TABLE IV.

FOR DETERMINING WITH GREATER ACCURACY THAN CAN BE DONE BY MEANS OF TABLE III.:

1. *log sin*, *log tan*, and *log cot*, when the angle is between 0° and 2°;
2. *log cos*, *log tan*, and *log cot*, when the angle is between 88° and 90°;
3. The value of the angle when the logarithm of the function does *not* lie between the limits 8.54 684 and 11.45 316.

FORMULAS FOR THE USE OF THE NUMBERS S AND T.

I. When the angle a is between 0° and 2°:

$\log \sin a = \log a'' + S.$ | $\log a'' = \log \sin a - S,$

$\log \tan a = \log a'' + T.$ | $\quad = \log \tan a - T,$

$\log \cot a = \operatorname{colog} \tan a.$ | $\quad = \operatorname{colog} \cot a - T.$

II. When the angle a is between 88° and 90°:

$\log \cos a = \log (90° - a)'' + S.$ | $\log (90° - a)'' = \log \cos a - S,$

$\log \cot a = \log (90° - a)'' + T.$ | $\quad = \log \cot a - T,$

$\log \tan a = \operatorname{colog} \cot a.$ | $\quad = \operatorname{colog} \tan a - T,$

and $a = 90° - (90° - a)$.

VALUES OF S AND T.

a''	S	log sin a
0		—
	4.68 557	
2 409		8.06 740
	4.68 556	
3 417		8.21 920
	4.68 555	
3 823		8.26 795
	4.68 555	
4 190		8.30 776
	4.68 554	
4 840		8.37 038
	4.68 553	
5 414		8.41 904
	4.68 552	
5 932		8.45 872
	4.68 551	
6 408		8.49 223
	4.68 550	
6 633		8.50 721
	4.68 550	
6 851		8.52 125
	4.68 549	
7 267		8.54 684
a''	S	log sin a

a''	T	log tan a
0		—
	4.68 557	
200		6.98 660
	4.68 558	
1 726		7.92 263
	4.68 559	
2 432		8.07 156
	4.68 560	
2 976		8.15 924
	4.68 561	
3 434		8.22 142
	4.68 562	
3 838		8.26 973
	4.68 563	
4 204		8.30 930
	4.68 564	
4 540		8.34 270
	4.68 565	
4 699		8.35 766
	4.68 565	
4 853		8.37 167
	4.68 566	
5 146		8.39 713
a''	T	log tan a

a	T	log tan a
5 146		8.39 713
	4.68 567	
5 424		8.41 999
	4.68 568	
5 689		8.44 072
	4.68 569	
5 941		8.45 955
	4.68 570	
6 184		8.47 697
	4.68 571	
6 417		8.49 305
	4.68 572	
6 642		8.50 802
	4.68 573	
6 859		8.52 200
	4.68 574	
7 070		8.53 516
	4.68 575	
7 173		8.54 145
	4.68 575	
7 274		8.54 753
a	T	log tan a

TABLE V.

THE NATURAL VALUES
OF
SINES, COSINES, TANGENTS, AND COTANGENTS,
IN THE UNIT CIRCLE.

0°—8°

° ′	sin	tan	cot	cos	′ °
0 0	0.0000	0.0000	infinite	1.0000	0 90
10	0.0029	0.0029	343.7737	1.0000	50
20	0.0058	0.0058	171.8854	1.0000	40
30	0.0087	0.0087	114.5887	1.0000	30
40	0.0116	0.0116	85.9398	0.9999	20
50	0.0145	0.0145	68.7501	0.9999	10
1 0	0.0175	0.0175	57.2900	0.9998	0 89
° ′	cos	cot	tan	sin	′ °

° ′	sin	tan	cot	cos	′ °
1 0	0.0175	0.0175	57.2900	0.9998	0 89
10	0.0204	0.0204	49.1039	0.9998	50
20	0.0233	0.0233	42.9641	0.9997	40
30	0.0262	0.0262	38.1885	0.9997	30
40	0.0291	0.0291	34.3678	0.9996	20
50	0.0320	0.0320	31.2416	0.9995	10
2 0	0.0349	0.0349	28.6363	0.9994	0 88
10	0.0378	0.0378	26.4316	0.9993	50
20	0.0407	0.0407	24.5418	0.9992	40
30	0.0436	0.0437	22.9038	0.9990	30
40	0.0465	0.0466	21.4704	0.9989	20
50	0.0494	0.0495	20.2056	0.9988	10
3 0	0.0523	0.0524	19.0811	0.9986	0 87
10	0.0552	0.0553	18.0750	0.9985	50
20	0.0581	0.0582	17.1693	0.9983	40
30	0.0610	0.0612	16.3499	0.9981	30
40	0.0640	0.0641	15.6048	0.9980	20
50	0.0669	0.0670	14.9244	0.9978	10
4 0	0.0698	0.0699	14.3007	0.9976	0 86
10	0.0727	0.0729	13.7267	0.9974	50
20	0.0756	0.0758	13.1969	0.9971	40
30	0.0785	0.0787	12.7062	0.9969	30
40	0.0814	0.0816	12.2505	0.9967	20
50	0.0843	0.0846	11.8262	0.9964	10
5 0	0.0872	0.0875	11.4301	0.9962	0 85
° ′	cos	cot	tan	sin	′ °

° ′	sin	tan	cot	cos	′ °
5 0	0.0872	0.0875	11.4301	0.9962	0 85
10	0.0901	0.0904	11.0594	0.9959	50
20	0.0929	0.0934	10.7119	0.9957	40
30	0.0958	0.0963	10.3854	0.9954	30
40	0.0987	0.0992	10.0780	0.9951	20
50	0.1016	0.1022	9.7882	0.9948	10
6 0	0.1045	0.1051	9.5144	0.9945	0 84
10	0.1074	0.1080	9.2553	0.9942	50
20	0.1103	0.1110	9.0098	0.9939	40
30	0.1132	0.1139	8.7769	0.9936	30
40	0.1161	0.1169	8.5555	0.9932	20
50	0.1190	0.1198	8.3450	0.9929	10
7 0	0.1219	0.1228	8.1443	0.9925	0 83
10	0.1248	0.1257	7.9530	0.9922	50
20	0.1276	0.1287	7.7704	0.9918	40
30	0.1305	0.1317	7.5958	0.9914	30
40	0.1334	0.1346	7.4287	0.9911	20
50	0.1363	0.1376	7.2687	0.9907	10
8 0	0.1392	0.1405	7.1154	0.9903	0 82
10	0.1421	0.1435	6.9682	0.9899	50
20	0.1449	0.1465	6.8269	0.9894	40
30	0.1478	0.1495	6.6912	0.9890	30
40	0.1507	0.1524	6.5606	0.9886	20
50	0.1536	0.1554	6.4348	0.9881	10
9 0	0.1564	0.1584	6.3138	0.9877	0 81
° ′	cos	cot	tan	sin	′ °

81°—89°

° ′	sin	tan	cot	cos	′ °	° ′	sin	tan	cot	cos	′ °
9 0	0.1564	0.1584	6.3138	0.9877	0 81	18 0	0.3090	0.3249	3.0777	0.9511	0 72
10	0.1593	0.1614	6.1970	0.9872	50	10	0.3118	0.3281	3.0475	0.9502	50
20	0.1622	0.1644	6.0844	0.9868	40	20	0.3145	0.3314	3.0178	0.9492	40
30	0.1650	0.1673	5.9758	0.9863	30	30	0.3173	0.3346	2.9887	0.9483	30
40	0.1679	0.1703	5.8708	0.9858	20	40	0.3201	0.3378	2.9600	0.9474	20
50	0.1708	0.1733	5.7694	0.9853	10	50	0.3228	0.3411	2.9319	0.9465	10
10 0	0.1736	0.1763	5.6713	0.9848	0 80	19 0	0.3256	0.3443	2.9042	0.9455	0 71
10	0.1765	0.1793	5.5764	0.9843	50	10	0.3283	0.3476	2.8770	0.9446	50
20	0.1794	0.1823	5.4845	0.9838	40	20	0.3311	0.3508	2.8502	0.9436	40
30	0.1822	0.1853	5.3955	0.9833	30	30	0.3338	0.3541	2.8239	0.9426	30
40	0.1851	0.1883	5.3093	0.9827	20	40	0.3365	0.3574	2.7980	0.9417	20
50	0.1880	0.1914	5.2257	0.9822	10	50	0.3393	0.3607	2.7725	0.9407	10
11 0	0.1908	0.1944	5.1446	0.9816	0 79	20 0	0.3420	0.3640	2.7475	0.9397	0 70
10	0.1937	0.1974	5.0658	0.9811	50	10	0.3448	0.3673	2.7228	0.9387	50
20	0.1965	0.2004	4.9894	0.9805	40	20	0.3475	0.3706	2.6985	0.9377	40
30	0.1994	0.2035	4.9152	0.9799	30	30	0.3502	0.3739	2.6746	0.9367	30
40	0.2022	0.2065	4.8430	0.9793	20	40	0.3529	0.3772	2.6511	0.9356	20
50	0.2051	0.2095	4.7729	0.9787	10	50	0.3557	0.3805	2.6279	0.9346	10
12 0	0.2079	0.2126	4.7046	0.9781	0 78	21 0	0.3584	0.3839	2.6051	0.9336	0 69
10	0.2108	0.2156	4.6382	0.9775	50	10	0.3611	0.3872	2.5826	0.9325	50
20	0.2136	0.2186	4.5736	0.9769	40	20	0.3638	0.3906	2.5605	0.9315	40
30	0.2164	0.2217	4.5107	0.9763	30	30	0.3665	0.3939	2.5386	0.9304	30
40	0.2193	0.2247	4.4494	0.9757	20	40	0.3692	0.3973	2.5172	0.9293	20
50	0.2221	0.2278	4.3897	0.9750	10	50	0.3719	0.4006	2.4960	0.9283	10
13 0	0.2250	0.2309	4.3315	0.9744	0 77	22 0	0.3746	0.4040	2.4751	0.9272	0 68
10	0.2278	0.2339	4.2747	0.9737	50	10	0.3773	0.4074	2.4545	0.9261	50
20	0.2306	0.2370	4.2193	0.9730	40	20	0.3800	0.4108	2.4342	0.9250	40
30	0.2334	0.2401	4.1653	0.9724	30	30	0.3827	0.4142	2.4142	0.9239	30
40	0.2363	0.2432	4.1126	0.9717	20	40	0.3854	0.4176	2.3945	0.9228	20
50	0.2391	0.2462	4.0611	0.9710	10	50	0.3881	0.4210	2.3750	0.9216	10
14 0	0.2419	0.2493	4.0108	0.9703	0 76	23 0	0.3907	0.4245	2.3559	0.9205	0 67
10	0.2447	0.2524	3.9617	0.9696	50	10	0.3934	0.4279	2.3369	0.9194	50
20	0.2476	0.2555	3.9136	0.9689	40	20	0.3961	0.4314	2.3183	0.9182	40
30	0.2504	0.2586	3.8667	0.9681	30	30	0.3987	0.4348	2.2998	0.9171	30
40	0.2532	0.2617	3.8208	0.9674	20	40	0.4014	0.4383	2.2817	0.9159	20
50	0.2560	0.2648	3.7760	0.9667	10	50	0.4041	0.4417	2.2637	0.9147	10
15 0	0.2588	0.2679	3.7321	0.9659	0 75	24 0	0.4067	0.4452	2.2460	0.9135	0 66
10	0.2616	0.2711	3.6891	0.9652	50	10	0.4094	0.4487	2.2286	0.9124	50
20	0.2644	0.2742	3.6470	0.9644	40	20	0.4120	0.4522	2.2113	0.9112	40
30	0.2672	0.2773	3.6059	0.9636	30	30	0.4147	0.4557	2.1943	0.9100	30
40	0.2700	0.2805	3.5656	0.9628	20	40	0.4173	0.4592	2.1775	0.9088	20
50	0.2728	0.2836	3.5261	0.9621	10	50	0.4200	0.4628	2.1609	0.9075	10
16 0	0.2756	0.2867	3.4874	0.9613	0 74	25 0	0.4226	0.4663	2.1445	0.9063	0 65
10	0.2784	0.2899	3.4495	0.9605	50	10	0.4253	0.4699	2.1283	0.9051	50
20	0.2812	0.2931	3.4124	0.9596	40	20	0.4279	0.4734	2.1123	0.9038	40
30	0.2840	0.2962	3.3759	0.9588	30	30	0.4305	0.4770	2.0965	0.9026	30
40	0.2868	0.2994	3.3402	0.9580	20	40	0.4331	0.4806	2.0809	0.9013	20
50	0.2896	0.3026	3.3052	0.9572	10	50	0.4358	0.4841	2.0655	0.9001	10
17 0	0.2924	0.3057	3.2709	0.9563	0 73	26 0	0.4384	0.4877	2.0503	0.8988	0 64
10	0.2952	0.3089	3.2371	0.9555	50	10	0.4410	0.4913	2.0353	0.8975	50
20	0.2979	0.3121	3.2041	0.9546	40	20	0.4436	0.4950	2.0204	0.8962	40
30	0.3007	0.3153	3.1716	0.9537	30	30	0.4462	0.4986	2.0057	0.8949	30
40	0.3035	0.3185	3.1397	0.9528	20	40	0.4488	0.5022	1.9912	0.8936	20
50	0.3062	0.3217	3.1084	0.9520	10	50	0.4514	0.5059	1.9768	0.8923	10
18 0	0.3090	0.3249	3.0777	0.9511	0 72	27 0	0.4540	0.5095	1.9626	0.8910	0 63
° ′	cos	cot	tan	sin	′ °	° ′	cos	cot	tan	sin	′ °

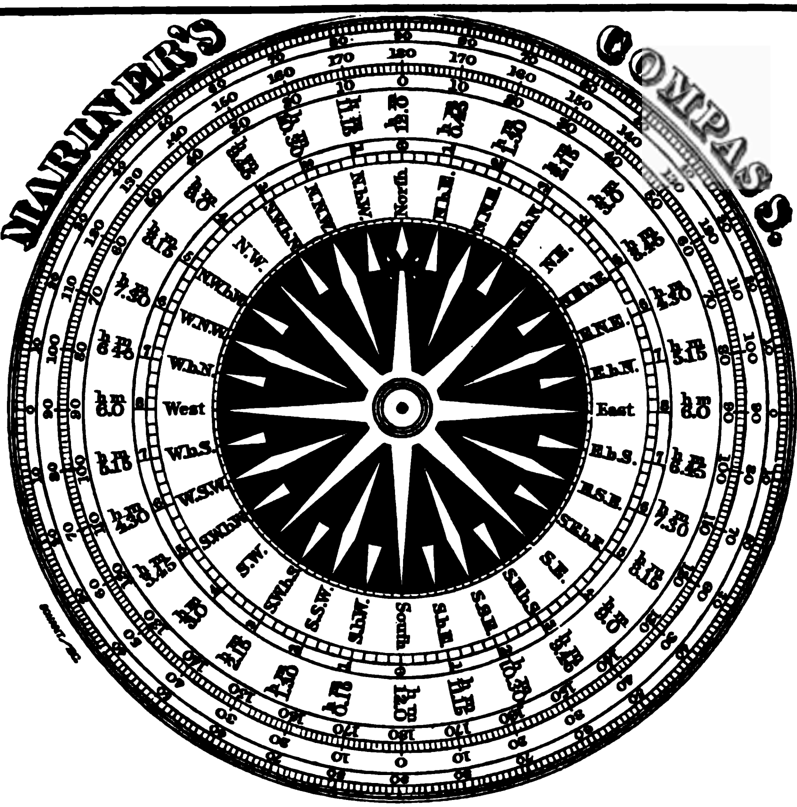
° ′	sin	tan	cot	cos	′ °	° ′	sin	tan	cot	cos	′ °
27 0	0.4540	0.5095	1.9626	0.8910	0 **63**	**36** 0	0.5878	0.7265	1.3764	0.8090	0 **54**
10	0.4566	0.5132	1.9486	0.8897	50	10	0.5901	0.7310	1.3680	0.8073	50
20	0.4592	0.5169	1.9347	0.8884	40	20	0.5925	0.7355	1.3597	0.8056	40
30	0.4617	0.5206	1.9210	0.8870	30	30	0.5948	0.7400	1.3514	0.8039	30
40	0.4643	0.5243	1.9074	0.8857	20	40	0.5972	0.7445	1.3432	0.8021	20
50	0.4669	0.5280	1.8940	0.8843	10	50	0.5995	0.7490	1.3351	0.8004	10
28 0	0.4695	0.5317	1.8807	0.8829	0 **62**	**37** 0	0.6018	0.7536	1.3270	0.7986	0 **53**
10	0.4720	0.5354	1.8676	0.8816	50	10	0.6041	0.7581	1.3190	0.7969	50
20	0.4746	0.5392	1.8546	0.8802	40	20	0.6065	0.7627	1.3111	0.7951	40
30	0.4772	0.5430	1.8418	0.8788	30	30	0.6088	0.7673	1.3032	0.7934	30
40	0.4797	0.5467	1.8291	0.8774	20	40	0.6111	0.7720	1.2954	0.7916	20
50	0.4823	0.5505	1.8165	0.8760	10	50	0.6134	0.7766	1.2876	0.7898	10
29 0	0.4848	0.5543	1.8040	0.8746	0 **61**	**38** 0	0.6157	0.7813	1.2799	0.7880	0 **52**
10	0.4874	0.5581	1.7917	0.8732	50	10	0.6180	0.7860	1.2723	0.7862	50
20	0.4899	0.5619	1.7796	0.8718	40	20	0.6202	0.7907	1.2647	0.7844	40
30	0.4924	0.5658	1.7675	0.8704	30	30	0.6225	0.7954	1.2572	0.7826	30
40	0.4950	0.5696	1.7556	0.8689	20	40	0.6248	0.8002	1.2497	0.7808	20
50	0.4975	0.5735	1.7437	0.8675	10	50	0.6271	0.8050	1.2423	0.7790	10
30 0	0.5000	0.5774	1.7321	0.8660	0 **60**	**39** 0	0.6293	0.8098	1.2349	0.7771	0 **51**
10	0.5025	0.5812	1.7205	0.8646	50	10	0.6316	0.8146	1.2276	0.7753	50
20	0.5050	0.5851	1.7090	0.8631	40	20	0.6338	0.8195	1.2203	0.7735	40
30	0.5075	0.5890	1.6977	0.8616	30	30	0.6361	0.8243	1.2131	0.7716	30
40	0.5100	0.5930	1.6864	0.8601	20	40	0.6383	0.8292	1.2059	0.7698	20
50	0.5125	0.5969	1.6753	0.8587	10	50	0.6406	0.8342	1.1988	0.7679	10
31 0	0.5150	0.6000	1.6643	0.8572	0 **59**	**40** 0	0.6428	0.8391	1.1918	0.7660	0 **50**
10	0.5175	0.6048	1.6534	0.8557	50	10	0.6450	0.8441	1.1847	0.7642	50
20	0.5200	0.6088	1.6426	0.8542	40	20	0.6472	0.8491	1.1778	0.7623	40
30	0.5225	0.6128	1.6319	0.8526	30	30	0.6494	0.8541	1.1708	0.7604	30
40	0.5250	0.6168	1.6212	0.8511	20	40	0.6517	0.8591	1.1640	0.7585	20
50	0.5275	0.6208	1.6107	0.8496	10	50	0.6539	0.8642	1.1571	0.7566	10
32 0	0.5299	0.6249	1.6003	0.8480	0 **58**	**41** 0	0.6561	0.8693	1.1504	0.7547	0 **49**
10	0.5324	0.6289	1.5900	0.8465	50	10	0.6583	0.8744	1.1436	0.7528	50
20	0.5348	0.6330	1.5798	0.8450	40	20	0.6604	0.8796	1.1369	0.7509	40
30	0.5373	0.6371	1.5697	0.8434	30	30	0.6626	0.8847	1.1303	0.7490	30
40	0.5398	0.6412	1.5597	0.8418	20	40	0.6648	0.8899	1.1237	0.7470	20
50	0.5422	0.6453	1.5497	0.8403	10	50	0.6670	0.8952	1.1171	0.7451	10
33 0	0.5446	0.6494	1.5399	0.8387	0 **57**	**42** 0	0.6691	0.9004	1.1106	0.7431	0 **48**
10	0.5471	0.6536	1.5301	0.8371	50	10	0.6713	0.9057	1.1041	0.7412	50
20	0.5495	0.6577	1.5204	0.8355	40	20	0.6734	0.9110	1.0977	0.7392	40
30	0.5519	0.6619	1.5108	0.8339	30	30	0.6756	0.9163	1.0913	0.7373	30
40	0.5544	0.6661	1.5013	0.8323	20	40	0.6777	0.9217	1.0850	0.7353	20
50	0.5568	0.6703	1.4919	0.8307	10	50	0.6799	0.9271	1.0786	0.7333	10
34 0	0.5592	0.6745	1.4826	0.8290	0 **56**	**43** 0	0.6820	0.9325	1.0724	0.7314	0 **47**
10	0.5616	0.6787	1.4733	0.8274	50	10	0.6841	0.9380	1.0661	0.7294	50
20	0.5640	0.6830	1.4641	0.8258	40	20	0.6862	0.9435	1.0599	0.7274	40
30	0.5664	0.6873	1.4550	0.8241	30	30	0.6884	0.9490	1.0538	0.7254	30
40	0.5688	0.6916	1.4460	0.8225	20	40	0.6905	0.9545	1.0477	0.7234	20
50	0.5712	0.6959	1.4370	0.8208	10	50	0.6926	0.9601	1.0416	0.7214	10
35 0	0.5736	0.7002	1.4281	0.8192	0 **55**	**44** 0	0.6947	0.9657	1.0355	0.7193	0 **46**
10	0.5760	0.7046	1.4193	0.8175	50	10	0.6967	0.9713	1.0295	0.7173	50
20	0.5783	0.7089	1.4106	0.8158	40	20	0.6988	0.9770	1.0235	0.7153	40
30	0.5807	0.7133	1.4019	0.8141	30	30	0.7009	0.9827	1.0176	0.7133	30
40	0.5831	0.7177	1.3934	0.8124	20	40	0.7030	0.9884	1.0117	0.7112	20
50	0.5854	0.7221	1.3848	0.8107	10	50	0.7050	0.9942	1.0058	0.7092	10
36 0	0.5878	0.7265	1.3764	0.8090	0 **54**	**45** 0	0.7071	1.0000	1.0000	0.7071	0 **45**
° ′	cos	cot	tan	sin	′ °	° ′	cos	cot	tan	sin	′ °

TABLE VI.—CIRCUMFERENCES AND AREAS OF CIRCLES.

If $N=$ the radius of the circle, the circumference $= 2\pi N$.
If $N=$ the radius of the circle, the area $= \pi N^2$.
If $N=$ the circumference of the circle, the radius $= \frac{1}{2\pi} N$.
If $N=$ the circumference of the circle, the area $= \frac{1}{4\pi} N^2$.

N	$2\pi N$	πN^2	$\frac{1}{2\pi} N$	$\frac{1}{4\pi} N^2$	N	$2\pi N$	πN^2	$\frac{1}{2\pi} N$	$\frac{1}{4\pi} N^2$
0	0.00	0.0	0.000	0.00	50	314.16	7 854	7.96	198.94
1	6.28	3.1	0.159	0.08	51	320.44	8 171	8.12	206.98
2	12.57	12.6	0.318	0.32	52	326.73	8 495	8.28	215.18
3	18.85	28.3	0.477	0.72	53	333.01	8 825	8.44	223.53
4	25.13	50.3	0.637	1.27	54	339.29	9 161	8.59	232.05
5	31.42	78.5	0.796	1.99	55	345.58	9 503	8.75	240.72
6	37.70	113.1	0.955	2.86	56	351.86	9 852	8.91	249.55
7	43.98	153.9	1.114	3.90	57	358.14	10 207	9.07	258.55
8	50.27	201.1	1.273	5.09	58	364.42	10 568	9.23	267.70
9	56.55	254.5	1.432	6.45	59	370.71	10 936	9.39	277.01
10	62.83	314.2	1.592	7.96	60	376.99	11 310	9.55	286.48
11	69.12	380.1	1.751	9.63	61	383.27	11 690	9.71	296.11
12	75.40	452.4	1.910	11.46	62	389.56	12 076	9.87	305.90
13	81.68	530.9	2.069	13.45	63	395.84	12 469	10.03	315.84
14	87.96	615.8	2.228	15.60	64	402.12	12 868	10.19	325.95
15	94.25	706.9	2.387	17.90	65	408.41	13 273	10.35	336.21
16	100.53	804.2	2.546	20.37	66	414.69	13 685	10.50	346.64
17	106.81	907.9	2.706	23.00	67	420.97	14 103	10.66	357.22
18	113.10	1 017.9	2.865	25.78	68	427.26	14 527	10.82	367.97
19	119.38	1 134.1	3.024	28.73	69	433.54	14 957	10.98	378.87
20	125.66	1 256.6	3.183	31.83	70	439.82	15 394	11.14	389.93
21	131.95	1 385.4	3.342	35.09	71	446.11	15 837	11.30	401.15
22	138.23	1 520.5	3.501	38.52	72	452.39	16 286	11.46	412.53
23	144.51	1 661.9	3.661	42.10	73	458.67	16 742	11.62	424.07
24	150.80	1 809.6	3.820	45.84	74	464.96	17 203	11.78	435.77
25	157.08	1 963.5	3.979	49.74	75	471.24	17 671	11.94	447.62
26	163.36	2 123.7	4.138	53.79	76	477.52	18 116	12.10	459.64
27	169.65	2 290.2	4.297	58.01	77	483.81	18 627	12.25	471.81
28	175.93	2 463.0	4.456	62.39	78	490.09	19 113	12.41	484.15
29	182.21	2 642.1	4.615	66.92	79	496.37	19 607	12.57	496.64
30	188.50	2 827.4	4.775	71.62	80	502.65	20 106	12.73	509.30
31	194.78	3 019.1	4.934	76.47	81	508.94	20 612	12.89	522.11
32	201.06	3 217.0	5.093	81.49	82	515.22	21 124	13.05	535.08
33	207.35	3 421.2	5.252	86.66	83	521.50	21 642	13.21	548.21
34	213.63	3 631.7	5.411	91.99	84	527.79	22 167	13.37	561.50
35	219.91	3 848.5	5.570	97.48	85	534.07	22 698	13.53	574.95
36	226.19	4 071.5	5.730	103.13	86	540.35	23 235	13.69	588.55
37	232.48	4 300.8	5.889	108.94	87	546.64	23 779	13.85	602.32
38	238.76	4 536.5	6.048	114.91	88	552.92	24 328	14.01	616.25
39	245.04	4 778.4	6.207	121.04	89	559.20	24 885	14.16	630.33
40	251.33	5 026.5	6.366	127.32	90	565.49	25 447	14.32	644.58
41	257.61	5 281.0	6.525	133.77	91	571.77	26 016	14.48	658.98
42	263.89	5 541.8	6.685	140.37	92	578.05	26 590	14.64	673.54
43	270.18	5 808.8	6.844	147.14	93	584.34	27 172	14.80	688.27
44	276.46	6 082.1	7.003	154.06	94	590.62	27 759	14.96	703.15
45	282.74	6 361.7	7.162	161.14	95	596.90	28 353	15.12	718.19
46	289.03	6 647.6	7.321	168.39	96	603.19	28 953	15.28	733.39
47	295.31	6 939.8	7.480	175.79	97	609.47	29 559	15.44	748.74
48	301.59	7 238.2	7.639	183.35	98	615.75	30 172	15.60	764.26
49	307.88	7 543.0	7.799	191.07	99	622.04	30 791	15.76	779.94
50	314.16	7 854.0	7.958	198.94	100	628.32	31 416	15.92	795.77
N	$2\pi N$	πN^2	$\frac{1}{2\pi} N$	$\frac{1}{4\pi} N^2$	N	$2\pi N$	πN^2	$\frac{1}{2\pi} N$	$\frac{1}{4\pi} N^2$

MARINER'S COMPASS.



A TABLE OF THE ANGLES

Which every Point and Quarter Point of the Compass makes with the Meridian.

North.		Points.	° ′ ″	Points.	South.	
N. by E.	N. by W.	0-¼ 0-½ 0-¾ 1	2 48 45 5 37 30 8 26 15 11 15 0	0-¼ 0-½ 0-¾ 1	S. by E.	S. by W.
N.N.E.	N.N.W.	1-¼ 1-½ 1-¾ 2	14 8 45 16 52 30 19 41 15 22 30 0	1-¼ 1-½ 1-¾ 2	S.S.E.	S.S.W.
N.E. by N.	N.W. by N.	2-¼ 2-½ 2-¾ 3	25 18 45 28 7 30 30 56 15 33 45 0	2-¼ 2-½ 2-¾ 3	S.E. by S.	S.W. by S.
N.E.	N.W.	3-¼ 3-½ 3-¾ 4	36 33 45 39 22 30 42 11 15 45 0 0	3-¼ 3-½ 3-¾ 4	S.E.	S.W.
N.E. by E.	N.W. by W.	4-¼ 4-½ 4-¾ 5	47 48 45 50 37 30 53 26 15 56 15 0	4-¼ 4-½ 4-¾ 5	S.E. by E.	S.W. by W.
E.N.E.	W.N.W.	5-¼ 5-½ 5-¾ 6	59 3 45 61 52 30 64 41 15 67 30 0	5-¼ 5-½ 5-¾ 6	E.S.E.	W.S.W.
E. by N.	W. by N.	6-¼ 6-½ 6-¾ 7	70 18 45 73 7 30 75 56 15 78 45 0	6-¼ 6-½ 6-¾ 7	E. by S.	W. by S.
East.	West.	7-¼ 7-½ 7-¾ 8	81 33 45 84 22 30 87 11 15 90 0 0	7-¼ 7-½ 7-¾ 8	East.	West.

TABLE VII.—TRAVERSE TABLE.

Bearing.	Distance 1.		Distance 2.		Distance 3.		Distance 4.		Distance 5.		Bearing.
° ′	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	° ′
0 15	1.000	0.004	2.000	0.009	3.000	0.013	4.000	0.017	5.000	0.022	89 45
30	1.000	0.009	2.000	0.017	3.000	0.026	4.000	0.035	5.000	0.044	30
45	1.000	0.013	2.000	0.026	3.000	0.039	4.000	0.052	5.000	0.065	15
1 0	1.000	0.017	2.000	0.035	3.000	0.052	3.999	0.070	4.999	0.087	89 0
15	1.000	0.022	2.000	0.044	2.999	0.065	3.999	0.087	4.999	0.109	45
30	1.000	0.026	1.999	0.052	2.999	0.079	3.999	0.105	4.998	0.131	30
45	1.000	0.031	1.999	0.061	2.999	0.092	3.998	0.122	4.998	0.153	15
2 0	0.999	0.035	1.999	0.070	2.998	0.105	3.998	0.140	4.997	0.174	88 0
15	0.999	0.039	1.998	0.079	2.998	0.118	3.997	0.157	4.996	0.196	45
30	0.999	0.044	1.998	0.087	2.997	0.131	3.996	0.174	4.995	0.218	30
45	0.999	0.048	1.998	0.096	2.997	0.144	3.995	0.192	4.994	0.240	15
3 0	0.999	0.052	1.997	0.105	2.996	0.157	3.995	0.209	4.993	0.262	87 0
15	0.998	0.057	1.997	0.113	2.995	0.170	3.994	0.227	4.992	0.283	45
30	0.998	0.061	1.996	0.122	2.994	0.183	3.993	0.244	4.991	0.305	30
45	0.998	0.065	1.996	0.131	2.994	0.196	3.991	0.262	4.989	0.327	15
4 0	0.998	0.070	1.995	0.140	2.993	0.209	3.990	0.279	4.988	0.349	86 0
15	0.997	0.074	1.995	0.148	2.992	0.222	3.989	0.296	4.986	0.371	45
30	0.997	0.078	1.994	0.157	2.991	0.235	3.988	0.314	4.985	0.392	30
45	0.997	0.083	1.993	0.166	2.990	0.248	3.986	0.331	4.983	0.414	15
5 0	0.996	0.087	1.992	0.174	2.989	0.261	3.985	0.349	4.981	0.436	85 0
15	0.996	0.092	1.992	0.183	2.987	0.275	3.983	0.366	4.979	0.458	45
30	0.995	0.096	1.991	0.192	2.986	0.288	3.982	0.383	4.977	0.479	30
45	0.995	0.100	1.990	0.200	2.985	0.301	3.980	0.401	4.975	0.501	15
6 0	0.995	0.105	1.989	0.209	2.984	0.314	3.978	0.418	4.973	0.523	84 0
15	0.994	0.109	1.988	0.218	2.982	0.327	3.976	0.435	4.970	0.544	45
30	0.994	0.113	1.987	0.226	2.981	0.340	3.974	0.453	4.968	0 566	30
45	0.993	0.118	1.986	0.235	2.979	0.353	3.972	0.470	4.965	0.588	15
7 0	0.993	0.122	1.985	0.244	2.978	0.366	3.970	0.487	4.963	0.609	83 0
15	0.992	0.126	1.984	0.252	2.976	0.379	3.968	0.505	4.960	0.631	45
30	0.991	0.131	1.983	0.261	2.974	0.392	3.966	0.522	4.957	0.653	30
45	0.991	0.135	1.982	0.270	2.973	0.405	3.963	0.539	4.954	0.674	15
8 0	0.990	0.139	1.981	0.278	2.971	0.418	3.961	0.557	4.951	0.696	82 0
15	0.990	0.143	1.979	0.287	2.969	0.430	3.959	0.574	4.948	0.717	45
30	0.989	0.148	1.978	0.296	2.967	0.443	3.956	0.591	4.945	0.739	30
45	0.988	0.152	1.977	0.304	2.965	0.456	3.953	0.608	4.942	0.761	15
9 0	0.988	0.156	1.975	0.313	2.963	0.469	3.951	0.626	4.938	0.782	81 0
15	0.987	0.161	1.974	0.321	2.961	0.482	3.948	0.643	4.935	0.804	45
30	0.986	0.165	1.973	0.330	2.959	0.495	3.945	0.660	4.931	0.825	30
45	0.986	0.169	1.971	0.339	2.957	0.508	3.942	0.677	4.928	0.847	15
10 0	0.985	0.174	1.970	0.347	2.954	0.521	3.939	0.695	4.924	0.868	80 0
15	0.984	0.178	1.968	0.356	2.952	0.534	3.936	0.712	4.920	0.890	45
30	0.983	0.182	1.967	0.364	2.950	0.547	3.933	0.729	4.916	0.911	30
45	0.982	0.187	1.965	0.373	2.947	0.560	3.930	0.746	4.912	0.933	15
11 0	0.982	0.191	1.963	0.382	2.945	0.572	3.927	0.763	4.908	0.954	79 0
15	0.981	0.195	1.962	0.390	2.942	0.585	3.923	0.780	4.904	0.975	45
30	0.980	0.199	1.960	0.399	2.940	0.598	3.920	0.797	4.900	0.997	30
45	0.979	0.204	1.958	0.407	2.937	0.611	3.916	0.815	4.895	1.018	15
12 0	0.978	0.208	1.956	0.416	2.934	0.624	3.913	0.832	4.891	1.040	78 0
15	0.977	0.212	1.954	0.424	2.932	0.637	3.909	0.849	4.886	1.061	45
30	0.976	0.216	1.953	0.433	2.929	0.649	3.905	0.866	4.881	1.082	30
45	0.975	0.221	1.951	0.441	2.926	0.662	3.901	0.883	4.877	1.103	15
13 0	0.974	0.225	1.949	0.450	2.923	0.675	3.897	0.900	4.872	1.125	77 0
15	0.973	0.229	1.947	0.458	2.920	0.688	3.894	0.917	4.867	1.146	45
30	0.972	0.233	1.945	0.467	2.917	0.700	3.889	0.934	4.862	1.167	30
45	0.971	0.238	1.943	0.475	2.914	0.713	3.885	0.951	4.857	1.188	15
14 0	0.970	0.242	1.941	0.484	2.911	0.726	3.881	0.968	4.851	1.210	76 0
15	0.969	0.246	1.938	0.492	2.908	0.738	3.877	0.985	4.846	1.231	45
30	0.968	0.250	1.936	0.501	2.904	0.751	3.873	1.002	4.841	1.252	30
45	0.967	0.255	1.934	0.509	2.901	0.764	3.868	1.018	4.835	1.273	15
15 0	0.966	0.259	1.932	0.518	2.898	0.776	3.864	1.035	4.830	1.294	75 0
° ′	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	° ′
Bearing.	Distance 1.		Distance 2.		Distance 3.		Distance 4.		Distance 5.		Bearing.

75°—90°

Bearing.	Distance 6.		Distance 7.		Distance 8.		Distance 9.		Distance 10.		Bearing.
° ′	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	° ′
0 15	6.000	0.026	7.000	0.031	8.000	0.035	9.000	0.039	10.000	0.044	89 45
30	6.000	0.052	7.000	0.061	8.000	0.070	9.000	0.079	10.000	0.087	30
45	5.999	0.079	6.999	0.092	7.999	0.105	8.999	0.118	9.999	0.131	15
1 0	5.999	0.105	6.999	0.122	7.999	0.140	8.999	0.157	9.999	0.175	89 0
15	5.999	0.131	6.998	0.153	7.998	0.175	8.998	0.196	9.998	0.218	45
30	5.998	0.157	6.998	0.183	7.997	0.209	8.997	0.236	9.997	0.262	30
45	5.997	0.183	6.997	0.214	7.996	0.244	8.996	0.275	9.995	0.305	15
2 0	5.996	0.209	6.996	0.244	7.995	0.279	8.995	0.314	9.994	0.349	88 0
15	5.995	0.236	6.995	0.275	7.994	0.314	8.993	0.353	9.992	0.393	45
30	5.994	0.262	6.993	0.305	7.992	0.349	8.991	0.393	9.991	0.436	30
45	5.993	0.288	6.992	0.336	7.991	0.384	8.990	0.432	9.989	0.480	15
3 0	5.992	0.314	6.990	0.366	7.989	0.419	8.988	0.471	9.986	0.523	87 0
15	5.990	0.340	6.989	0.397	7.987	0.454	8.986	0.510	9.984	0.567	45
30	5.989	0.366	6.987	0.427	7.985	0.488	8.983	0.549	9.981	0.611	30
45	5.987	0.392	6.985	0.458	7.983	0.523	8.981	0.589	9.979	0.654	15
4 0	5.985	0.419	6.983	0.488	7.981	0.558	8.978	0.628	9.976	0.698	86 0
15	5.984	0.445	6.981	0.519	7.978	0.593	8.975	0.667	9.973	0.741	45
30	5.982	0.471	6.978	0.549	7.975	0.628	8.972	0.706	9.969	0.785	30
45	5.979	0.497	6.976	0.580	7.973	0.662	8.969	0.745	9.966	0.828	15
5 0	5.977	0.523	6.973	0.610	7.970	0.697	8.966	0.784	9.962	0.872	85 0
15	5.975	0.549	6.971	0.641	7.966	0.732	8.962	0.824	9.958	0.915	45
30	5.972	0.575	6.968	0.671	7.963	0.767	8.959	0.863	9.954	0.959	30
45	5.970	0.601	6.965	0.701	7.960	0.802	8.955	0.902	9.950	1.002	15
6 0	5.967	0.627	6.962	0.732	7.956	0.836	8.951	0.941	9.945	1.045	84 0
15	5.964	0.653	6.958	0.762	7.952	0.871	8.947	0.980	9.941	1.089	45
30	5.961	0.679	6.955	0.792	7.949	0.906	8.942	1.019	9.936	1.132	30
45	5.958	0.705	6.951	0.823	7.945	0.940	8.938	1.058	9.931	1.175	15
7 0	5.955	0.731	6.948	0.853	7.940	0.975	8.933	1.097	9.926	1.219	83 0
15	5.952	0.757	6.944	0.883	7.936	1.010	8.928	1.136	9.920	1.262	45
30	5.949	0.783	6.940	0.914	7.932	1.044	8.923	1.175	9.914	1.305	30
45	5.945	0.809	6.936	0.944	7.927	1.079	8.918	1.214	9.909	1.349	15
8 0	5.942	0.835	6.932	0.974	7.922	1.113	8.912	1.253	9.903	1.392	82 0
15	5.938	0.861	6.928	1.004	7.917	1.148	8.907	1.291	9.897	1.435	45
30	5.934	0.887	6.923	1.035	7.912	1.182	8.901	1.330	9.890	1.478	30
45	5.930	0.913	6.919	1.065	7.907	1.217	8.895	1.369	9.884	1.521	15
9 0	5.926	0.939	6.914	1.095	7.902	1.251	8.889	1.408	9.877	1.564	81 0
15	5.922	0.964	6.909	1.125	7.896	1.286	8.883	1.447	9.870	1.607	45
30	5.918	0.990	6.904	1.155	7.890	1.320	8.877	1.485	9.863	1.651	30
45	5.913	1.016	6.899	1.185	7.884	1.355	8.870	1.524	9.856	1.694	15
10 0	5.909	1.042	6.894	1.216	7.878	1.389	8.863	1.563	9.848	1.737	80 0
15	5.904	1.068	6.888	1.246	7.872	1.424	8.856	1.601	9.840	1.779	45
30	5.900	1.093	6.883	1.276	7.866	1.458	8.849	1.640	9.833	1.822	30
45	5.895	1.119	6.877	1.306	7.860	1.492	8.842	1.679	9.825	1.865	15
11 0	5.890	1.145	6.871	1.336	7.853	1.526	8.835	1.717	9.816	1.908	79 0
15	5.885	1.171	6.866	1.366	7.846	1.561	8.827	1.756	9.808	1.951	45
30	5.880	1.196	6.859	1.396	7.839	1.595	8.819	1.794	9.799	1.994	30
45	5.874	1.222	6.853	1.425	7.832	1.629	8.811	1.833	9.791	2.036	15
12 0	5.869	1.247	6.847	1.455	7.825	1.663	8.803	1.871	9.782	2.079	78 0
15	5.863	1.273	6.841	1.485	7.818	1.697	8.795	1.910	9.772	2.122	45
30	5.858	1.299	6.834	1.515	7.810	1.732	8.787	1.948	9.763	2.164	30
45	5.852	1.324	6.827	1.545	7.803	1.766	8.778	1.986	9.753	2.207	15
13 0	5.846	1.350	6.821	1.575	7.795	1.800	8.769	2.025	9.744	2.250	77 0
15	5.840	1.375	6.814	1.604	7.787	1.834	8.760	2.063	9.734	2.292	45
30	5.834	1.401	6.807	1.634	7.779	1.868	8.751	2.101	9.724	2.335	30
45	5.828	1.426	6.799	1.664	7.771	1.902	8.742	2.139	9.713	2.377	15
14 0	5.822	1.452	6.792	1.693	7.762	1.935	8.733	2.177	9.703	2.419	76 0
15	5.815	1.477	6.785	1.723	7.754	1.969	8.723	2.215	9.692	2.462	45
30	5.809	1.502	6.777	1.753	7.745	2.003	8.713	2.253	9.682	2.504	30
45	5.802	1.528	6.769	1.782	7.736	2.037	8.703	2.291	9.671	2.546	15
15 0	5.796	1.553	6.761	1.812	7.727	2.071	8.693	2.329	9.659	2.588	75 0
° ′	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	° ′
Bearing.	Distance 6.		Distance 7.		Distance 8.		Distance 9.		Distance 10.		Bearing.

15°— 30°

Bearing.	Distance 1.		Distance 2.		Distance 3.		Distance 4.		Distance 5.		Bearing.
° ′	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	° ′
15 15	0.965	0.263	1.930	0.526	2.894	0.789	3.859	1.052	4.824	1.315	74 45
30	0.964	0.267	1.927	0.534	2.891	0.802	3.855	1.069	4.818	1.336	30
45	0.962	0.271	1.925	0.543	2.887	0.814	3.850	1.086	4.812	1.357	15
16 0	0.961	0.276	1.923	0.551	2.884	0.827	3.845	1.103	4.806	1.378	74 0
15	0.960	0.280	1.920	0.560	2.880	0.839	3.840	1.119	4.800	1.399	45
30	0.959	0.284	1.918	0.568	2.876	0.852	3.835	1.136	4.794	1.420	30
45	0.958	0.288	1.915	0.576	2.873	0.865	3.830	1.153	4.788	1.441	15
17 0	0.956	0.292	1.913	0.585	2.869	0.877	3.825	1.169	4.782	1.462	73 0
15	0.955	0.297	1.910	0.593	2.865	0.890	3.820	1.186	4.775	1.483	45
30	0.954	0.301	1.907	0.601	2.861	0.902	3.815	1.203	4.769	1.504	30
45	0.952	0.305	1.905	0.610	2.857	0.915	3.810	1.220	4.762	1.524	15
18 0	0.951	0.309	1.902	0.618	2.853	0.927	3.804	1.236	4.755	1.545	72 0
15	0.950	0.313	1.899	0.626	2.849	0.939	3.799	1.253	4.748	1.566	45
30	0.948	0.317	1.897	0.635	2.845	0.952	3.793	1.269	4.742	1.587	30
45	0.947	0.321	1.894	0.643	2.841	0.964	3.788	1.286	4.735	1.607	15
19 0	0.946	0.326	1.891	0.651	2.837	0.977	3.782	1.302	4.728	1.628	71 0
15	0.944	0.330	1.888	0.659	2.832	0.989	3.776	1.319	4.720	1.648	45
30	0.943	0.334	1.885	0.668	2.828	1.001	3.771	1.335	4.713	1.669	30
45	0.941	0.338	1.882	0.676	2.824	1.014	3.765	1.352	4.706	1.690	15
20 0	0.940	0.342	1.879	0.684	2.819	1.026	3.759	1.368	4.698	1.710	70 0
15	0.938	0.346	1.876	0.692	2.815	1.038	3.753	1.384	4.691	1.731	45
30	0.937	0.350	1.873	0.700	2.810	1.051	3.747	1.401	4.683	1.751	30
45	0.935	0.354	1.870	0.709	2.805	1.063	3.741	1.417	4.676	1.771	15
21 0	0.934	0.358	1.867	0.717	2.801	1.075	3.734	1.433	4.668	1.792	69 0
15	0.932	0.362	1.864	0.725	2.796	1.087	3.728	1.450	4.660	1.812	45
30	0.930	0.367	1.861	0.733	2.791	1.100	3.722	1.466	4.652	1.833	30
45	0.929	0.371	1.858	0.741	2.786	1.112	3.715	1.482	4.644	1.853	15
22 0	0.927	0.375	1.854	0.749	2.782	1.124	3.709	1.498	4.636	1.873	68 0
15	0.926	0.379	1.851	0.757	2.777	1.136	3.702	1.515	4.628	1.893	45
30	0.924	0.383	1.848	0.765	2.772	1.148	3.696	1.531	4.619	1.913	30
45	0.922	0.387	1.844	0.773	2.767	1.160	3.689	1.547	4.611	1.934	15
23 0	0.921	0.391	1.841	0.781	2.762	1.172	3.682	1.563	4.603	1.954	67 0
15	0.919	0.395	1.838	0.789	2.756	1.184	3.675	1.579	4.594	1.974	45
30	0.917	0.399	1.834	0.797	2.751	1.196	3.668	1.595	4.585	1.994	30
45	0.915	0.403	1.831	0.805	2.746	1.208	3.661	1.611	4.577	2.014	15
24 0	0.914	0.407	1.827	0.813	2.741	1.220	3.654	1.627	4.568	2.034	66 0
15	0.912	0.411	1.824	0.821	2.735	1.232	3.647	1.643	4.559	2.054	45
30	0.910	0.415	1.820	0.829	2.730	1.244	3.640	1.659	4.550	2.073	30
45	0.908	0.419	1.816	0.837	2.724	1.256	3.633	1.675	4.541	2.093	15
25 0	0.906	0.423	1.813	0.845	2.719	1.268	3.625	1.690	4.532	2.113	65 0
15	0.904	0.427	1.809	0.853	2.713	1.280	3.618	1.706	4.522	2.133	45
30	0.903	0.431	1.805	0.861	2.708	1.292	3.610	1.722	4.513	2.153	30
45	0.901	0.434	1.801	0.869	2.702	1.303	3.603	1.738	4.503	2.172	15
26 0	0.899	0.438	1.798	0.877	2.696	1.315	3.595	1.753	4.494	2.192	64 0
15	0.897	0.442	1.794	0.885	2.691	1.327	3.587	1.769	4.484	2.211	45
30	0.895	0.446	1.790	0.892	2.685	1.339	3.580	1.785	4.475	2.231	30
45	0.893	0.450	1.786	0.900	2.679	1.350	3.572	1.800	4.465	2.250	15
27 0	0.891	0.454	1.782	0.908	2.673	1.362	3.564	1.816	4.455	2.270	63 0
15	0.889	0.458	1.778	0.916	2.667	1.374	3.556	1.831	4.445	2.289	45
30	0.887	0.462	1.774	0.923	2.661	1.385	3.548	1.847	4.435	2.309	30
45	0.885	0.466	1.770	0.931	2.655	1.397	3.540	1.862	4.425	2.328	15
28 0	0.883	0.469	1.766	0.939	2.649	1.408	3.532	1.878	4.415	2.347	62 0
15	0.881	0.473	1.762	0.947	2.643	1.420	3.524	1.893	4.404	2.367	45
30	0.879	0.477	1.758	0.954	2.636	1.431	3.515	1.909	4.394	2.386	30
45	0.877	0.481	1.753	0.962	2.630	1.443	3.507	1.924	4.384	2.405	15
29 0	0.875	0.485	1.749	0.970	2.624	1.454	3.498	1.939	4.373	2.424	61 0
15	0.872	0.489	1.745	0.977	2.617	1.466	3.490	1.954	4.362	2.443	45
30	0.870	0.492	1.741	0.985	2.611	1.477	3.481	1.970	4.352	2.462	30
45	0.868	0.496	1.736	0.992	2.605	1.489	3.473	1.985	4.341	2.481	15
30 0	0.866	0.500	1.732	1.000	2.598	1.500	3.464	2.000	4.330	2.500	60 0
° ′	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	° ′
Bearing.	Distance 1.		Distance 2.		Distance 3.		Distance 4.		Distance 5.		Bearing.

60°—75°

Bearing.	Distance 6.		Distance 7.		Distance 8.		Distance 9.		Distance 10.		Bearing.
° ′	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	° ′
15 15	5.789	1.578	6.754	1.841	7.718	2.104	8.683	2.367	9.648	2.630	74 45
30	5.782	1.603	6.745	1.871	7.709	2.138	8.673	2.405	9.636	2.672	30
45	5.775	1.629	6.737	1.900	7.700	2.172	8.662	2.443	9.625	2.714	15
16 0	5.768	1.654	6.729	1.929	7.690	2.205	8.651	2.481	9.613	2.756	74 0
15	5.760	1.679	6.720	1.959	7.680	2.239	8.640	2.518	9.601	2.798	45
30	5.753	1.704	6.712	1.988	7.671	2.272	8.629	2.556	9.588	2.840	30
45	5.745	1.729	6.703	2.017	7.661	2.306	8.618	2.594	9.576	2.882	15
17 0	5.738	1.754	6.694	2.047	7.650	2.339	8.607	2.631	9.563	2.924	73 0
15	5.730	1.779	6.685	2.076	7.640	2.372	8.595	2.669	9.550	2.965	45
30	5.722	1.804	6.676	2.105	7.630	2.406	8.583	2.706	9.537	3.007	30
45	5.714	1.829	6.667	2.134	7.619	2.439	8.572	2.744	9.524	3.049	15
18 0	5.706	1.854	6.657	2.163	7.608	2.472	8.560	2.781	9.511	3.090	72 0
15	5.698	1.879	6.648	2.192	7.598	2.505	8.547	2.818	9.497	3.132	45
30	5.690	1.904	6.638	2.221	7.587	2.538	8.535	2.856	9.483	3.173	30
45	5.682	1.929	6.629	2.250	7.575	2.572	8.522	2.893	9.469	3.214	15
19 0	5.673	1.953	6.619	2.279	7.564	2.605	8.510	2.930	9.455	3.256	71 0
15	5.665	1.978	6.609	2.308	7.553	2.638	8.497	2.967	9.441	3.297	45
30	5.656	2.003	6.598	2.337	7.541	2.670	8.484	3.004	9.426	3.338	30
45	5.647	2.028	6.588	2.365	7.529	2.703	8.471	3.041	9.412	3.379	15
20 0	5.638	2.052	6.578	2.394	7.518	2.736	8.457	3.078	9.397	3.420	70 0
15	5.629	2.077	6.567	2.423	7.506	2.769	8.444	3.115	9.382	3.461	45
30	5.620	2.101	6.557	2.451	7.493	2.802	8.430	3.152	9.367	3.502	30
45	5.611	2.126	6.546	2.480	7.481	2.834	8.416	3.189	9.351	3.543	15
21 0	5.601	2.150	6.535	2.509	7.469	2.867	8.402	3.225	9.336	3.584	69 0
15	5.592	2.175	6.524	2.537	7.456	2.900	8.388	3.262	9.320	3.624	45
30	5.582	2.199	6.513	2.566	7.443	2.932	8.374	3.299	9.304	3.665	30
45	5.573	2.223	6.502	2.594	7.430	2.964	8.359	3.335	9.288	3.706	15
22 0	5.563	2.248	6.490	2.622	7.417	2.997	8.345	3.371	9.272	3.746	68 0
15	5.553	2.272	6.479	2.651	7.404	3.029	8.330	3.408	9.255	3.787	45
30	5.543	2.296	6.467	2.679	7.391	3.061	8.315	3.444	9.239	3.827	30
45	5.533	2.320	6.455	2.707	7.378	3.094	8.300	3.480	9.222	3.867	15
23 0	5.523	2.344	6.444	2.735	7.364	3.126	8.285	3.517	9.205	3.907	67 0
15	5.513	2.368	6.432	2.763	7.350	3.158	8.269	3.553	9.188	3.947	45
30	5.502	2.392	6.419	2.791	7.336	3.190	8.254	3.589	9.171	3.988	30
45	5.492	2.416	6.407	2.819	7.322	3.222	8.238	3.625	9.153	4.028	15
24 0	5.481	2.440	6.395	2.847	7.308	3.254	8.222	3.661	9.136	4.067	66 0
15	5.471	2.464	6.382	2.875	7.294	3.286	8.206	3.696	9.118	4.107	45
30	5.460	2.488	6.370	2.903	7.280	3.318	8.190	3.732	9.100	4.147	30
45	5.449	2.512	6.357	2.931	7.265	3.349	8.173	3.768	9.081	4.187	15
25 0	5.438	2.536	6.344	2.958	7.250	3.381	8.157	3.804	9.063	4.226	65 0
15	5.427	2.559	6.331	2.986	7.236	3.413	8.140	3.839	9.045	4.266	45
30	5.416	2.583	6.318	3.014	7.221	3.444	8.123	3.875	9.026	4.305	30
45	5.404	2.607	6.305	3.041	7.206	3.476	8.106	3.910	9.007	4.345	15
26 0	5.393	2.630	6.292	3.069	7.190	3.507	8.089	3.945	8.988	4.384	64 0
15	5.381	2.654	6.278	3.096	7.175	3.538	8.072	3.981	8.969	4.423	45
30	5.370	2.677	6.265	3.123	7.160	3.570	8.054	4.016	8.949	4.462	30
45	5.358	2.701	6.251	3.151	7.144	3.601	8.037	4.051	8.930	4.501	15
27 0	5.346	2.724	6.237	3.178	7.128	3.632	8.019	4.086	8.910	4.540	63 0
15	5.334	2.747	6.223	3.205	7.112	3.663	8.001	4.121	8.890	4.579	45
30	5.322	2.770	6.209	3.232	7.096	3.694	7.983	4.156	8.870	4.618	30
45	5.310	2.794	6.195	3.259	7.080	3.725	7.965	4.190	8.850	4.656	15
28 0	5.298	2.817	6.181	3.286	7.064	3.756	7.947	4.225	8.829	4.695	62 0
15	5.285	2.840	6.166	3.313	7.047	3.787	7.928	4.260	8.809	4.733	45
30	5.273	2.863	6.152	3.340	7.031	3.817	7.909	4.294	8.788	4.772	30
45	5.260	2.886	6.137	3.367	7.014	3.848	7.891	4.329	8.767	4.810	15
29 0	5.248	2.909	6.122	3.394	6.997	3.878	7.872	4.363	8.746	4.848	61 0
15	5.235	2.932	6.107	3.420	6.980	3.909	7.852	4.398	8.725	4.886	45
30	5.222	2.955	6.093	3.447	6.963	3.939	7.833	4.432	8.704	4.924	30
45	5.209	2.977	6.077	3.474	6.946	3.970	7.814	4.466	8.682	4.962	15
30 0	5.196	3.000	6.062	3.500	6.928	4.000	7.794	4.500	8.660	5.000	60 0
° ′	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	° ′
Bearing.	Distance 6.		Distance 7.		Distance 8.		Distance 9.		Distance 10.		Bearing.

30°— 45°

Bearing.	Distance 1.		Distance 2.		Distance 3.		Distance 4.		Distance 5.		Bearing.
° ′	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	° ′
30 15	0.864	0.504	1.728	1.008	2.592	1.511	3.455	2.015	4.319	2.519	59 45
30	0.862	0.508	1.723	1.015	2.585	1.523	3.447	2.030	4.308	2.538	30
45	0.859	0.511	1.719	1.023	2.578	1.534	3.438	2.045	4.297	2.556	15
31 0	0.857	0.515	1.714	1.030	2.572	1.545	3.429	2.060	4.286	2.575	59 0
15	0.855	0.519	1.710	1.038	2.565	1.556	3.420	2.075	4.275	2.594	45
30	0.853	0.522	1.705	1.045	2.558	1.567	3.411	2.090	4.263	2.612	30
45	0.850	0.526	1.701	1.052	2.551	1.579	3.401	2.105	4.252	2.631	15
32 0	0.848	0.530	1.696	1.060	2.544	1.590	3.392	2.120	4.240	2.650	58 0
15	0.846	0.534	1.691	1.067	2.537	1.601	3.383	2.134	4.229	2.668	45
30	0.843	0.537	1.687	1.075	2.530	1.612	3.374	2.149	4.217	2.686	30
45	0.841	0.541	1.682	1.082	2.523	1.623	3.364	2.164	4.205	2.705	15
33 0	0.839	0.545	1.677	1.089	2.516	1.634	3.355	2.179	4.193	2.723	57 0
15	0.836	0.548	1.673	1.097	2.509	1.645	3.345	2.193	4.181	2.741	45
30	0.834	0.552	1.668	1.104	2.502	1.656	3.336	2.208	4.169	2.760	30
45	0.831	0.556	1.663	1.111	2.494	1.667	3.326	2.222	4.157	2.778	15
34 0	0.829	0.559	1.658	1.118	2.487	1.678	3.316	2.237	4.145	2.796	56 0
15	0.827	0.563	1.653	1.126	2.480	1.688	3.306	2.251	4.133	2.814	45
30	0.824	0.566	1.648	1.133	2.472	1.699	3.297	2.266	4.121	2.832	30
45	0.822	0.570	1.643	1.140	2.465	1.710	3.287	2.280	4.108	2.850	15
35 0	0.819	0.574	1.638	1.147	2.457	1.721	3.277	2.294	4.096	2.868	55 0
15	0.817	0.577	1.633	1.154	2.450	1.731	3.267	2.309	4.083	2.886	45
30	0.814	0.581	1.628	1.161	2.442	1.742	3.257	2.323	4.071	2.904	30
45	0.812	0.584	1.623	1.168	2.435	1.753	3.246	2.337	4.058	2.921	15
36 0	0.809	0.588	1.618	1.176	2.427	1.763	3.236	2.351	4.045	2.939	54 0
15	0.806	0.591	1.613	1.183	2.419	1.774	3.226	2.365	4.032	2.957	45
30	0.804	0.595	1.608	1.190	2.412	1.784	3.215	2.379	4.019	2.974	30
45	0.801	0.598	1.603	1.197	2.404	1.795	3.205	2.393	4.006	2.992	15
37 0	0.799	0.602	1.597	1.204	2.396	1.805	3.195	2.407	3.993	3.009	53 0
15	0.796	0.605	1.592	1.211	2.388	1.816	3.184	2.421	3.980	3.026	45
30	0.793	0.609	1.587	1.218	2.380	1.826	3.173	2.435	3.967	3.044	30
45	0.791	0.612	1.581	1.224	2.372	1.837	3.163	2.449	3.953	3.061	15
38 0	0.788	0.616	1.576	1.231	2.364	1.847	3.152	2.463	3.940	3.078	52 0
15	0.785	0.619	1.571	1.238	2.356	1.857	3.141	2.476	3.927	3.095	45
30	0.783	0.623	1.565	1.245	2.348	1.868	3.130	2.490	3.913	3.113	30
45	0.780	0.626	1.560	1.252	2.340	1.878	3.120	2.504	3.899	3.130	15
39 0	0.777	0.629	1.554	1.259	2.331	1.888	3.109	2.517	3.886	3.147	51 0
15	0.774	0.633	1.549	1.265	2.323	1.898	3.098	2.531	3.872	3.164	45
30	0.772	0.636	1.543	1.272	2.315	1.908	3.086	2.544	3.858	3.180	30
45	0.769	0.639	1.538	1.279	2.307	1.918	3.075	2.558	3.844	3.197	15
40 0	0.766	0.643	1.532	1.286	2.298	1.928	3.064	2.571	3.830	3.214	50 0
15	0.763	0.646	1.526	1.292	2.290	1.938	3.053	2.584	3.816	3.231	45
30	0.760	0.649	1.521	1.299	2.281	1.948	3.042	2.598	3.802	3.247	30
45	0.758	0.653	1.515	1.306	2.273	1.958	3.030	2.611	3.788	3.264	15
41 0	0.755	0.656	1.509	1.312	2.264	1.968	3.019	2.624	3.774	3.280	49 0
15	0.752	0.659	1.504	1.319	2.256	1.978	3.007	2.637	3.759	3.297	45
30	0.749	0.663	1.498	1.325	2.247	1.988	2.996	2.650	3.745	3.313	30
45	0.746	0.666	1.492	1.332	2.238	1.998	2.984	2.664	3.730	3.329	15
42 0	0.743	0.669	1.486	1.338	2.229	2.007	2.973	2.677	3.716	3.346	48 0
15	0.740	0.672	1.480	1.345	2.221	2.017	2.961	2.689	3.701	3.362	45
30	0.737	0.676	1.475	1.351	2.212	2.027	2.949	2.702	3.686	3.378	30
45	0.734	0.679	1.469	1.358	2.203	2.036	2.937	2.715	3.672	3.394	15
43 0	0.731	0.682	1.463	1.364	2.194	2.046	2.925	2.728	3.657	3.410	47 0
15	0.728	0.685	1.457	1.370	2.185	2.056	2.913	2.741	3.642	3.426	45
30	0.725	0.688	1.451	1.377	2.176	2.065	2.901	2.753	3.627	3.442	30
45	0.722	0.692	1.445	1.383	2.167	2.075	2.889	2.766	3.612	3.458	15
44 0	0.719	0.695	1.439	1.389	2.158	2.084	2.877	2.779	3.597	3.473	46 0
15	0.716	0.698	1.433	1.396	2.149	2.093	2.865	2.791	3.582	3.489	45
30	0.713	0.701	1.427	1.402	2.140	2.103	2.853	2.804	3.566	3.505	30
45	0.710	0.704	1.420	1.408	2.131	2.112	2.841	2.816	3.551	3.520	15
45 0	0.707	0.707	1.414	1.414	2.121	2.121	2.828	2.828	3.536	3.536	45 0
° ′	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	° ′
Bearing.	Distance 1.		Distance 2.		Distance 3.		Distance 4.		Distance 5.		Bearing.

45°— 60°

30°—45°

Bearing.	Distance 6.		Distance 7.		Distance 8.		Distance 9.		Distance 10.		Bearing.
° ′	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	° ′
30 15	5.183	3.023	6.047	3.526	6.911	4.030	7.775	4.534	8.638	5.038	**59** 45
30	5.170	3.045	6.031	3.553	6.893	4.060	7.755	4.568	8.616	5.075	30
45	5.156	3.068	6.016	3.579	6.875	4.090	7.735	4.602	8.594	5.113	15
31 0	5.143	3.090	6.000	3.605	6.857	4.120	7.715	4.635	8.572	5.150	**59** 0
15	5.129	3.113	5.984	3.631	6.839	4.150	7.694	4.669	8.549	5.188	45
30	5.116	3.135	5.968	3.657	6.821	4.180	7.674	4.702	8.526	5.225	30
45	5.102	3.157	5.952	3.683	6.803	4.210	7.653	4.736	8.504	5.262	15
32 0	5.088	3.180	5.936	3.709	6.784	4.239	7.632	4.769	8.481	5.299	**58** 0
15	5.074	3.202	5.920	3.735	6.766	4.269	7.612	4.802	8.457	5.336	45
30	5.060	3.224	5.904	3.761	6.747	4.298	7.591	4.836	8.434	5.373	30
45	5.046	3.246	5.887	3.787	6.728	4.328	7.569	4.869	8.410	5.410	15
33 0	5.032	3.268	5.871	3.812	6.709	4.357	7.548	4.902	8.387	5.446	**57** 0
15	5.018	3.290	5.854	3.838	6.690	4.386	7.527	4.935	8.363	5.483	45
30	5.003	3.312	5.837	3.864	6.671	4.416	7.505	4.967	8.339	5.519	30
45	4.989	3.333	5.820	3.889	6.652	4.445	7.483	5.000	8.315	5.556	15
34 0	4.974	3.355	5.803	3.914	6.632	4.474	7.461	5.033	8.290	5.592	**56** 0
15	4.960	3.377	5.786	3.940	6.613	4.502	7.439	5.065	8.266	5.628	45
30	4.945	3.398	5.769	3.965	6.593	4.531	7.417	5.098	8.241	5.664	30
45	4.930	3.420	5.752	3.990	6.573	4.560	7.395	5.130	8.217	5.700	15
35 0	4.915	3.441	5.734	4.015	6.553	4.589	7.372	5.162	8.192	5.736	**55** 0
15	4.900	3.463	5.716	4.040	6.533	4.617	7.350	5.194	8.166	5.772	45
30	4.885	3.484	5.699	4.065	6.513	4.646	7.327	5.226	8.141	5.807	30
45	4.869	3.505	5.681	4.090	6.493	4.674	7.304	5.258	8.116	5.843	15
36 0	4.854	3.527	5.663	4.115	6·472	4.702	7.281	5.290	8.090	5.878	**54** 0
15	4.839	3.548	5.645	4.139	6.452	4.730	7.258	5.322	8.064	5.913	45
30	4.823	3.569	5.627	4.164	6.431	4.759	7.235	5.353	8.039	5.948	30
45	4.808	3.590	5.609	4.188	6.410	4.787	7.211	5.385	8.013	5.983	15
37 0	4.792	3.611	5.590	4.213	6.389	4.815	7.188	5.416	7.986	6.018	**53** 0
15	4.776	3.632	5.572	4.237	6.368	4.842	7.164	5.448	7.960	6.053	45
30	4.760	3.653	5.554	4.261	6.347	4.870	7.140	5.479	7.934	6.088	30
45	4.744	3.673	5.535	4.286	6.326	4.898	7.116	5.510	7.907	6.122	15
38 0	4.728	3.694	5.516	4.310	6.304	4.925	7.092	5.541	7.880	6.157	**52** 0
15	4.712	3.715	5.497	4.334	6.283	4.953	7.068	5.572	7.853	6.191	45
30	4.696	3.735	5.478	4.358	6.261	4.980	7.043	5.603	7.826	6.225	30
45	4.679	3.756	5.459	4.381	6.239	5.007	7.019	5.633	7.799	6.259	15
39 0	4.663	3.776	5.440	4.405	6.217	5.035	6.994	5.664	7.772	6.293	**51** 0
15	4.646	3.796	5.421	4.429	6.195	5.062	6.970	5.694	7.744	6.327	45
30	4.630	3.816	5.401	4.453	6.173	5.089	6.945	5.725	7.716	6.361	30
45	4.613	3.837	5.382	4.476	6.151	5.116	6.920	5.755	7.688	6.394	15
40 0	4.596	3.857	5.362	4.500	6.128	5.142	6.894	5.785	7.660	6.428	**50** 0
15	4.579	3.877	5.343	4.523	6.106	5.169	6.869	5.815	7.632	6.461	45
30	4.562	3.897	5.323	4.546	6.083	5.196	6.844	5.845	7.604	6.495	30
45	4.545	3.917	5.303	4.569	6.061	5.222	6.818	5.875	7.576	6.528	15
41 0	4.528	3.936	5.283	4.592	6.038	5.248	6.792	5.905	7.547	6.561	**49** 0
15	4.511	3.956	5.263	4.615	6.015	5.275	6.767	5.934	7.518	6.594	45
30	4.494	3.976	5.243	4.638	5.992	5.301	6.741	5.964	7.490	6.626	30
45	4.476	3.995	5.222	4.661	5.968	5.327	6.715	5.993	7.461	6.659	15
42 0	4.459	4.015	5.202	4.684	5.945	5.353	6.688	6.022	7.431	6.691	**48** 0
15	4.441	4.034	5.182	4.707	5.922	5.379	6.662	6.051	7.402	6.724	45
30	4.424	4.054	5.161	4.729	5.898	5.405	6.635	6.080	7.373	6.756	30
45	4.406	4.073	5.140	4.752	5.875	5.430	6.609	6.109	7.343	6.788	15
43 0	4.388	4.092	5.119	4.774	5.851	5.456	6.582	6.138	7.314	6.820	**47** 0
15	4.370	4.111	5.099	4.796	5.827	5.481	6.555	6.167	7.284	6.852	45
30	4.352	4.130	5.078	4.818	5.803	5.507	6.528	6.195	7.254	6.884	30
45	4.334	4.149	5.057	4.841	5.779	5.532	6.501	6.224	7.224	6.915	15
44 0	4.316	4.168	5.035	4.863	5.755	5.557	6.474	6.252	7.193	6.947	**46** 0
15	4.298	4.187	5.014	4.885	5.730	5.582	6.447	6.280	7.163	6.978	45
30	4.280	4.206	4.993	4.906	5.706	5.607	6.419	6.308	7.133	7.009	30
45	4.261	4.224	4.971	4.928	5.681	5.632	6.392	6.336	7.102	7.040	15
45 0	4.243	4.243	4.950	4.950	5.657	5.657	6.364	6.364	7.071	7.071	**45** 0
° ′	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	° ′
Bearing.	Distance 6.		Distance 7.		Distance 8.		Distance 9.		Distance 10.		Bearing.

45°—60°

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GINN & COMPANY,
Boston.